## memo

to Dustin Nilsen and Will Norris, City of Hood River<br>from Nathan Polanski, PE, Alex Dupey, AICP, MIG<br>re $\quad$ The Heights Streetscape Plan - Evaluation Summary of Design Alternatives<br>date February 25, 2022

This memorandum summarizes findings from the project team's evaluation of the preliminary design alternatives. The evaluation included a traffic analysis and a review of project specific evaluation criteria to determine the alignment of design alternatives with the Urban Renewal Agency Board (URAB) adopted project goals.

The memorandum includes an overview of:

- how each design alternative aligns with project goals,
- key findings from the traffic analysis,
- which evaluation criteria appear to be differentiators when comparing the performance of design alternatives,
- design adjustments needed to improve the mobility performance based on issues observed during the traffic analysis, and
- cost considerations for the design alternative for future implementation.

The purpose of this memorandum is to provide an overview of the design alternatives and evaluation process and to identify and focus on key issues that distinguish between the design alternatives. These key issues will be used to lead a discussion with the Urban Renewal Advisory Committee (URAC), URAB, ODOT and the public to understand the trade-offs between the design alternatives as we develop a preferred design alternative.

## Evaluation Process

The evaluation is based on the evaluation criteria and design alternatives approved by the URAB and URAC on October 21, 2021, with the following modifications based on URAB and URAC feedback:

1. Intersection at $13^{\text {th }}$ Street/May Street: Given the concern for both traffic flow, and routine closures impacting vehicle traffic travelling south uphill on $13^{\text {th }}$, as well as the expressed safety concern for school and pedestrian traffic crossing $13^{\text {th }}$ between May Street Elementary and Hood River Middle School, the URA felt this intersection would be best served by a roundabout rather than a traffic signal (the existing intersection has two-way stop control for east/west traffic and the City's adopted Transportation System Plan calls for a roundabout or traffic signal).
2. Modifications to Design Alternative 3: the URA recommended exploring two modifications to Design Alternative 3:
a. Explore shifting on-street parking along $13^{\text {th }}$ Street from the east side of street to the west side of the street to improve on street parking access
b. Explore modifying the street design along $12^{\text {th }}$ Street to eliminate the straight line-ofsight and calm traffic between Belmont Street and May Street.

The evaluation, which included quantitative and qualitative criteria, considered the overall function of each alternative and the individual function of $12^{\text {th }}$ and $13^{\text {th }}$ Streets. This approach helped the project team better understand how each alternative aligns with project goals given differences between the designs for $12^{\text {th }}$ and $13^{\text {th }}$ Street within a single alternative.

While the evaluation does get into the details of each design the purpose of the evaluation is not intended to compare the performance of individual criteria but to gain a more complete understanding of the overall performance of each design alternative as related to project goals. This will help guide conversations with the URA and community as we discuss trade-offs between the designs and work towards developing a preferred design alternative, which we anticipate may combine components from each of the design alternatives.

## Overview of Design Alternatives

The preliminary design alternatives (Appendix D) identify potential elements that could be considered, together or in part, for the preferred design that will be developed with URAB, URAC and community input. The intent of these preliminary alternatives is not to provide a single alternative that will be selected, but options for consideration. The preferred alternative may combine aspects of more than one design alternative that best meets the goals of the project and incorporates community input.

## Design Alternative 1

This alternative converts existing one-way traffic on $12^{\text {th }}$ and $13^{\text {th }}$ Streets to two-way traffic, eliminating one-way streets that lead to wrong-way drivers who are unfamiliar with the area. Two travel lanes are maintained on each street; however, each street is designed differently:

- $12^{\text {th }}$ Street is designed to function as more of a traditional "Main Street" with two-way vehicle travel and parking on both sides of the street.
- $13^{\text {th }}$ Street is designed to function as more of a "Mobility Street" that focuses on moving people driving and biking north and south through the Heights.

This approach prioritizes people headed to local destinations along $12^{\text {th }}$ Street while people passing through the Heights can use $13^{\text {th }}$ Street. The conversion to two-way traffic also provides an all ages and abilities bike facility on one-way separated bike lanes, which are separated from the roadway with a curb and are not located adjacent to parking. Key intersections at $12^{\text {th }}$ and $13^{\text {th }}$ Streets along May Street and Belmont Avenue would be controlled with traffic signals.

## Design Alternative 2

This alternative reduces $12^{\text {th }}$ Street and $13^{\text {th }}$ Street to one lane of one-way traffic in each direction. This alternative was developed to slow traffic through the Heights, provide shared space for walking and biking, and provide on-street parking on $12^{\text {th }}$ and $13^{\text {th }}$ Streets. For this alternative:

- $12^{\text {th }}$ Street is designed as a "Parking Street" with on-street parking on both sides of the street.
- $13^{\text {th }}$ Street is designed as a "Green Street" with a shared use path for people walking and biking and a wider planting area for healthy trees and landscaping.

A mini roundabout at $13^{\text {th }} /$ May and a double roundabout at $13^{\text {th }} / 12^{\text {th }} /$ Belmont help reduce impacts to traffic flow (compared to a traffic signal) for the one lane, one-way roadways.

## Design Alternative 3

This alternative changes how the streets are used and how traffic and people move through the Heights. This alternative converts the existing one-way traffic on $13^{\text {th }}$ Street to two-way traffic while maintaining one-way traffic on $12^{\text {th }}$ Street. For this alternative:

- $12^{\text {th }}$ Street is designed as more of a "People Street" with diagonal parking, a two-way protected bike lane (or cycle track), and opportunities for gathering spaces.
- $13^{\text {th }}$ Street is designed to function as more of a "Vehicle Street" with a center turn lane and onstreet parking.

This alternative was developed to balance the community's desires to maintain traffic flow, accommodate on-street parking, and create safe places for people biking and gathering. Key intersections at $12^{\text {th }}$ and $13^{\text {th }}$ Streets along May Street and Belmont Avenue would be controlled with traffic signals.

## Goal Alignment

When the design alternatives were initially presented to the URAB, we highlighted how each design alternative aligned with project goals based on key evaluation criteria (Appendix A). Since that initial presentation a full evaluation of the design alternatives has been completed across all criteria and additional implementation feasibility criteria. This full evaluation uses the same rating system based on how each criterion aligns with the project goals:


Based on feedback received from the URAB and URAC on October 21, 2021 each criteria is weighted equally, with no prioritization of one goal over another.

The project goals adopted by the URAB in Phase 1 are:
Project Goal 1: Calm traffic and improve intersections to improve safety for people driving, walking, biking, taking transit and supporting local businesses.

Project Goal 2: Preserve and promote a livable community and economy through streetscape improvements that increases safety for people walking and biking and addresses parking needs to support local business access, and future mixed-use development.

Project Goal 3: Create an identify for the Heights that reflects the diverse culture and history of the area and as destination for local residents for goods and services.

Project Goal 4: Create streets and gathering spaces that provide safe, comfortable places for people walking, accessing transit, and biking along and across the corridor and that connects area recreation and commercial destinations and neighborhoods.

Project Goal 5: Support existing and future development by maintaining and improving utility infrastructure as part of the streetscape project.

Project Goal 6: Engage local residents and businesses, the school district, and those that use the corridor to provide ongoing input in the streetscape project.

- Note, this goal is not part of the current evaluation but will be part of the final evaluation after the public has had the opportunity to review and provide comments on the design alternatives and evaluation process.

Project Goal 7: Provide locations for people to gather, to stop and rest.

The additional feasibility criteria that are part of this evaluation include the following:

- Potential cost and funding opportunities for implementation
- Potential construction impacts
- Ability to maintain the proposed infrastructure improvements
- Ease of obtaining ODOT design approval
- Property impacts and the potential need for right of way acquisition

Table 1 is a summary of the full evaluation for each design alternative. The colored rating shown for each goal is an average rating derived from ratings for each individual criterion based on how the design alternative aligns with project goals. Based on this evaluation Design Alternative 1 aligns best with project goals followed by Design Alternative 3 and then Design Alternative 2.

Table 1: Evaluation Summary of Preliminary Design Alternatives

|  | Goal 1 Traffic | Goal 2 <br> Livability | Goal 3 <br> Identity | Goal 4 Connecting People | Goal 5 Utility | Goal 7 <br> Placemaking | Feasibility |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Design Alternative 1 |  | $\square$ | $\infty$ |  | $\square$ |  | ( |
| Design Alternative 2 |  | $\square$ | $\Delta$ |  |  |  | $\cdots$ |
| Design Alternative 3 | $\square$ | $\square$ |  |  |  |  |  |

What stands out from this table is that many of the ratings have a "good" alignment with projects goals and only a few ratings have "very good" or "poor" alignment with project goals.

Of the seven project goals:

- two goals (4 and 7) have the same rating for each alternative,
- three goals (2,3 and 5 ) are only separated by one rating "step" across each alternative, and
- Goal 1 and the Feasibility Criteria have different ratings for each alternative.

For Goal 1 and the Feasibility Criteria, which have all different ratings, the variation in ratings suggests these categories might be differentiators when comparing alternatives:

- Goal 1 evaluation metrics include how the design accomodates vehicular traffic, improves intersection functionality, and accomodates truck and emergency vehicle access.
- Feasibility Criteria generally refers to the ablity to fund and construct street improvements and metrics include considerations such as costs and funding differences, implementation, construction impacts, obtaining design approval, property impacts, and additional right of way land needed.

For both of these categories Design Alternative 2 aligns poorly with project goals. Goal 1 was identified by the URAB as being the most important goal for addressing community needs. The following discussion highlights findings from the traffic analysis.

## Traffic Analysis

Each of the design alternatives creates significant changes from today's traffic patterns and reduces the comfort and convenience for vehicular traffic. Therfore, a critical part in identifying a preferred design for the Heights is understanding how vehicle mobility will be impacted today and in the future. To provide a comparison to today's vehicle traffic the traffic analysis evaluated all three design alternatives and the Transportation System Plan (TSP) Scenario. This section highlights key findings from the traffic analysis (see Appendix B for the complete analysis).

The evaluation of future traffic is based on forecasted traffic volumes for 2039 from the City's Transportation System Plan.

## Traffic Flow and Intersection Performance

All three alternatives result in more traffic congestion and delay travelling through the Heights compared to the future TSP Scenario.

Design Alternative 1 performs the best and has the least delay, adding approximately 30 additional seconds for vehicles travelling through the Heights.

Design Alternative 2 performs the worst with vehicles experiencing delays up to approximately 90 additional seconds to travel through the Heights. At key intersections vehicle queues extend for multiple blocks for Design Alternative 2 and are significantly longer than vehicle queues for Design Alternatives 1 and 3 .

Alternative 2, with only one lane of one-way traffic, could have the highest potential to divert traffic away from the Heights. However, because there are not good alternate routes through the Heights (i.e. a lack of parallel routes to 12th and 13th Streets) the amount of traffic that could travel a different route is low regardless of the design alternative.

The performance of Design Alternative 3 depends on the direction of travel. Vehicles travelling south through the Heights on 13th Street might experience delays similar to Design Alternative 2 (up to 90 additional seconds to travel through the Heights) whereas northbound delays on 13th are expected to be more reasonable and increase by less than 30 seconds.

## Key Intersection Bottlenecks

Two key intersections, $13^{\text {th }} /$ May and $13^{\text {th }} / 12^{\text {th }} /$ Belmont, function as "bottlenecks" for vehicle performance in each of the alternatives. These locations function poorly for each of the alternatives and require adjustments to the preliminary intersection designs (i.e. capacity enhancements) to improve the performance at the intersections and overall function of the design alternatives. These adjustments will increase property impacts at intersections to accommodate additional or longer intersection channelization and the streetscape experience near the intersections.

## Roundabouts

Although roundabouts are only included in Design Alternatives 2 and 3 both roundabouts and traffic signals were tested at each major intersection ( $13^{\text {th }} /$ May, $13^{\text {th }} /$ Belmont, $13^{\text {th }} / 12^{\text {th }} /$ Belmont $)$ for each of the alternatives. Because the intersection control (i.e. roundabout vs signal) is not necessarily a requirement of the broader circulation changes and active transportation improvements this comparison was conducted to understand potential trade-offs for selecting intersection controls.

The results showed that given the high traffic volumes on 13th Street, single-lane roundabouts do not perform well, with significant delay expected, similar to the preliminary intersection design with a traffic
signal. To improve the performance of the roundabouts, a second lane would need to be added through part of the roundabout. For example:

- 13th/May - a single lane mini roundabout (as originally drawn), or even a full-sized single-lane roundabout, would fail to meet mobility targets during the 2039 p.m. peak hour and would experience significant congestion and long vehicle queues. Instead, a larger roundabout with a second southbound lane through the intersection would be needed, making the roundabout a partial multilane roundabout. Due to the circulation changes associated with Alternative 3, a westbound right turn slip lane would also be required.
- $13^{\text {th }} / 12^{\text {th }} /$ Belmont - a double roundabout such as the one shown in Design Alternative 2 should include two southbound lanes through the roundabout and two northbound lanes exiting the roundabout on $12^{\text {th }}$ Street. The northbound lanes would extend one or two blocks north of Belmont and would impact the streetscape character and experience on $12^{\text {th }}$ Street.

These changes would greatly increase the footprints of the intersections and the street approaching/ exiting the roundabout, compared to what is currently drawn, and will require significant right of way acquisition (see Figure 1), have greater impacts on adjacent properties, and significantly increase implementation costs. At $13^{\text {th }} /$ May the existing topography and slopes of the roadway also present challenges for a larger roundabout.

Figure 1 - Footprint comparison of potential future traffic signal vs roundabout at 13th Street/May Street


## Design Adjustments to Improve Vehicle Performance

The traffic analysis memo (Appendix B) discusses specific design adjustments (or mitigation measures) needed for the intersection concepts at the two "bottleneck" intersections of $13^{\text {th }} /$ May and $13^{\text {th }} / 12^{\text {th }} /$ Belmont. These adjustments are needed to address significant mobility deficiency issues for each design alternative.

To identify these adjustments an alternative-by-alternative analysis was performed to confirm that reasonable modifications could be made to the original intersection concepts to achieve "acceptable" results. Although these adjustments will be further refined with the preferred design alternative, we
recommend communicating these modifications to the URAB, URAC, ODOT, and community when the preliminary design alternatives and evaluation are presented; while the adjustments help improve operational issues they do come with tradeoffs including additional property impacts or turn restrictions.

Updated intersection graphics that incorporate the adjustments will be developed for the final preferred design alternative.

## How Design Alternatives Differ

In addition to exploring the traffic analysis we also examine ratings within individual criteria to look for differences in the performance across design alternatives. The average ratings for each goal in Table 1 were based from ratings for each individual criterion, which included separate ratings for $12^{\text {th }}$ and $13^{\text {th }}$ for each design alternative. A matrix of the full evaluation and individual ratings for all of the evaluation criteria is included in Appendix C.

Table 2 below presents a more detailed graphic of the full evaluation matrix. Each colored square corresponds to a rating given to a specific street ( $12^{\text {th }}$ or $13^{\text {th }}$ ) for each specific evaluation criteria (note, gray squares indicate a criterion that did not apply). Each column of colored squares represents the ratings across a single criterion for each design alternative.

Goal 2


Although the graphic in Table 2 does not have labels to indicate which column is associated with a specific evaluation criterion it does show at a high-level how the ratings vary across evaluation criteria within each goal and across each of the design alternatives.
Table 2: Evaluation Summary of Preliminary Design Alternatives

|  |  | Goal 1 | Goal 2 | Goal 3 | Goal 4 | Goal 5 Goal 7 | Feasibility |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Design | $12^{\text {th }}$ |  |  |  |  |  |  |
| Alternative 1 | $13^{\text {th }}$ |  |  |  |  |  |  |
| Design | $12^{\text {th }}$ |  |  |  |  |  |  |
| Alternative 2 | $13^{\text {th }}$ |  |  |  |  |  |  |
| Design | $12^{\text {th }}$ |  |  |  |  |  |  |
| Alternative 3 | $13^{\text {th }}$ |  |  |  |  |  |  |

Looking closely at this graphic we can identify a handful of evaluation criteria (shown as columns) that have a wider range of color coding from top to bottom. These evaluation criteria have ratings that range from "very good to poor" or "good to undesirable" across the three design alternatives. These criteria are:

- Goal 1 (column 1) - Traffic calming: All alternatives were rated as having very good traffic calming except for the three-lane street section on $13^{\text {th }}$ Street in Design Alternative 3. The three-lane street section is not ideal for calming traffic (however, the typical street section can be mitigated by integrating design measures along the street such as medians).
- Goal 1 (column 2) - Accommodates vehicular traffic: Design Alternative 2 with single travel lanes performs significantly the worse for vehicle traffic along the corridor and at intersections and present challenges for emergency service vehicles and was rated as undesirable.
- Goal 2 (column 1) - Accommodates parking: Parking is maintained or reduced in all scenarios, however in Design Alternative 1 parking is removed entirely from $13^{\text {th }}$ Street, which is rated as undesirable.
- Goal 4 (column 1) - Comfortable places for walking: Design Alternative 2 provides wider sidewalks than existing width and aligns very good with project goals. However, although sidewalks are not reduced in any alternative, the sidewalk on $13^{\text {th }}$ Street in Design Alternative 3 has no buffer from the northbound travel lane and was given a poor rating.
- Goal 7 - Opportunities for Placemaking: In Design Alternative $312^{\text {th }}$ Street functions as a "People Street" and offers very good opportunities for placemaking but $13^{\text {th }}$ Street is designed as a "Vehicle Street" had poor opportunities for placemaking.
- Feasibility criteria (column 2) - Potential implementation considerations and construction impacts: The implementation of Design Alternatives 1 and 3 was rated as good or very good given the similarities for where future travel lanes would be located compared to today's roadway and because the wider two- or three-lane streets provide more flexibility, whereas the single travel lanes in Design Alternative 2 was rated as poor due to concerns associated with having one travel lane in each direction through the Heights, which creates both challenges for both operations and construction.
- Feasibility criteria, last column - Property impacts/ROW acquisition: the roundabouts in Design Alternatives 2 and 3 require more right of way acquisition and have greater impacts on adjacent properties than traffic signals would have at the same intersections and were rated as poor..

Although we have only singled out a few evaluation criteria, when coupled with key findings from the traffic analysis, we can begin to see where key differences exist between the design alternatives. Based on our analysis and evaluation of design alternatives we have identified the following as key elements to be discussed further with the URAB, URAC, ODOT, and broader community:

1. Confirm the level of congestion that can be tolerated for vehicle traffic to achieve a safer, more comfortable street environment for all modes of travel.
2. Key intersections are not well suited for roundabouts.
3. Impacts to parking, loading, and delivery vary between the design alternatives with the impact depending on the configuration and location of on-street parking and number of travel lanes on the street, which can impact access.
4. One lane streets rate poor in terms of flexibility, adaptability, and feasibility compared to two lane streets.
5. Are future bike connections and alignment with Safe Routes to School recommendations, which best align with Design Alternative 3.

## Cost Considerations for Constructing Future Street Improvements

A planning level cost estimate was developed for each design alternative to identify an order of magnitude cost range for constructing future street improvements and to determine whether significant cost differences exist between the design alternatives. This cost range should not be used for budgeting or future project planning. A cost estimate for the preferred design alternative will be developed during the next phase of the project for the City and Urban Renewal Agency's use in planning future street improvements.

The order of magnitude cost range was developed using the following steps:

1. A list of typical unit costs was identified for each element shown in the typical street cross sections (e.g. unit costs per square foot of concrete sidewalk, asphalt pavement, planting area, bike lane, planting area and linear foot for curb and gutter).
2. Unit costs were multiplied by the widths shown in the typical street sections to identify a linear foot cost for constructing the street.
3. Linear foot costs for each street were multiplied by the lengths of each roadway.
4. Cost allowances were added for intersection improvements, including key intersections (i.e. roundabouts and traffic signals) and minor intersections at local streets (e.g. A, B, C Streets).
5. Costs were added for providing new storm drainage infrastructure, planting street trees, adjusting existing utilities to grade, removing existing pavement and sidewalks, and providing street furnishings.
6. Costs were added as a percentage of total costs to account for site preparation, earthwork, temporary traffic control, and mobilization.
7. Cost allowances were added for property acquisition at $13^{\text {th }} /$ May and $13^{\text {th }} /$ Belmont for the construction of traffic signals and roundabouts. These allowances are not based on a market analysis and include the following assumptions:
a. $\$ 125 \mathrm{k}$ to accommodate a traffic signal and additional channelization
b. $\$ 1.5 \mathrm{M}$ to accommodate a roundabout at $13^{\text {th }} / \mathrm{May}$
c. $\$ 2.5 \mathrm{M}$ to accommodate a double roundabout at $13^{\text {th }} /$ Belmont $/ 12^{\text {th }}$
8. Finally, costs were added as a percentage of total costs for design contingency and the phasing of future street improvements; the phasing allowance recognizes the project area will not be constructed at one time and allows for some rework as portions of the streetscape are implemented over.

The table below identifies a possible cost range for constructing new streets and intersections within the Heights. Additional assumptions and notes that apply to the development of this cost include:

- Assumes that all of the study area streets are fully reconstructed.
- Does not include new street or pedestrian lighting.
- Does not include costs to replace existing utilities or underground exiting overheard utilities.
- Does not include soft costs, such as design and engineering, city project management, permitting, and construction management.
- Includes an allowance for treating stormwater runoff from roadways.
- Does not include a cost for flow control to detain stormwater runoff from new pavement surfaces. If required, infrastructure for flow control will be designed and costed as part of future design phases.
- Does not include escalation.

Table 1: Planning level range of cost for constructing future street improvements

|  | Low Range | High Range |
| :--- | :---: | :---: |
| Design Alternative 1 | $\$ 26 \mathrm{M}$ | $\$ 33 \mathrm{M}$ |
| Design Alternative 2 | $\$ 35 \mathrm{M}$ | $\$ 44 \mathrm{M}$ |
| Design Alternative 3 | $\$ 31 \mathrm{M}$ | $\$ 39 \mathrm{M}$ |

Similar to the findings of the traffic analysis the key differences for costs between the design alternatives is the cost to implement key intersection improvements. The larger footprint for the roundabouts requires more cost to construct and acquire property.

Although this range in costs assumes full reconstruction of the full right of way, it is anticipated that some elements of the project could be partially retrofit and may not need full replacement.

As noted above this cost exercise was conducted to identify a possible order of magnitude cost range for constructing future street improvements and to determine whether significant cost differences exist between the design alternatives. This cost range should not be used for future project planning as it does not include design, engineering, and management and other soft costs. A planning level cost estimate for the preferred design alternative will be developed during the next phase of the project for the City and Urban Renewal Agency's use in planning future street improvements.

## Next Steps

We recommend sharing the results of the evaluation with the URAB and URAC while the project team prepares for a public open house to present the preliminary design alternatives and evaluation findings to the public. The purpose of the open house will be to gather public feedback on the design alternatives to help the City and Urban Renewal Agency move forward with developing a preferred design alternative., which may combine aspects of more than one design alternative to best meets the goals of the project and incorporate community input.

Attached<br>Appendix A - Preliminary Evaluation Summary<br>Appendix B - Alternatives Transportation Evaluation Memorandum<br>Appendix C - Full Evaluation of Preliminary Design Alternatives<br>Appendix D - Preliminary Design Alternatives

## PRELIMINARY EVALUATION SUMMARY

This graphic presents is a side-by-side summary of the preliminary evaluation for each of the preliminary design alternatives and the City's current adopted plan in the TSP. This preliminary evaluation highlights key evaluation criteria and rates each alternative based on its alignment with the project goals.
Current

| Design |
| :---: |
| Adopted Plan |
| TSP |


| Design |
| :---: |
| Twornative 1 |
| Twe Two-way |

Capacional
The evaluation shown for operational capacity for each concept is not based on alignment with project goals
One lane, One-way

but how the roadway is anticipated to function based on the typical street cross sections proposed. | Design |
| :---: |
| Alternative 3 |
| Hybrid |

## Legend for Preliminary Evaluation

入 Very good alignment with project goals
A Good alignment with project goals


Average alignment with project goals

- Poor alignment with project goals
$\approx$ Undesirable alignment with project goals


## TECHNICAL MEMORANDUM

DATE: February 28, 2022
TO: Nathan Polanski, PE \| MIG
FROM: Alex Correa; Will McKenzie; Kayla Fleskes, PE; John Bosket, PE | DKS Associates

SUBJECT: Hood River Heights Streetscape Plan - Alternatives Project \#20203-000 Transportation Evaluation

This memorandum evaluates transportation conditions associated with alternatives being considered for improving multimodal travel within the Hood River Heights District, especially $12^{\text {th }}$ and $13^{\text {th }}$ Streets between May Street and the end of the couplet south of Belmont Avenue/Union Street. It is anticipated that this evaluation will act as a supplement to a larger evaluation of each alternative's ability to meet the project goals. The following sections provide a comparison of each alternative's strengths and weaknesses from the perspectives of travelers driving, walking, biking, and using transit (in the future).

## ALTERNATIVES EVALUATED

Concept drawings of the alternatives evaluated from the Heights Streetscape Plan project are included in Appendix A. Below is a summary of the major elements of each alternative and key assumptions made for the evaluation process that are not explicitly shown in the conceptual layouts.

- Design Alternative 1: Two-Lane, Two-Way Circulation
- Both 12th Street and 13th Street are converted to two-lane, two-way streets. 13th Street includes a separated bike lane in both directions, but all on-street parking is removed.
- 13th Street/May Street and 13th Street/Belmont Avenue were evaluated under conditions with a traffic signal and with a roundabout.
- Under the assumption of a traffic signal, the westbound lane figuration at 13th Street/May Street is assumed to be a dedicated left turn lane and a through/right lane rather than as drawn with a dedicated right turn lane and a through/left lane. This would require the through lane alignment to be adjusted through the intersection.
- Design Alternative 2: One-Lane, One-Way Circulation

。 Both 12th Street and 13th Street remain as one-way streets but are reduced to one lane in each direction.

- 13th Street/May Street was evaluated under conditions with a traffic signal and with a roundabout.
- 12th Street/Belmont Avenue and 12th Street/13th Street were evaluated as a joined "dog bone" roundabout where both intersections are fed into the same roundabout (See concept drawings in Appendix A for details).
- Union Street is assumed to be changed to right in/right out access and does not directly tie into the roundabout.
- Design Alternative 3: Hybrid Circulation

13th Street is a two-way, two-lane street with a center turn lane/median between 13th Street/Taylor Avenue and 13th Street/12th Street.
。 13th Street/May Street and 13th Street/Belmont Avenue were evaluated under conditions with a traffic signal and with a roundabout.

Under the assumption of a traffic signal, the westbound lane configuration at 13th Street/May Street is assumed to be a dedicated left turn lane and a through/right lane rather than as drawn with a dedicated right turn lane and a through/left lane. This would require the through lane alignment to be adjusted through the intersection.

## ALTERNATIVES EVALUATION

The alternatives were evaluated using performance metrics that describe conditions important to each of the major modes of travel in the corridor and that align with the goals of the project. The following sections describe conditions for people driving, walking, biking, and using transit beginning with conditions for people driving since the alternatives being considered will significantly alter travel patterns and speeds by automobile, which will in turn influence comfort and safety for the other modes of travel.

## CONDITIONS FOR PEOPLE DRIVING

The nature of all alternatives being considered involves a reallocation of the public right-of-way with the purpose of improving the balance of comfort and convenience for all modes of travel.
Each alternative lessens the amount of comfort and convenience for motor vehicle travel, which in the past has been given priority, but by varying degrees. The alternatives were evaluated for motor vehicle mobility using the following three-step process:

1. Traffic Volume Development - Future year traffic volumes were re-distributed throughout the Hood River transportation system due to changes in circulation brought on by characteristics of each design alternative such as intersection lane configurations, one-way vs two-way streets, number of lanes on each street, etc. Each alternative has a unique traffic volume set based on the re-distribution of trips in the area.
2. Intersection Performance Evaluation - Performance for all intersections within the study area was evaluated, utilizing the volumes developed in Step 1. Signalized and stopcontrolled intersection calculations were performed using Synchro 10th edition and Highway Capacity Manual $6^{\text {th }}$ Edition methodology. Roundabout intersection calculations were performed using PTV Vistro 2021 and Highway Capacity Manual 6 ${ }^{\text {th }}$ Edition methodology.

Intersection delay, level of service, volume-to-capacity ratio ( $\mathrm{v} / \mathrm{c}$ ), travel time, and vehicle queuing, were all used to evaluate mobility.
3. Alternative Mitigation - In cases where mobility deficiencies for motor vehicle travel were found to be significant, reasonable modifications to the original concept to improve conditions were tested.

Evaluation criteria for motor vehicle travel are not only limited to mobility. Accessibility for truck and emergency vehicles, impacts on property access, and safety were all evaluated for each alternative as well. For each alternative, the degree to which the criteria are supported by each of the main corridors along $12^{\text {th }}$ Street and $13^{\text {th }}$ Street has been rated, with brief descriptions provided below and a summary chart provided in Table 5.

## TRAFFIC VOLUME DEVELOPMENT AND DIVERSION IMPACTS

$12^{\text {th }}$ and $13^{\text {th }}$ Streets currently form a couplet through the Hood River Heights District. Each of the alternatives makes modifications to circulation on $12^{\text {th }}$ Street, $13^{\text {th }}$ Street, and May Street. To understand future traffic volume shifts based on the changes in circulation, each of the alternatives were coded into the Hood River travel forecasting model developed for the Hood River Transportation System Plan (TSP). Based on the changes in circulation identified in the model, the future 2039 "No-Build" traffic volumes ${ }^{1}$ were adjusted at each intersection.

In general, the following adjustments were made for each alternative:

- Alternative 1
- Both northbound and southbound traffic volumes were split between $12^{\text {th }}$ Street and $13^{\text {th }}$ Street with the conversion to two-way traffic. Approximately 55 percent of northbound traffic is expected to remain on $12^{\text {th }}$ Street, with 45 percent utilizing $13^{\text {th }}$ Street instead.
- Southbound volumes on $12^{\text {th }}$ Street are significantly lower than southbound volumes on $13^{\text {th }}$ Street given the limited connectivity north of May Street, representing only 15 to 20 percent of all traffic traveling southbound.
。 There is a slight increase in eastbound trips along May Street to the west of $13^{\text {th }}$ Street as the eastbound left turn at May Street/ $13^{\text {th }}$ Street, which is not allowed today, is allowed under Alternative 1.
With northbound travel now allowed on $13^{\text {th }}$ Street, the number of northbound left turning vehicles at May Street/ $12^{\text {th }}$ Street that subsequently turn right at $13^{\text {th }}$ Street is reduced by approximately 80 percent.
- Alternative 2
- Alternative 2 results in more diversion to the east and west than the other alternatives, but the amount of diverted traffic is relatively minor due to the limited north-south connectivity in the vicinity. To the west, about 75 p.m. peak hour southbound trips could be expected to divert to $22^{\text {nd }}$ Street and Belmont Avenue. This is expected to increase eastbound right turns at $13^{\text {th }}$ Street/Belmont Avenue by nearly 90 percent. To the east, where connectivity is

[^0]significantly more limited, there is the potential for a small amount (up to 25 p.m. peak hour trips) of trips to divert to local streets like $7^{\text {th }}$ Street and Pine Street.

- There is a slight increase in eastbound trips along May Street to the west of $13^{\text {th }}$ Street as the eastbound left turn at May Street/ $13^{\text {th }}$ Street, which is not allowed today, is allowed under Alternative 1.
- Alternative 3

Alternative 3 sees a slightly higher shift in northbound traffic to $13^{\text {th }}$ Street compared to Alternative 1 , with approximately 65 percent utilizing $13^{\text {th }}$ Street and 35 percent utilizing $12^{\text {th }}$ Street.

- There is a slight increase in eastbound trips along May Street to the west of $13^{\text {th }}$ Street as the eastbound left turn at May Street/ $13^{\text {th }}$ Street, which is not allowed today, is allowed under Alternative 1.

The average daily traffic volumes projected for the primary travel corridors of $12^{\text {th }}$ Street, $13^{\text {th }}$ Street, and May Street as a result of the circulation changes in each alternative are shown in Table 1. For reference, average daily traffic volumes today are approximately $9,700-10,600$ on $12^{\text {th }}$ and $13^{\text {th }}$ Street and 9,400 on May Street ${ }^{2}$.

Alternative 2 is expected to serve a similar amount of daily traffic on $12^{\text {th }}$ Street and $13^{\text {th }}$ Street as the No-Build conditions. Daily trips significantly increase on $13^{\text {th }}$ Street in both Alternative 3 and Alternative 1 as $13^{\text {th }}$ Street becomes the more natural through route. A corresponding decrease in daily traffic occurs on $12^{\text {th }}$ Street in Alternatives 1 and 3. Daily trips increase more significantly on $13^{\text {th }}$ Street in Alternative 3, as $13^{\text {th }}$ Street serves both northbound and southbound traffic while $12^{\text {th }}$ Street only serves northbound traffic and would be designed to be a slower "people street". Under both alternatives, $13^{\text {th }}$ Street would serve a significant amount of daily traffic in a single lane per direction (for reference, Cascade Avenue today serves approximately 12,000-14,000 vehicles per day).

Traffic on May Street between 12th Street and 13th Street decreases in Alternative 1 and Alternative 3 as northbound traffic no longer needs to turn left at $12^{\text {th }}$ Street and right on $13^{\text {th }}$ Street to travel through the Heights.

[^1]TABLE 1. APPROXIMATE 2039 DAILY TRAFFIC VOLUMES ON AREA STREETS

| STREET | APPROXIMATE 2039 DAILY TRAFFIC VOLUMES |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | NO-BUILD | ALTERNATIVE 1 | ALTERNATIVE 2 | ALTERNATIVE 3 |
| $12^{\text {TH }}$ STREET <br> (BELMONT TO MAY) | 13,000 | 10,000 | 13,000 | 6,000 |
| $13^{\text {TH }}$ STREET <br> (MAY TO BELMONT) | 13,000 | 16,000 | 13,000 | 20,000 |
| MAY STREET $\left(12^{\mathrm{TH}} \mathrm{TO} 13^{\mathrm{TH}}\right)$ | 9,500 | 6,500 | 11,000 | 8,000 |

## INTERSECTION PERFORMANCE EVALUATION

Intersection operations were analyzed in Synchro/SimTraffic software and PTV Vistro 2021 using Highway Capacity Manual $6^{\text {th }}$ Edition methodology to understand the impact of the various alternatives. Performance measures used for this analysis include volume-to-capacity (v/c) ratios, seconds of control delay, and levels of service (LOS). Intersection operations and queueing reports are included in Appendix B to E. Table 2 lists the intersection operations for each alternative, as well as the TSP Build alternative, which maintains the existing traffic circulation and lane configuration but adds a traffic signal at $13^{\text {th }}$ Street/May Street and $13^{\text {th }}$ Street/Belmont Avenue. Both roundabouts and traffic signals were tested at the major intersections for each of the alternatives, as specific intersection control is not necessarily a requirement of the broader circulation changes and active transportation improvements identified in each alternative.
$13^{\text {th }}$ Street, $12^{\text {th }}$ Street, and May Street between $12^{\text {th }}$ and $13^{\text {th }}$ Streets are under the jurisdiction of the Oregon Department of Transportation (ODOT) ${ }^{3}$, while all other streets analyzed in this study are under the jurisdiction of the City of Hood River. For the ODOT roadways, the adopted mobility target is a $\mathrm{v} / \mathrm{c}$ ratio at or below $0.95^{4}$. For all other roadways, the City of Hood River's adopted mobility standard is LOS D or better.

While ODOT's adopted mobility target ( $\mathrm{v} / \mathrm{c} \leq 0.95$ ) already allows for a considerable amount of congestion, ODOT would allow more ( $\mathrm{v} / \mathrm{c} \leq 1.0$ ) if this area were designated as a Special Transportation Area. Special Transportation Areas are intended to be areas with compact, mixeduse development and well-developed transit, bicycle, and pedestrian facilities, which aligns with the vision for the Heights. Therefore, for planning purposes, a maximum v/c ratio threshold of 1.0 will be used to indicate when there is too much congestion at intersections. Similarly a LOS F condition

[^2]will be used to identify areas where delays would be excessively long, even where $\mathrm{v} / \mathrm{c}$ ratios are less than 1.0.

As presented in Table 2, there are areas in each alternative where mobility deficiencies exist. The TSP Build alternative performs the best at the major bottlenecks at $13^{\text {th }}$ Street/May Street and $13^{\text {th }}$ Street/Belmont Avenue, as there are two southbound through lanes and no conflicting northbound traffic. Without additional capacity enhancements, neither roundabouts nor signalized intersections are able to serve the expected demand at those intersections in any of the alternatives, with $\mathrm{v} / \mathrm{c}$ ratios above 1.0 (with the exception of a signalized intersection at $13^{\text {th }}$ Street/Belmont Avenue in Alternative 3). $12^{\text {th }}$ Street/May Street operates well below capacity, regardless of alternative.

| STUDY INTERSECTION | TSP BuILd |  |  | Alternative 1 |  |  | Alternative 2 |  |  | ALTERNATIVE 3 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Los | delay | v/c | Los | Delay | v/c | Los | delay | v/c | Los | Delay | v/c |
| SIGNALIZED |  |  |  |  |  |  |  |  |  |  |  |  |
| $13^{\text {TH }}$ STREET / MAY STREET | c | 31 | 0.96 | D | 36 | 1.11 | F | 96 | 1.47 | D | 37 | 1.12 |
| $12^{\text {th }}$ STREET / MAY STREET | c | 23 | 0.62 | c | 27 | 0.66 | D | 41 | 0.76 | c | 20 | 0.32 |
| $13^{\text {TH }}$ StREET / BELMONT AVE | A | 9 | 0.71 | D | 35 | 1.55 | N/A | N/A | N/A | c | 26 | 0.92 |
| ROUNDABOUT |  |  |  |  |  |  |  |  |  |  |  |  |
| $13^{\text {TH }}$ STREET / MAY STREET | N/A | N/A | N/A | E | 50 | 1.14 | E | 45 | 1.09 | F | 92 | 1.25 |
| $13^{\text {TH }}$ STREET / BELMONT AVE | N/A | N/A | N/A | E | 47 | 1.09 | N/A | N/A | N/A | F | 59 | 1.12 |
| $13^{\text {TH }}$ STREET $/ \mathbf{1 2}^{\text {TH }}$ STREET $/$ BELMONT AVE | N/A | N/A | N/A | N/A | N/A | N/A | F | 94 | 1.20 | N/A | N/A | N/A |
| TWO-WAY STOP-CONTROLLED |  |  |  |  |  |  |  |  |  |  |  |  |
| $13^{\text {TH }}$ STREET / TAYLOR AVE | A/F | 7/400 | 0.56/1.68 | B/F | 11/73 | 0.42/0.62 | A/F | 7/135 | 0.73/0.99 | B/F | 12/291 | 0.54/1.21 |
| $13^{\text {TH }}$ StREET / A StREET | A/F | 7/246 | 0.61/1.24 | B/F | 11/208 | 0.38/0.99 | A/F | 7/84 | 0.75/0.66 | B/F | 11/642 | 0.56/1.89 |
| $12^{\text {TH }}$ STREET / TAYLOR AVE | A/F | 8/58 | 0.72/0.48 | A/C | 8/17 | 0.53/0.18 | A/F | 8/134 | 0.86/0.71 | A/C | 7/15 | 0.36/0.06 |
| $12^{\text {Th }}$ Street / Pine Street | A/F | 0/80 | 0.63/0.86 | B/D | 10/27 | 0.16/0.40 | A/F | 0/76 | 0.81/0.79 | A/B | 0/14 | 0.34/0.22 |
| $12^{\text {Th }}$ Street / wilson Street | A/F | 7/368 | 0.65/1.40 | A/D | 10/30 | 0.15/0.19 | A/F | 7/138 | 0.79/0.80 | A/C | 7/15 | 0.32/0.07 |
| $12^{\text {TH }}$ StREET / UNION STREET | A/F | 8/1214 | 0.68/3.40 | A/E | 10/48 | 0.14/0.49 | N/A | N/A | N/A | A/C | 7/18 | 0.34/0.21 |
| $13^{\text {TH }}$ STREET $/ 12{ }^{\text {TH }}$ StREET | N/A | N/A | N/A | -/D | -/26 | -/0.56 | N/A | N/A | N/A | N/A | N/A | N/A |

Bold and red indicates a "failing" condition, which could be a v/c ratio of 1.0 or greater or a LOS F.
For two-way stop-controlled intersections, results are shown for the major street/minor street approaches with the most congestion, where the minor street would be stop-controlled.

Key findings for the major intersections (as currently drawn in the concepts and without any additional mitigations) are discussed below:

## - $13^{\text {th }}$ Street/May Street

- This intersection functions well under the TSP Build scenario. It would feel somewhat congested, but not excessively.
- A single lane roundabout at this location is not expected to perform well, with the southbound approach operating over capacity in each of the three alternatives (ranging from a v/c of 1.09 to 1.25 ). Southbound queues would be expected to extend to Eugene Street. In Alternative 3, the westbound approach is also over capacity and would need further mitigation.
- A traffic signal at this intersection is not expected to perform well under either Alternative 1, 2 , or 3 as designed in the original concept. In particular, a single shared southbound lane is shown in each of the alternatives, which significantly increases queueing and delay on the southbound approach.
- $13^{\text {th }}$ Street/Belmont Avenue

This intersection would operate very well under the TSP Build scenario.

- A single lane roundabout would be unable to serve the demand at this intersection, with the southbound approach experiencing significant delay and queues expected to extend beyond C Street.
- A traffic signal at this intersection is not expected to perform well in Alternative 1 with an expected intersection $\mathrm{v} / \mathrm{c}$ ratio of 1.55 . However, when a southbound left turn lane is added in Alternative 3, the intersection v/c ratio is significantly improved and operates below capacity.

The "dog bone" roundabout at $12^{\text {th }}$ Street $/ 13^{\text {th }}$ Street/Belmont Avenue (shown in Alternative 2) also would not perform well with only a single lane to serve demand at the northbound and southbound approaches. The resulting vehicle queues on those approaches would be very long.

- $12^{\text {th }}$ Street/May Street
- The signalized intersection generally performs well under all alternatives, with a v/c ratio well below 1.0.
- Under Alternative 2, there is only a single westbound through lane between the north and south leg of the intersection, which provides limited storage space and causes queue spillback on the southbound and westbound legs of the intersection.
- Two-way stop-controlled intersections
- In general, many future two-way stop-controlled intersections operate with significant sidestreet delay, regardless of alternatives.
- Side street delay is higher on $12^{\text {th }}$ Street in Alternative 2 as there is significant northbound volume in a single through lane, leading to fewer gaps for side street vehicles to turn onto $12^{\text {th }}$ Street.
- Alternatives 1 and 3 experience less side street delay than the TSP Build scenario, with Alternative 1 having slightly better performance overall, especially on $13^{\text {th }}$ Street.
- The southbound connection from $12^{\text {th }}$ Street to $13^{\text {th }}$ Street in Alternative 2 is expected to function well as the southbound traffic only yields to a single northbound lane prior to turning into an added southbound lane shadowed by the pedestrian refuge island.


## ALTERNATIVE MITIGATION

The key to identifying what aspects of which streetscape alternative work best and which have areas for improvement relies on looking closely at "bottleneck" intersections. To do this, an alternative-by-alternative analysis is performed, and reasonable mitigation measures are implemented to improve mobility while taking into account right-of-way limitations, topography, and the inclusion of improved pedestrian and bicycle facilities included in each alternative. The two main bottleneck intersections evaluated for mitigations for each alternative are $13^{\text {th }}$ Street/May Street and $13^{\text {th }}$ Street/Belmont Avenue. Table 3 summarizes the operational results for the proposed mitigations, described in more detail below.

## 13 ${ }^{\text {th }}$ Street/May Street

- A traffic signal at this intersection should include the addition of a dedicated southbound left turn lane8. This addition could be difficult due to topographical concerns in the northwest corner and right-of-way limitations with the hospital parking lot in the northeast corner of the intersection.
- A traffic signal is not expected to perform well in Alternative 2 without significant mitigation, such as converting May Street between $12^{\text {th }}$ Street and $13^{\text {th }}$ Street to westbound only and adding extra turn lanes (which would have a significant impact on connectivity in the area and to the hospital and the ability to maintain the pedestrian and cyclist improvements shown in Alternative 2 on May Street) or adding a second southbound through lane (which is inconsistent with the rest of the alternative, which includes a single southbound lane on $13^{\text {th }}$ Street).
- A roundabout at this intersection should include an additional southbound through lane, making the roundabout a partial multilane roundabout. This mitigation would greatly increase the footprint of the intersection, have large impacts to adjacent properties and significantly increase costs (see concept drawing in Appendix F). Due to the circulation changes associated with Alternative 3, a westbound right turn slip lane would also be required to reduce to the westbound $\mathrm{v} / \mathrm{c}$ ratio below 1.0.


## $13^{\text {th }}$ Street/Belmont Avenue

- A traffic signal at this intersection could include varying levels of mitigations, depending on the alternative.
- For the alternatives with two-way traffic on $13^{\text {th }}$ Street (Alternatives 1 and 3), the following mitigations should be included to reduce southbound queueing and reduce the potential for queue spillback between $12^{\text {th }}$ Street and $13^{\text {th }}$ Street on Belmont Avenue:
> Add a southbound left turn lane (already included in Alternative 3).
> Close the northbound left turn, rerouting traffic along $12^{\text {th }}$ Street to Belmont Avenue to become a westbound through movement instead.
> Close the westbound left turn. The vehicle rerouting caused by this mitigation would be more easily accommodated in Alternative 1 as $12^{\text {th }}$ Street connects directly to southbound $12^{\text {th }}$ Street at the south end of the couplet.
- For Alternative 2 with one-way traffic on $13^{\text {th }}$ Street, dual southbound through lanes would be necessary at the intersection with a traffic signal (similar to what exists today) and an eastbound right turn lane would be needed to reduce excessive queueing eastbound. The dual southbound through lanes would minimally need to extend the block between A Street and Belmont Avenue.
- A roundabout at this intersection would function best with dual southbound through lanes, regardless of if the roundabout is a dog bone style, such as the one shown in Alternative 2 or a standard roundabout.
- Even with dual southbound lanes approaching the roundabout, in Alternative 2 with the dog bone configuration, the northbound approach v/c would be 1.07, as shown in Table 3 below. To mitigate the northbound approach $\mathrm{v} / \mathrm{c}$, a second northbound through lane would need to be carried through the roundabout before being dropped as a turn lane at A Street or B Street.

In Alternative 1, instead of dual southbound through lanes, Belmont Avenue could be converted to eastbound only (i.e., only a roundabout exit) to reduce the southbound v/c ratio just below 1.0 as shown in Table 3.

## TABLE 3: MITIGATED INTERSECTION OPERATIONAL RESULTS (2039 WEEKDAY PM PEAK HOUR)

| STUDY <br> INTERSECTION | ALTERNATIVE 1 |  |  | ALTERNATIVE 2 |  |  | ALTERNATIVE 3 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | LOS | DELAY | v/C | Los | DELAY | V/C | LOS | DELAY | V/C |
| SIGNALIZED |  |  |  |  |  |  |  |  |  |
| $13^{\text {TH }}$ STREET / <br> MAY STREET | C | 29 | 0.92 | D | 38 | 0.71 | C | 30 | 0.92 |
| $13^{\text {TH }}$ STREET / BELMONT AVE | C | 20 | 0.80 | A | 9 | 0.68 | C | 23 | 0.83 |
| ROUNDABOUT |  |  |  |  |  |  |  |  |  |
| $13^{\text {TH }}$ STREET / MAY STREET | C | 17 | 0.83 | C | 17 | 0.87 | C | 18 | 0.86 |
| $13^{\text {TH }}$ STREET / BELMONT AVE | D | 33 | 0.97 | N/A | N/A | N/A | D | 27 | 0.97 |
| $13^{\text {TH }}$ STREET / <br> $12^{\text {TH }}$ STREET / <br> BELMONT AVE | N/A | N/A | N/A | D | 32 | 1.07 | N/A | N/A | N/A |

Bold and red indicates a "failing" condition, which could be a v/c ratio of 1.0 or greater or a LOS F.
For two-way stop-controlled intersections, results are shown for the major street/minor street approaches with the most congestion, where the minor street would be stop-controlled.

With the mitigations listed above, intersection operations can be significantly improved compared to the original concept drawings. However, each of the mitigations come with various tradeoffs related to property impacts, costs, and impacts to other modes of travel. These tradeoffs will need to be weighed before deciding on a preferred concept. In general, the following summarizes the operational performance of each alternative:

- Alternative 1 performs the best between alternatives, as two-way traffic allows the demand to spread across both $12^{\text {th }}$ and $13^{\text {th }}$ Street. With mitigation, there would still be significant queueing southbound, with $95^{\text {th }}$ percentile queues ${ }^{5}$ extending from Belmont Avenue nearly to May Street.
- Alternative $\mathbf{2}$ is expected to perform poorly, even with mitigation, as there is only a single northbound and southbound through lane to serve the traffic demand, resulting in significant queueing and spillback between intersections, particularly at $13^{\text {th }}$ Street/May Street
- Alternative 3 performs slightly better than Alternative 2, but since there is still only a single southbound through lane to serve the demand, it does not perform as well as Alternative 1, and experiences significant southbound queue spillback on $13^{\text {th }}$ Street.


## SIDE STREET DELAY

Side street delay (i.e., how long it takes to turn onto $12^{\text {th }}$ and $13^{\text {th }}$ Streets from stop-controlled side streets) is another performance measure used to describe levels of congestion associated with each alternative. Based on the performance listed in Table 2, the following summarizes key findings related to side street delay.

- Overall, side street delay is the lowest on Alternative 1 with moderate delays on $13^{\text {th }}$ Street and low delays on $12^{\text {th }}$ Street.
- Side street delay is generally the worst with Alternative 2 . The is especially true along $12^{\text {th }}$ Street, where there is significant northbound volume in a single through lane leading to fewer gaps for side street vehicles to turn onto 12th Street.
- With Alternative 3, side street delay on $13^{\text {th }}$ Street is significant, as $13^{\text {th }}$ Street is serving far more traffic than under the other alternatives and the street crossing is wider. However, side street delays on $12^{\text {th }}$ Street are low.


## TRAVEL TIME

Travel time is a practical measure of mobility that can help to contextualize the performance of a system and can be used to make high-level comparisons between alternatives. For the Hood River Heights, travel time from the north end of the area (12th or 13th Street bounded by May Street) and the south end of the area (where the couplet converges) is of particular importance for local and regional connectivity.

The change in travel time for each alternative with the traffic signal mitigations relative to the TSP Build scenario is shown below in Table 4. Tavel times were calculated using SimTraffic software for comparison purposes only between scenarios, as this model was not calibrated to existing conditions travel times.

Alternative 1 experiences reasonable increases in travel times compared to the TSP Build scenario, with about 30 seconds or fewer of added time in either direction. Travel times under Alternative 2 increase significantly, taking more than 90 seconds longer to travel southbound ( $13^{\text {th }}$ Street) and 60 seconds longer to travel northbound ( $12^{\text {th }}$ Street). Southbound travel times under Alternative 3

[^3]also take about 90 seconds longer ( $13^{\text {th }}$ Street) but northbound travel times (also $13^{\text {th }}$ Street) are reasonable and increase by less than 30 seconds.

TABLE 4. TRAVEL TIMES ALONG $12^{\text {TH }}$ AND $13^{\text {TH }}$ STREETS

| DIRECTION | STREET | CHANGE IN TRAVEL TIME RELATIVE TO TSP BUILD SCENARIO (SECONDS / PERCENT CHANGE) |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | ALTERNATIVE 1 W/ SIGNAL MITIGATIONS | ALTERNATIVE 2 W/ SIGNAL MITIGATIONS | ALTERNATIVE 3 W/ SIGNAL MITIGATIONS |
| NORTHBOUND <br> (SOUTH COUPLET END TO MAY ST) | $12^{\text {th }}$ Street | + 33s / 43\% | + 60s / 78\% | + 63s / 82\% |
|  | $13^{\text {th }}$ Street | + 18s / 23\% | - | + 23s / 30\% |
| SOUTHBOUND <br> (MAY ST TO SOUTH COUPLET END) | $12^{\text {th }}$ Street | - 100s / - $57 \%$ A | - | - |
|  | $13^{\text {th }}$ Street | + 35s / 20\% | + 95s / 54\% | + 90s / 51\% |
| ${ }^{\text {a }}$ Southbound travel time in Alternative 1 on $12^{\text {th }}$ Street is compared to the TSP Build southbound travel time on $13^{\text {th }}$ Street. The Alternative 1 travel time does not include any signal delay at May Street/ $12^{\text {th }}$ Street while the TSP Build southbound travel time on $13^{\text {th }}$ Street does include the signal delay at May Street $/ 13^{\text {th }}$ Street, making it appear as if there is a decrease in travel time. |  |  |  |  |

## TRUCK ACCESIBILITY AND EMERGENCY SERVICE NEEDS

Given the location of the hospital on the north end of the couplet, it is critical that emergency vehicles can easily pass through this corridor. Alternatives that include multiple travel lanes on each street provide more opportunities for emergency vehicles to pass around stopped traffic. In addition, the presence of parallel parking may provide more space for vehicles to pull over, as long as there are a sufficient number of empty spaces. Parallel parking also provides opportunities for loading zones, so parallel parking in close proximity to businesses would be beneficial for delivery truck access.

With multiple travel lanes on both $13^{\text {th }}$ and $12^{\text {th }}$ Streets, Alternative 1 provides opportunities for emergency vehicles to pass around stopped traffic. The parallel parking on $12^{\text {th }}$ Street may make this easier at times and also creates opportunities for truck loading zones. With only single travel lanes on both $13^{\text {th }}$ and $12^{\text {th }}$ Streets, emergency vehicle access could be restricted under Alternative 2 , though the parallel parking may create opportunities if empty. Having parallel parking on both streets under Alternative 2 creates many opportunities for loading zones close to businesses. $13^{\text {th }}$ Street may be the most accessible for emergency vehicles under Alternative 3, but $12^{\text {th }}$ Street could be the most restricted. Loading zones could be located on one side of $13^{\text {th }}$ Street, but may not be possible on $12^{\text {th }}$ Street without losing many parking spaces.

One freight concern identified along $13^{\text {th }}$ Street is the ability for trucks to travel up the hill just north of May Street, particularly during icy conditions. If a roundabout was installed at that intersection instead of a traffic signal, it could provide an opportunity for trucks to continue with less stopping (as roundabouts often have rolling queues). Trucks would occasionally have to stop on the hill if a traffic signal was installed, although a technology application that detects oncoming
trucks and extends the signal green time could be used to reduce the need to stop during inclement weather.

Consideration will need to be given to intersections where truck turning needs are more common when designing and locating curb extensions. Even with reduced size curb extensions, larger trucks may be required to encroach upon adjacent lanes when making turns. Alternatives with wider space between curbs typically allows for trucks to more easily make turns.

## IMPACTS ON PROPERTY ACCESS

Each alternative may have different levels of impact to property access. While much won't be known until a project advances to engineering design, at the concept level it is assumed that most impacts to property access would occur from: 1) the need for additional right-of-way to build wider streets and intersections and 2) changes to street designs that could make direct connections for driveways infeasible or undesirable.

The conceptual improvements under consideration generally maintain existing right-of-way widths along street corridors, but all alternatives will require improvements around the major intersections (primarily $13^{\text {th }}$ Street/May Street and $13^{\text {th }}$ Street/Belmont Avenue) that will need additional right-of-way. At the current level of concept design it is not known if there would be a significant difference in right-of-way needs and associated property access impacts between the alternatives.

However, the alternatives do include fairly different street designs that could impact the ability or desire to have direct driveway connections. The primary street element that could impact property access is the type and design of bicycle facility. The main conflicts between bicycle facilities and driveways include:

- Two-way bicycle facilities and driver expectations - Drivers pulling out of driveways may not expect to have cyclists approaching from both directions when crossing a bicycle facility like a shared use path or two-way cycle track. It is generally preferred to minimize the number of driveway crossings with two-way bicycle facilities for safety reasons, and also to preserve the high level of comfort that these types of facilities are intended to provide for people biking. Where these conflicts cannot be avoided, design treatments can be applied to make drivers aware that they need to look both ways for people biking.
- Off-street bicycle facilities and driveway designs - Because sidewalks are higher than street level, driveways must be designed to comfortably allow vehicles to transition between these high and low points within a relatively short distance. Ideally, the area where the driveway crosses the sidewalk would be level to maintain a comfortable crossing for people with mobility devices. However, maintaining a level sidewalk requires some separation between the sidewalk and street - ideally about five feet. While there are various driveway designs that can accommodate vehicle passage with little to no separation between the sidewalk and street, such designs will include partial to full cross slopes in the sidewalk or require the sidewalk to ramp down and back up across the driveway. These designs are not fatally flawed, but may not provide an ideal walking or biking environment.

In both cases, closing driveways where feasible should be considered to eliminate these conflicts and provide a low-stress bikeway. However, design treatments are possible to mitigate conflicts in lieu of driveway closures.

Alternative 1 includes the most potential conflicts with driveways and new bicycle facilities (about 17 in total). Four of these conflicts are on May Street, but the proposed street design includes the five-foot buffer between the raised bike lane and street needed for a comfortable design. However, there are about 13 driveways on $13^{\text {th }}$ Street and Belmont Avenue where the bicycle facility is anticipated to be next to the curb with very little separation from the street.

Alternative 2 has the fewest potential conflicts with driveways and new bicycle facilities (about 13 in total). Similar to Alternative 1, there are four conflicts on May Street, but the proposed street design includes a sufficient buffer between the raised bike lane and street. Because the bike facility is only on one side of the street, there are only nine conflicts along $13^{\text {th }}$ Street and Belmont Avenue. However, while there may be sufficient space between the bike facility and street, Alternative 2 includes a two-way bikeway that will require special signing and pavement markings to alert drivers.

Alternative 3 includes 12 potential driveway/bike facility conflicts, with seven on $12^{\text {th }}$ Street, three on May Street, and two on Belmont Avenue. A small, three-foot buffer is provided between the bikeway and street, but the two-way bikeways on May Street and $12^{\text {th }}$ Street will require special signing and pavement markings to alert drivers.

## SAFETY

Several factors influence safety along the corridor, as discussed in more detail below.

## Active Transportation

Each of the alternatives are expected to enhance safety for active transportation compared to current conditions. For example, all of the alternatives are expected to add curb extensions and enhance pedestrian crossings to improve safety and visibility of people walking. Each of the alternatives include bike enhancements (bike lanes, cycle tracks or buffered bike lanes) that would improve the safety of people biking.

## Turning Movement Conflicts and Predictable Routing

Alternative 2 is the only alternative that maintains one-way traffic on the couplet. Converting to two-way traffic (like in Alternative 1 and Alternative 3) increases the number of conflicting turning movements. While the higher number of potential conflicts could result in more crashes, it may also have a calming effect on traffic and could result in lower travel speeds that counteract the impact of having more potential conflicts.

Adding left turn lanes and adding protected left turn phasing (such as the ones proposed in the mitigations) could also reduce potential conflicts. Alternative 3 also adds a center left turn lane on $13^{\text {th }}$ Street, providing a space for left turning vehicles to wait for an appropriate gap in conflicting traffic before turning.

In general, Alternatives 1 and 2 provide more predictable routing for drivers who may be unfamiliar with the area. Alternative 3 only includes northbound traffic on $12^{\text {th }}$ Street, which could be confusing to unfamiliar drivers.

## Intersection Control

In general, roundabouts have great potential to reduce the severity of crashes at intersections and have the potential to reduce injury crashes by up to 82 percent $^{6}$ and also reduce vehicle speeds. Traffic signals would improve safety compared to the existing two-way stop-control, but not as greatly as roundabouts. Any alternative could include roundabouts or traffic signals at the major intersections. Therefore, this factor does not help in the selection of a preferred alternative.

TABLE 5. SUMMARY OF PERFORMANCE FOR PEOPLE DRIVING

| PERFORMANCE CRITERIA | $13^{\text {TH }}$ STREET |  |  | $12^{\text {TH }}$ STREET |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ALT 1 | ALT 2 | ALT 3 | ALT 1 | ALT 2 | ALT 3 |
| GOAL 1: CALM TRAFFIC AND IMPROVE INTERSECTIONS TO IMPROVE SAFETY FOR PEOPLE DRIVING WALKING, BIKING, TAKING TRANSIT AND SUPPORTING LOCAL BUSINESSES. |  |  |  |  |  |  |
| INTERSECTION OPERATIONS |  |  |  |  |  |  |
| TRAVEL TIME THROUGH THE HEIGHTS |  | $\vee$ |  |  |  |  |
| SIDE STREET DELAY | $1$ |  |  |  |  |  |
| FIRE/EMERGENCY SERVICE NEEDS |  |  |  |  |  | $\cdots$ |
| TRUCK ACCESSIBILITY |  |  |  |  |  |  |
| SAFETY |  |  |  |  |  | $\hat{N}$ |

GOAL 2: PRESERVE AND PROMOTE A LIVABLE COMMUNITY AND ECONOMY THROUGH STREETSCAPE IMPROVEMENTS THAT INCREASES SAFETY FOR PEOPLE WALKING AND BIKING AND ADDRESSES PARKING NEEDS TO SUPPORT LOCAL BUSINESS ACCESS, AND FUTURE MIXED-USE DEVELOPMENT.

DIVERSION IMPACTS

IMPACTS ON PROPERTY ACCESS


[^4]Today, $12^{\text {th }}$ and $13^{\text {th }}$ Streets are challenging for pedestrians to navigate. The existing two-lane cross section of both busy streets have unmarked crossings, several skewed or offset intersections, and on-street parking with no curb extensions. All of these conditions increase pedestrian exposure, reduce pedestrian visibility, and introduces risk for "double threat" crashes - where a vehicle which has stopped for a pedestrian then blocks that same pedestrian from view of the adjacent travel lane (see Figure 1). Although there are painted "continental" pedestrian crossings at some intersections, these treatments do not warn or control oncoming traffic and there are no pedestrian median refuges in the corridor other than at the intersection of $13^{\text {th }}$ Street and May Street.


FIGURE 1: ILLUSTRATION OF THE "DOUBLE THREAT" RISK

To enhance conditions for people walking on either $12^{\text {th }}$ or $13^{\text {th }}$ Streets, each of the three alternatives contain elements such as additional separation from vehicle traffic (via landscaping or bicycle facilities), wider sidewalks, and signal or roundabout control at the intersections along $13^{\text {th }}$ Street at May Street and Belmont Avenue. While not explicitly shown in the concept drawings, the alternatives are also assumed to include ADA improvements, curb extensions to shorten crossing distances and improve pedestrian visibility, pedestrian-scale lighting, and enhanced crossings that could include treatments such as flashing beacons and pedestrian refuge islands. Appendix $G$ documents analysis for level of pedestrian treatment may be warranted within each alternative.

Corridor conditions for people walking were evaluated for each alternative using the criteria described below. These will be considered alongside additional criteria related to each alternative's ability to complete connections to area destinations that are being evaluated by others. For each alternative, the degree to which the criteria is supported by each of the main corridors along $12^{\text {th }}$ Street and $13^{\text {th }}$ Street has been rated, with brief descriptions provided below and a summary chart provided in Table 6.

- Visibility at crossings was assessed qualitatively by considering factors that could increase pedestrian visibility (e.g., curb extensions or median refuges) and factors that could decrease pedestrian visibility (e.g., landscaping, on-street parking). Each alternative was also evaluated for its ability to reduce the potential risk for "double threat" crashes where a stopped vehicle blocks a crossing pedestrian from view of the adjacent travel lane.


## Alternative 1

$13^{\text {th }}$ Street: No on-street parking improves visibility but pedestrians are still set back from the corner due to the presence of the bicycle facility.
$12^{\text {th }}$ Street: On-street parking is present but it is assumed that curb extensions will be used to enhance visibility. With no bicycle facilities, pedestrians waiting to cross are close to the street and easily within a driver's field of vision.

## Alternative 2

$13^{\text {th }}$ Street: Parked cars with curb extensions on one side, no obstructions on the other side.
$12^{\text {th }}$ Street: Parked cars with curb extensions on both sides.

## Alternative 3

$13^{\text {th }}$ Street: Parked cars with curb extensions on one side, no obstructions on the other side.
$12^{\text {th }}$ Street: Parked cars with curb extensions on one side. On the other side, there are no visibility obstructions but pedestrians are still set back from the corner due to the presence of the bicycle facility.

- Time exposed to vehicular traffic at crossings was assessed by considering factors along $12^{\text {th }}$ and $13^{\text {th }}$ streets such as the number of vehicle lanes to cross as well as curb extensions and pedestrian median refuges, which shorten the pedestrian crossing distance and reduce vehicle exposure.


## Alternative 1

$13^{\text {th }}$ Street: The street crossing is 22 feet wide. The bicycle facilities must also be crossed, adding another 16 feet.
12th Street: The street crossing is 24 feet wide (similar to existing conditions if curb extensions were provided).

## Alternative 2

$13^{\text {th }}$ Street: The street crossing is 12 feet wide, with only one direction of travel to cross.
$12^{\text {th }}$ Street: The street crossing is 12 feet wide, with only one direction of travel to cross

## Alternative 3

$13^{\text {th }}$ Street: If no median refuge islands are provided, this alternative has the widest crossings at 32 feet. If median refuge islands are provided, crossing distances are reduced to about 11 feet (twice).
$12^{\text {th }}$ Street: The street crossing is 12 feet with only one direction of travel to cross. The cycle track crossing is 10 feet.

- Access to low-stress crossings was assessed by considering the total potential number of low-stress, unsignalized pedestrian crossings and the distance between low-stress crossings along the corridor. Providing evenly spaced crossings minimizes out-of-direction travel for pedestrians. The ongoing Hood River Safe Routes to School project identification program has identified key routes along May Street, $12^{\text {th }}$ Street, Taylor Avenue, B Street, Pine Street, A Street, and Wilson Street. To connect these routes, enhanced street crossings are being called for at the following intersections:
$13^{\text {th }}$ Street / May Street
$13^{\text {th }}$ Street / Taylor Avenue
$13^{\text {th }}$ Street / A Street
- $12^{\text {th }}$ Street / May Street
- $12^{\text {th }}$ Street / Taylor Avenue
- $12^{\text {th }}$ Street / Pine Street
- $12^{\text {th }}$ Street / B Street
- $12^{\text {th }}$ Street / Wilson Street

All alternatives can accommodate enhanced crossing improvements at these locations. However, some alternatives may result in lower stress, easier crossings, as noted below.

## Alternative 1

$13^{\text {th }}$ Street: Accommodates enhanced crossings, but the 22 -foot crossing distance will reduce comfort.

12th Street: Accommodates enhanced crossings, but the 24 -foot crossing distance will reduce comfort.

## Alternative 2

$13^{\text {th }}$ Street: Accommodates enhanced crossings and the single-lane crossings will significantly improve comfort.
$12^{\text {th }}$ Street: Accommodates enhanced crossings and the single-lane crossings will significantly improve comfort.

## Alternative 3

$13^{\text {th }}$ Street: Median refuge islands should be provided to create low-stress crossings. This may require prohibiting left turns from 13 Street at alternating intersections (i.e., prohibiting southbound lefts at one intersection and northbound lefts at the next) to create space in the center lane for a refuge island. Where median refuge islands are provided, the ability to cross one lane at a time will improve comfort.
$12^{\text {th }}$ Street: Accommodates enhanced crossings and the single-lane crossings will significantly improve comfort.

- Width of walkways was assessed by simply measuring the width of provided pedestrian facilities and accounting for space shared with street furniture and landscaping zones or people biking. Wider spaces dedicated solely for people walking were rated more highly.


## Alternative 1

$13^{\text {th }}$ Street: 10 feet but includes the furniture/landscaping zone (about the same as the no build condition).

12th Street: 10 feet but includes the furniture/landscaping zone (about the same as the no build condition).

## Alternative 2

$13^{\text {th }}$ Street: 14 feet but shared with people biking on one side, 8 feet on the other side.
$12^{\text {th }}$ Street: 9 feet on one side, 10 feet on the other side.

## Alternative 3

$13^{\text {th }}$ Street: 10 feet but includes the furniture/landscaping zone (about the same as the no build condition).
$12^{\text {th }}$ Street: 10 feet on one side, 8 feet on the other but includes the furniture/landscaping zone.

- Buffer from traffic and bikes was assessed by the horizontal separation from traffic and bikes as well as the presence of any physical barrier such as a curb.


## Alternative 1

$13^{\text {th }}$ Street: Adjacent to raised bike lanes on both sides, which provide a buffer from traffic.
12th Street: Buffered by parking on both sides. Bikes would be in the street.

## Alternative 2

$13^{\text {th }}$ Street: Mixed with bikes on one side. Buffered from traffic by a landscape strip on one side and by parking and a landscape strip on the other.
$12^{\text {th }}$ Street: Buffered by parking and landscaping on both sides. Bikes would be in the street.

## Alternative 3

$13^{\text {th }}$ Street: Buffered by parking on one side but adjacent to the travel lane on the other. Bikes would be in the street.
$12^{\text {th }}$ Street: Buffered by parking on one side. Buffered from traffic on the other side by the cycle track, but would be adjacent to the cycle track (uncertain if any barrier would be present).

TABLE 6. SUMMARY OF PERFORMANCE FOR PEOPLE WALKING


Today, people biking on $13^{\text {th }}, 12^{\text {th }}$, and May Streets, as well as Belmont Avenue, must share a travel lane with motor vehicles, which is a high-stress environment that can limit use to more experienced riders. These conditions create a significant gaps in bicycle facilities that otherwise could facilitate a safe, low-stress, multimodal connections within the corridor to local businesses, nearby schools, recreation, and healthcare. Furthermore, needing to cross two lanes of uncontrolled traffic can be discouraging and with both lanes traveling in the same direction, there is the risk of "double threat" crashes.

To enhance conditions for people biking along the corridor, each of the three alternatives contain:

- Various bicycle facilities along May Street plus Belmont Avenue, and either along $12^{\text {th }}$ or $13^{\text {th }}$ Streets, ranging from traditional bicycle lanes, a raised dedicated cycle track, and a raised shared use path.
- Different bicycle crossing treatments at the ends of the corridor, including use of bicycle traffic signals.
- Improvements for bicycle connectivity, extending facilities the full length of the project corridor with attention to future connections such as to the Indian Creek Trail and other proposed bike lane upgrades to May Street.

Corridor conditions for people biking were evaluated for each alternative using the criteria described below. These will be considered alongside additional criteria related to each alternative's ability to complete connections to area destinations and other planned bike routes and ease of use by riders unfamiliar to the area that are being evaluated by others. For each alternative, the degree to which the criteria is supported by each of the main corridors along 12th Street and 13th Street has been rated, with brief descriptions provided below and a summary chart provided in Table 7.

- Visibility at crossings was assessed based on the type of crossing provided and the type of bicycle facility, such as a two-way cycle track or a separated one-way bicycle lane. Factors that could decrease bicyclist visibility (e.g., landscaping, on-street parking) were also considered, though thoughtful landscaping can restrict vehicle movement while still allowing access for people biking which generally reduces conflicts, increases visibility, and provides safer crossings for bicyclists.


## Alternative 1

$13^{\text {th }}$ Street: No on-street parking improves visibility but crossing cyclists are still set back from the corner due to the presence of the bicycle facility (though they are likely to wait in the bike lane if no oncoming bikes are present).
$12^{\text {th }}$ Street: On-street parking is present but it is assumed that curb extensions will be used to enhance visibility. With no bicycle facilities, cyclists waiting to cross are close to the street and easily within a driver's field of vision.

## Alternative 2

$13^{\text {th }}$ Street: Parked cars with curb extensions on one side, no obstructions on the other side. Drivers may not expect to encounter people biking from both directions along the
shared use path. However, design treatments at street crossings can be applied to improve awareness.
$12^{\text {th }}$ Street: Parked cars with curb extensions on both sides.

## Alternative 3

$13^{\text {th }}$ Street: Parked cars with curb extensions on one side, no obstructions on the other side.
$12^{\text {th }}$ Street: Parked cars with curb extensions on one side. On the other side, there are no visibility obstructions but crossing cyclists are still set back from the corner due to the presence of the bicycle facility (though they are likely to wait in the bike lane if no oncoming bikes are present).

- Access to low-stress crossings was assessed by considering the total potential number of low-stress, unsignalized crossings and the distance between low-stress crossings along the corridor. Providing evenly spaced crossings minimizes out-of-direction travel for people biking. The ongoing Hood River Safe Routes to School project identification program has identified key routes along May Street, $12^{\text {th }}$ Street, Taylor Avenue, B Street, Pine Street, A Street, and Wilson Street (previously mentioned under Conditions for People Walking).

All alternatives can accommodate enhanced crossing improvements at these locations. However, some alternatives may result in lower stress, easier crossings, as noted below.

## Alternative 1

$13^{\text {th }}$ Street: Accommodates enhanced crossings, but the 22 -foot crossing distance will reduce comfort.

12th Street: Accommodates enhanced crossings, but the 24 -foot crossing distance will reduce comfort.

## Alternative 2

$13^{\text {th }}$ Street: Accommodates enhanced crossings and the single-lane crossings will significantly improve comfort.
$12^{\text {th }}$ Street: Accommodates enhanced crossings and the single-lane crossings will significantly improve comfort.

## Alternative 3

$13^{\text {th }}$ Street: Median refuge islands should be provided to create low-stress crossings. This may require prohibiting left turns from 13 Street at alternating intersections (i.e., prohibiting southbound lefts at one intersection and northbound lefts at the next) to create space in the center lane for a refuge island. Where median refuge islands are provided, the ability to cross one lane at a time will improve comfort.
12th Street: Accommodates enhanced crossings and the single-lane crossings will significantly improve comfort.

- Width of bikeways was assessed by simply measuring the width of provided bicycle facilities and accounting for space shared with people walking. Wider spaces dedicated solely for people biking were rated more highly.


## Alternative 1

$13^{\text {th }}$ Street: 8-foot separated bike lanes.
12th Street: No bike facilities are provided on this street.

## Alternative 2

$13^{\text {th }}$ Street: 14 feet on one side but must accommodate both directions of travel and would be shared with people. 8 feet on the other side.
$12^{\text {th }}$ Street: No bike facilities are provided on this street.

## Alternative 3

$13^{\text {th }}$ Street: No bike facilities are provided on this street.
$12^{\text {th }}$ Street: The 10 -foot width of the two-way cycle track is less than the desired 12 -foot width but more than the minimum with of 8 feet for constrained areas.

- Buffer from traffic and pedestrians was assessed by the horizontal separation from traffic and people walking, as well as the presence of any physical barrier such as a curb.


## Alternative 1

$13^{\text {th }}$ Street: The raised bike lanes keep people biking off of the street. The bikeways are adjacent to walkways.

12th Street: No bike facilities are provided on this street.

## Alternative 2

$13^{\text {th }}$ Street: Mixed with people walking on a shared use path.
$12^{\text {th }}$ Street: No bike facilities are provided on this street.

## Alternative 3

$13^{\text {th }}$ Street: No bike facilities are provided on this street.
12th Street: The two-way cycle track is physically separated from traffic and pedestrians.

TABLE 7. SUMMARY OF PERFORMANCE FOR PEOPLE BIKING

| PERFORMANCE CRITERIA | $13^{\text {TH }}$ STREET |  |  | $12^{\text {TH }}$ STREET |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ALT 1 | ALT 2 | ALT 3 | ALT 1 | ALT 2 | ALT 3 |

GOAL 1: CALM TRAFFIC AND IMPROVE INTERSECTIONS TO IMPROVE SAFETY FOR PEOPLE DRIVING, WALKING, BIKING, TAKING TRANSIT AND SUPPORTING LOCAL BUSINESSES.
VISIBILITY AT
CROSSINGS
GOAL 2: PRESERVE AND PROMOTE A LIVABLE COMMUNITY AND ECONOMY THROUGH STREETSCAPE
IMPROVEMENTS THAT INCREASES SAFETY FOR PEOPLE WALKING AND BIKING AND ADDRESSES
PARKING NEEDS TO SUPPORT LOCAL BUSINESS ACCESS, AND FUTURE MIXED-USE DEVELOPMENT.

```
ACCESS TO LOW-STRESS
CROSSINGS
```

GOAL 4: CREATE STREETS AND GATHERING SPACES THAT PROVIDE SAFE, COMFORTABLE PLACES FOR PEOPLE WALKING, ACCESSING TRANSIT, AND BIKING ALONG AND ACROSS THE CORRIDOR AND THAT CONNECTS AREA RECREATION AND COMMERCIAL DESTINATIONS AND NEIGHBORHOODS.

| WIDTH OF BIKEWAYS | NA | $N A$ | $N A$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| BUFFER FROM TRAFFIC <br> AND PEDESTRIANS | N | $N$ | $N A$ | $N A$ |

## CONDITONS FOR PEOPLE USING TRANSIT

There are currently no transit stops in the Heights District, though Columbia Area Transit (CAT) has expressed interest in establishing stops in this area in the future. The project team has coordinated with CAT to identify potential future stops along $12^{\text {th }}$ and $13^{\text {th }}$ Streets. Specific locations of interest vary by alternative and could include (note, this does not include stops outside of the project area, such as north of May Street):

## Alternative 1

$13^{\text {th }}$ Street: No stops proposed; assumes buses would operate along $12^{\text {th }}$ Street.
$12^{\text {th }}$ Street: Northbound, north of June Street; Southbound, north of A Street or south of Belmont Avenue.

## Alternative 2

$13^{\text {th }}$ Street: Southbound, north of A Street
$12^{\text {th }}$ Street: Northbound, north of June Street

## Alternative 3

$13^{\text {th }}$ Street: Southbound, north of A Street; Northbound, north of Taylor Street (OR the northbound stop on $12^{\text {th }}$ Street)
$12^{\text {th }}$ Street: Northbound, north of June Street (OR the northbound stop on $13^{\text {th }}$ Street)

The accessibility of each of the stops (given the proximity to enhanced pedestrian crossings proposed by the Safe Routes to School program) is summarized below:

- All proposed bus stops along $13^{\text {th }}$ Street (Alternatives 2 and 3) would be sited near enhanced crossings proposed by the Safe Routes to School program.
- The proposed stop on $12^{\text {th }}$ Street north of June Street in all alternatives would not be located adjacent to an enhanced crossing already proposed by the Safe Routes to School program, but would be within one block of the signalized crossing at May Street and just over a block from the proposed crossing at Taylor Avenue.
- The proposed stop on $12^{\text {th }}$ Street at A Street (Alternative 1) would align with a proposed enhanced crossing.
- The proposed stop on $12^{\text {th }}$ Street south of Belmont Avenue (Alternative 1) would be more than a block from the proposed enhanced crossing at A Street.

The ability to accommodate transit amenities at the proposed bus stops is primarily driven by two factors: the presence of a raised bicycle lane or cycle track that would conflict with any transit stops and the width of sidewalk, buffer, and parking lanes (space which could be used for transit amenities). Alternative 3 includes a cycle track on the east side of 12 th Street, which would need to be designed to minimize conflicts with a proposed bus stop on 12th Street.

To allow for transit shelters, a minimum of 10 feet is needed (four-foot shelter, five-foot clear zone and one-foot buffer to the curb), although a wider clear zone of eight-feet and buffer to the curb of 18 inches are generally preferred ${ }^{7}$. All of the alternatives can accommodate the minimum width for a shelter, with Alternative 2 providing the most potential space for amenities.

Table 8 summarizes the performance of the alternatives for people using transit based on the accessibility of transit stops and the ability to accommodate transit amenities.

[^5]TABLE 8. SUMMARY OF PERFORMANCE FOR PEOPLE USING TRANSIT

| PERFORMANCE CRITERIA | $13^{\text {TH }}$ STREET |  |  | $12^{\text {TH }}$ STREET |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ALT 1 | ALT 2 | ALT 3 | ALT 1 | ALT 2 | ALT 3 |
| GOAL 4: CREATE STREETS AND GATHERING SPACES THAT PROVIDE SAFE, COMFORTABLE PLACES FOR PEOPLE WALKING, ACCESSING TRANSIT, AND BIKING ALONG AND ACROSS THE CORRIDOR AND THAT CONNECTS AREA RECREATION AND COMMERCIAL DESTINATIONS AND NEIGHBORHOODS. |  |  |  |  |  |  |
| STOP ACCESSIBILITY PROXIMITY TO ENHANCED CROSSINGS |  |  |  |  |  |  |
| ABILITY TO <br> ACCOMMODATE <br> AMENITIES AT STOPS |  |  |  |  |  |  |

## SUMMARY OF FINDINGS

This section provides a summary of the key findings for the major modes of travel evaluated.

## CONDITIONS FOR PEOPLE DRIVING

- The $12^{\text {th }}$ Street/ $13^{\text {th }}$ Street corridor is forecast to serve about 26,000 vehicle trips per day by 2039 (it serves about 20,000 today). As this area becomes congested there may be some diversion of traffic to other routes but such diversion is expected to be minimal because regional and local street connectivity is limited.
- Overall, Alternative 1 performs the best for people driving as two-way traffic allows the demand to spread across both $12^{\text {th }}$ and $13^{\text {th }}$ Streets. As a result, Alternative 1 will provide the least amount of congestion at the key bottleneck intersections, will have the least amount of side street delay for drivers turning onto $12^{\text {th }}$ and $13^{\text {th }}$ Streets, will result in the least amount of added travel time to drive through the Heights, and would experience the shortest vehicle queues.
- Alternative 3 performs better than Alternative 2, but since there is still only a single southbound through lane to serve the demand, it does not perform as well as Alternative 1. While Alternative 3 can provide comparable levels of congestion relief at the key bottleneck intersections, side street delay for drivers turning onto $13^{\text {th }}$ Street will be much longer, southbound travel times through the Heights will be about one minute longer, and vehicle queues will extend farther.
- Alternative 2 is expected to perform poorly as there is only a single northbound and southbound through lane to serve the traffic demand, resulting in significant queueing and spillback between intersections, particularly at $13^{\text {th }}$ Street/May Street. This alternative is expected to have the worst side street delay for drivers turning onto $12^{\text {th }}$ and $13^{\text {th }}$ Streets and the longest travel times through the Heights.
- Roundabouts can provide good congestion relief at the key bottleneck intersections on $13^{\text {th }}$ Street at May Street and Belmont Avenue but are expected to have greater right-of-way impacts than traffic signals would at those same locations.
- Alternative 1 provides opportunities for emergency vehicles to pass around stopped traffic on both 12th and 13th Streets, with multiple travel lanes on each.
- With only single travel lanes on both $13^{\text {th }}$ and $12^{\text {th }}$ Streets, emergency vehicle access could be restricted under Alternative 2, though the parallel parking may create opportunities for bypassing traffic, if empty.
- $13^{\text {th }}$ Street may be the most accessible for emergency vehicles under Alternative 3 , but $12^{\text {th }}$ Street could be the most restricted.
- Under Alternative 1, the lack of parking on $13^{\text {th }}$ Street will place loading zones farther from businesses.
- Having parallel parking on both streets under Alternative 2 creates good opportunities for loading zones close to businesses.
- Loading zones in Alternative 3 could be located on one side of $13^{\text {th }}$ Street but may not be possible on $12^{\text {th }}$ Street without losing many parking spaces.


## CONDITIONS FOR PEOPLE WALKING

- All alternatives can be designed to provide good visibility of pedestrians at street crossings and will eliminate the "double threat" environment currently present with two lanes of one-way traffic on each street.
- Alternative 2 mixes people walking with people biking on a shared-use path along $13^{\text {th }}$ Street, which may be less comfortable than having a separate, designated space.
- There are many opportunities to provide enhanced, low-stress street crossings on $12^{\text {th }}$ and $13^{\text {th }}$ Streets under all alternatives.
- Alternative 2 significantly reduces street crossing times and exposure to traffic with only one lane of one-way traffic on each street.
- Alternative 1 may provide the longest street crossings on $12^{\text {th }}$ and $13^{\text {th }}$ Streets, with exposure to traffic approaching from two directions.


## CONDITIONS FOR PEOPLE BIKING

- All alternatives can be designed to provide good visibility of people biking at street crossings and will eliminate the "double threat" environment currently present with two lanes of one-way traffic on each street.
- Alternative 2 mixes people walking with people biking on a shared-use path along $13^{\text {th }}$ Street, which may be less comfortable and efficient than having a separate, designated space.
- There are many opportunities to provide enhanced, low-stress street crossings on $12^{\text {th }}$ and $13^{\text {th }}$ Streets under all alternatives.
- Under Alternative 3, the 10 -foot width of the two-way cycle track on $12^{\text {th }}$ Street is less than the desired 12 -foot width but more than the minimum width of 8 feet for constrained areas.
- Drivers may not expect to encounter people biking from both directions when crossing two-way bikeways, such as those in Alternatives 2 and 3. This can be a safety concern, but appropriate design treatments can be applied to improve driver awareness and cyclist visibility.


## CONDITIONS FOR PEOPLE USING TRANSIT

- The locations of nearly all proposed future bus stops align well with proposed low-stress street crossings with the exception of the bus stop on $12^{\text {th }}$ Street south of Belmont Avenue (Alternative 1) would be more than a block from the proposed enhanced crossing at A Street.
- It is anticipated that all alternatives could accommodate bus stops where proposed, however, the cycle track on the east side of $12^{\text {th }}$ Street in Alternative 3 presents conflicts that must be addressed.


## APPENDIX

- Appendix A - Alternative Concept Drawings
- Appendix B - TSP Build Traffic Operations
- Appendix C - Alternative Traffic Operations (Unmitigated)
- Appendix D - Alternative Traffic Operations (Mitigated)
- Appendix E - SimTraffic Reports
- Appendix F - Mitigated Roundabout Concept at May Street/13 ${ }^{\text {th }}$ Street
- Appendix G - NCHRP 562 Pedestrian Crossing Treatment

APPENDIX A: ALTERNATIVE CONCEPT DRAWINGS


13th STREET "MOBILITY STREET"

(50' R/W + [2] $5^{\prime}$ Utility Easements)
EXAMPLE OF RAISED SEPARATED BIKE LANE - 13TH STREET


12th STREET "MAIN STREET WITH PARKING"

[60'R/W)

MAY STREET

( $60^{\prime}$ R/W $+10^{\prime}$ Easement)
EXAMPLE O F RAISED SEPARATED BIIE LANE-MAY STREET


October 2021

STREETSCAPE PLAN


| ーニ R Rightof Way | 1. Limits of sidewalk extend to R/W or existing |
| :---: | :---: |
| - Parcel Lines | back of walk, whichever is further. |
| Roodway | 2. Trees to be located in a later design phase. |
| Sidewalk | 3. Existing driveway locations are not shown and |
| - Planting | will be incorporated in a later design phase. |
| Bike Lane |  |




| LEGEND |
| :---: |
| ー こ Rightof Way |
| $\square$ Parcel Lines |
| - Roodway |
| Sidewalk |
| - Planting |
| Bike Lane |
| NOTES |
| 1. Limits of sidewalk extend to $\mathrm{R} / \mathrm{W}$ or existing back of walk, whichever is further. |
| 2. Trees to be located in 0 later design phase |
| 3. Existing driveway locations |
| are not shown and will |
| be incorporated in a later |
| design phase. |



13th STREET "GREENSTREET"

(50 R R/W + [2] $5^{\prime}$ Utility Easements) EXAMPLE OF SHARED USE PATH-13TH STREET


12th STREET "PARKING STREET"


MAY STREET

[ $60^{\prime} \mathrm{R} / \mathrm{W}+10^{\prime}$ Easement)
example of ralsed vegetation separated bike lane-may street




## ROUNDABOUT DISCUSSION

1. The design shown for the double roundabout is conceptual and should only be considered an illustration of potentiol traffic flow. The actual extents of the roundabout design and potential property impacts will be refined if fecommended as part of a refined concept and troffic analysis,




STREETSCAPE PLAN


APPENDIX B: TSP BUILD TRAFFIC OPERATIONS

c Critical Lane Group


## Notes

Unsignalized Delay for [WBR] is excluded from calculations of the approach delay and intersection delay.

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  |  |  |  | * $\uparrow$ |  |  |
| Traffic Vol, veh/h | 0 | 8 | 8 | 112 | 38 | 0 | 0 | 0 | 0 | 14 | 1130 | 13 |  |
| Future Vol, veh/h | 0 | 8 | 8 | 112 | 38 | 0 | 0 | 0 | 0 | 14 | 1130 | 13 |  |
| Conflicting Peds, \#hr | 8 | 0 | 11 | 11 | 0 | 8 | 5 | 0 | 2 | 2 | 0 | 5 |  |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | - | - | - | - | - |  | - | - | - | - |  |
| Veh in Median Storage, \# | \# - | 0 | - | - | 0 | - | - | - | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |  |
| Mvmt Flow | 0 | 9 | 9 | 122 | 41 | 0 | 0 | 0 | 0 | 15 | 1228 | 14 |  |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 3.4 |  |  |  |  |  |  |  |  |  |  |  |
| Movement E | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  |  |  |  | * $\uparrow$ |  |
| Traffic Vol, veh/h | 0 | 10 | 5 | 77 | 16 | 0 | 0 | 0 | 0 | 55 | 1195 | 10 |
| Future Vol, veh/h | 0 | 10 | 5 | 77 | 16 | 0 | 0 | 0 | 0 | 55 | 1195 | 10 |
| Conflicting Peds, \#/hr | 8 | 0 | 4 | 4 | 0 | 8 | 3 | 0 | 7 | 7 | 0 | 3 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | - | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| Mvmt Flow | 0 | 11 | 5 | 81 | 17 | 0 | 0 | 0 | 0 | 58 | 1258 | 11 |








| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |






| Movement E | EBT | EBR | WBL | WBT | NBL | NBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | $\uparrow$ |  |  | 个 $\uparrow$ | \% | F |
| Traffic Volume (veh/h) 1 | 112 | 0 | 0 | 404 | 634 | 642 |
| Future Volume (veh/h) 1 | 112 | 0 | 0 | 404 | 634 | 642 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) |  | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No | No |  |
| Adj Sat Flow, veh/h/ln 18 | 1870 | 0 | 0 | 1900 | 1885 | 1885 |
| Adj Flow Rate, veh/h 12 | 123 | 0 | 0 | 444 | 697 | 705 |
| Peak Hour Factor 0.01 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Percent Heavy Veh, \% | 2 | 0 | 0 | 0 | 1 | 1 |
| Cap, veh/h 7 | 755 | 0 | 0 | 1457 | 866 | 770 |
| Arrive On Green 0.81 | 0.81 | 0.00 | 0.00 | 0.40 | 0.48 | 0.48 |
| Sat Flow, veh/h 187 | 1870 | 0 | 0 | 3800 | 1795 | 1598 |
| Grp Volume(v), veh/h 123 | 123 | 0 | 0 | 444 | 697 | 705 |
| Grp Sat Flow(s), veh/h/ln1870 | 1870 | 0 | 0 | 1805 | 1795 | 1598 |
| Q Serve(g_s), s | 1.0 | 0.0 | 0.0 | 5.9 | 23.0 | 28.6 |
| Cycle Q Clear(g_c), s | 1.0 | 0.0 | 0.0 | 5.9 | 23.0 | 28.6 |
| Prop In Lane |  | 0.00 | 0.00 |  | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h 7 | 755 | 0 | 0 | 1457 | 866 | 770 |
| V/C Ratio(X) 0.1 | 0.16 | 0.00 | 0.00 | 0.30 | 0.81 | 0.92 |
| Avail Cap(c_a), veh/h 7 | 755 | 0 | 0 | 1457 | 1129 | 1004 |
| HCM Platoon Ratio 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 4.1 | 0.0 | 0.0 | 14.2 | 15.3 | 16.8 |
| Incr Delay (d2), s/veh | 0.5 | 0.0 | 0.0 | 0.5 | 2.5 | 9.2 |
| Initial Q Delay(d3),s/veh 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/r0. 5 |  | 0.0 | 0.0 | 2.4 | 9.0 | 11.3 |

Unsig. Movement Delay, s/veh

| LnGrp Delay(d),s/veh | 4.6 | 0.0 | 0.0 | 14.7 | 17.8 | 26.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| LnGrp LOS | A | A | A | B | B | C |
| Approach Vol, veh/h | 123 |  |  | 444 | 1402 |  |
| Approach Delay, s/veh | 4.6 |  |  | 14.7 | 21.9 |  |
| Approach LOS | A |  |  | B | C |  |


| Timer - Assigned Phs | 2 | 4 | 8 |
| :--- | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 37.8 | 32.2 | 32.2 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 44.0 | 18.0 | 18.0 |
| Max Q Clear Time (g_c+11), s | 30.6 | 7.9 | 3.0 |
| Green Ext Time (p_c), s | 3.1 | 2.3 | 0.5 |

## Intersection Summary

HCM 6th Ctrl Delay 19.2
HCM 6th LOS B







HCM 6th Signalized Intersection Summary
5: 13th \& Belmont
01/13/2022

|  | 4 | $\rightarrow$ |  | $\dagger$ |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }_{7}$ | $\hat{*}$ |  |  | $\hat{\beta}$ |  | \% | $\hat{\beta}$ |  |  | ${ }_{4}$ |  |
| Traffic Volume (veh/h) | 70 | 45 | 200 | 45 | 50 | 5 | 125 | 565 | 5 | 50 | 930 | 60 |
| Future Volume (veh/h) | 70 | 45 | 200 | 45 | 50 | 5 | 125 | 565 | 5 | 50 | 930 | 60 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 0.99 | 1.00 |  | 0.99 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1856 | 1781 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1885 |
| Adj Flow Rate, veh/h | 77 | 49 | 72 | 49 | 55 | 5 | 137 | 621 | 5 | 55 | 1022 | 66 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Percent Heavy Veh, \% | 2 | 3 | 3 | 8 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 1 |
| Cap, veh/h | 206 | 92 | 135 | 93 | 91 | 7 | 330 | 1466 | 12 | 77 | 1134 | 72 |
| Arrive On Green | 0.14 | 0.14 | 0.13 | 0.13 | 0.14 | 0.13 | 0.05 | 0.79 | 0.79 | 0.70 | 0.71 | 0.70 |
| Sat Flow, veh/h | 1337 | 675 | 992 | 333 | 670 | 48 | 1781 | 1853 | 15 | 60 | 1608 | 102 |
| Grp Volume(v), veh/h | 77 | 0 | 121 | 109 | 0 | 0 | 137 | 0 | 626 | 1143 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1337 | 0 | 1668 | 1051 | 0 | 0 | 1781 | 0 | 1868 | 1770 | 0 | 0 |
| Q Serve(g_s), s | 0.0 | 0.0 | 7.4 | 4.7 | 0.0 | 0.0 | 2.1 | 0.0 | 11.6 | 37.4 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 8.2 | 0.0 | 7.4 | 12.2 | 0.0 | 0.0 | 2.1 | 0.0 | 11.6 | 58.8 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.60 | 0.45 |  | 0.05 | 1.00 |  | 0.01 | 0.05 |  | 0.06 |
| Lane Grp Cap (c), veh/h | 206 | 0 | 227 | 186 | 0 | 0 | 330 | 0 | 1478 | 1275 | 0 | 0 |
| V/C Ratio(X) | 0.37 | 0.00 | 0.53 | 0.59 | 0.00 | 0.00 | 0.42 | 0.00 | 0.42 | 0.90 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 328 | 0 | 379 | 325 | 0 | 0 | 372 | 0 | 1478 | 1275 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 44.6 | 0.0 | 44.4 | 46.8 | 0.0 | 0.0 | 3.1 | 0.0 | 3.6 | 13.1 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.4 | 0.0 | 0.7 | 1.1 | 0.0 | 0.0 | 0.3 | 0.0 | 0.9 | 10.0 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 2.0 | 0.0 | 3.2 | 3.0 | 0.0 | 0.0 | 0.7 | 0.0 | 3.9 | 24.1 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 45.0 | 0.0 | 45.1 | 47.9 | 0.0 | 0.0 | 3.4 | 0.0 | 4.5 | 23.1 | 0.0 | 0.0 |
| LnGrp LOS | D | A | D | D | A | A | A | A | A | C | A | A |
| Approach Vol, veh/h |  | 198 |  |  | 109 |  |  | 763 |  |  | 1143 |  |
| Approach Delay, s/veh |  | 45.1 |  |  | 47.9 |  |  | 4.3 |  |  | 23.1 |  |
| Approach LOS |  | D |  |  | D |  |  | A |  |  | C |  |
| Timer - Assigned Phs |  | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s |  | 91.0 |  | 19.0 | 9.4 | 81.6 |  | 19.0 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  | 4.5 |  | 4.5 | 4.5 | 4.5 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s |  | 86.5 |  | 24.5 | 7.5 | 74.5 |  | 24.5 |  |  |  |  |
| Max Q Clear Time (g_c+1), s |  | 13.6 |  | 10.2 | 4.1 | 60.8 |  | 14.2 |  |  |  |  |
| Green Ext Time (p_c), s |  | 5.4 |  | 0.5 | 0.1 | 8.6 |  | 0.2 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr DelayHCM 6th LOS |  |  | 19.8 |  |  |  |  |  |  |  |  |  |
|  |  |  | B |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | * |  |  | \$ |  |  | \& |  |
| Traffic Vol, veh/h | 45 | 25 | 5 | 5 | 10 | 5 | 60 | 750 | 40 | 5 | 185 | 30 |
| Future Vol, veh/h | 45 | 25 | 5 | 5 | 10 | 5 | 60 | 750 | 40 | 5 | 185 | 30 |
| Conflicting Peds, \#/hr | 13 | 0 | 0 | 0 | 0 | 13 | 1 | 0 | 8 | 8 | 0 | 1 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 3 | 2 | 2 | 2 | 17 | 2 | 2 | 3 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 47 | 26 | 5 | 5 | 11 | 5 | 63 | 789 | 42 | 5 | 195 | 32 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.7 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | \$ |  |  | * |  |  | * |  |
| Traffic Vol, veh/h | 10 | 15 | 5 | 5 | 35 | 20 | 30 | 730 | 50 | 10 | 210 | 5 |
| Future Vol, veh/h | 10 | 15 | 5 | 5 | 35 | 20 | 30 | 730 | 50 | 10 | 210 | 5 |
| Conflicting Peds, \#/hr | 15 | 0 | 20 | 20 | 0 | 15 | 8 | 0 | 13 | 13 | 0 | 8 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 3 | 2 | 2 | 3 | 6 | 2 | 2 | 2 |
| Mvmt Flow | 11 | 16 | 5 | 5 | 38 | 22 | 32 | 785 | 54 | 11 | 226 | 5 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.4 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\mathbf{F}$ |  |  | $\mathbf{\uparrow}$ |
| Traffic Vol, veh/h | 35 | 65 | 745 | 80 | 10 | 225 |
| Future Vol, veh/h | 35 | 65 | 745 | 80 | 10 | 225 |
| Conflicting Peds, \#/hr | 15 | 0 | 0 | 23 | 23 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 91 | 91 | 91 | 91 | 91 | 91 |
| Heavy Vehicles, \% | 2 | 2 | 3 | 2 | 2 | 2 |
| Mvmt Flow | 38 | 71 | 819 | 88 | 11 | 247 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1170 | 886 | 0 | 0 | 930 | 0 |
| Stage 1 | 886 | - | - | - | - | - |
| Stage 2 | 284 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 213 | 343 | - | - | 736 | - |
| Stage 1 | 403 | - | - | - | - | - |
| Stage 2 | 764 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 202 | 335 | - | - | 720 | - |
| Mov Cap-2 Maneuver | 202 | - | - | - | - | - |
| Stage 1 | 394 | - | - | - | - | - |
| Stage 2 | 740 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 26.9 |  | 0 |  | 0.4 |  |
| HCM LOS | D |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 272 | 720 | - |
| HCM Lane V/C Ratio |  | - | - | 0.404 | 0.015 | - |
| HCM Control Delay (s) |  | - | - | 26.9 | 10.1 | 0 |
| HCM Lane LOS |  | - | - | D | B | A |
| HCM 95th \%tile Q(veh) |  | - | - | 1.9 | 0 | - |







## Table of Contents

Intersection Analysis Summary ..... 2
Intersection Level Of Service Report .....  3
Intersection 1: 13th/Belmont ..... 3
Turning Movement Volume: Summary ..... 5
Turning Movement Volume: Detail .....  6

Generated with PTV VISTRO
Version 2021 (SP 0-6)

Vistro File: C:I...IScen 1_HoodRiver OR281 RABs.vistro
Scenario 1 1-lane
Report File: X:I...IScenario 1.pdf
1/13/2022

Intersection Analysis Summary

| ID | Intersection Name | Control Type | Method | Worst Mvmt | V/C | Delay (s/veh) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 13 th/Belmont | Roundabout | HCM 6th <br> Edition | SB Thru |  | 46.8 | E |

V/C, Delay, LOS: For two-way stop, these values are taken from the movement with the worst (highest) delay value. For all other control types, they are taken for the whole intersection.

## Intersection Level Of Service Report Intersection 1: 13th/Belmont

Control Type: Analysis Method: Analysis Period:
Roundabout HCM 6th Edition 15 minutes

Intersection Setup

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |
| Turning Movement | Thru | Right | Right2 | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | Yes |  |  | Yes |  |  | Yes |  |  | Yes |  |  |

## Volumes

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 125 | 565 | 5 | 50 | 930 | 60 | 70 | 45 | 200 | 45 | 50 | 5 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 1.00 | 2.00 | 3.00 | 3.00 | 8.00 | 2.00 | 2.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 125 | 565 | 5 | 50 | 930 | 60 | 70 | 45 | 200 | 45 | 50 | 5 |
| Peak Hour Factor | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 34 | 155 | 1 | 14 | 255 | 16 | 19 | 12 | 55 | 12 | 14 | 1 |
| Total Analysis Volume [veh/h] | 137 | 621 | 5 | 55 | 1022 | 66 | 77 | 49 | 220 | 49 | 55 | 5 |
| Pedestrian Volume [ped/h] | 2 |  |  | 0 |  |  | 5 |  |  | 3 |  |  |

## Generated with PTV VISTRO

Version 2021 (SP 0-6)
Intersection Settings

| Number of Conflicting Circulating Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Circulating Flow Rate [veh/h] | 185 |  |  | 249 |  |  | 1151 |  |  | 852 |  |  |
| Exiting Flow Rate [veh/h] | 1322 |  |  | 717 |  |  | 263 |  |  | 112 |  |  |
| Demand Flow Rate [veh/h] | 125 | 565 | 5 | 50 | 930 | 60 | 70 | 45 | 200 | 45 | 50 | 5 |
| Adjusted Demand Flow Rate [veh/h] | 137 | 621 | 5 | 55 | 1022 | 66 | 77 | 49 | 220 | 49 | 55 | 5 |

## Lanes

| Overwrite Calculated Critical Headway | No | No | No |
| :---: | :---: | :---: | :---: |
| User-Defined Critical Headway [s] | 4.00 | 4.00 | 4.00 |
| Overwrite Calculated Follow-Up Time | No | No | No |
| User-Defined Follow-Up Time [s] | 3.00 | 3.00 | 3.00 |
| A (intercept) | 1380.00 | 1380.00 | 1380.00 |
| B (coefficient) | 0.00102 | 0.00102 | 0.00102 |
| HV Adjustment Factor | 0.98 | 0.98 | 0.97 |
| Entry Flow Rate [veh/h] | 779 | 1166 | 356 |
| Capacity of Entry and Bypass Lanes [veh/h] | 1143 | 1071 | 427 |
| Pedestrian Impedance | 1.00 | 1.00 | 1.00 |
| Capacity per Entry Lane [veh/h] | 1120 | 1051 | 1.00 |
| X, volume / capacity | 0.68 | 579 |  |

Movement, Approach, \& Intersection Results

| Lane LOS | B | F | E | A |
| :---: | :---: | :---: | :---: | :---: |
| 95th-Percentile Queue Length [veh] | 5.69 | 27.29 | 7.87 | 0.73 |
| 95th-Percentile Queue Length [ft] | 142.22 | 682.23 | 196.81 | 18.17 |
| Approach Delay [s/veh] | 13.19 | 73.80 | 43.70 | 9.08 |
| Approach LOS | B | F | E | A |
| Intersection Delay [s/veh] | 46.81 |  |  |  |
| Intersection LOS | E |  |  |  |

Generated with PTV VISTRO
Version 2021 (SP 0-6)

Vistro File: C:I...IScen 1_HoodRiver OR281 RABs.vistro
Report File: X:I...IScenario 1.pdf
Turning Movement Volume: Summary

| ID | Intersection Name | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Thru | Right | 2 | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| 1 | 13th/Belmont | 125 | 565 | 5 | 50 | 930 | 60 | 70 | 45 | 200 | 45 | 50 | 5 | 2150 |

Generated with PTV VISTRO
Version 2021 (SP 0-6)

Vistro File: C:I...IScen 1_HoodRiver OR281 RABs.vistro

Turning Movement Volume: Detail

| ID | Intersection Name | Volume Type | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Thru | Right | 2 | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| 1 | 13th/Belmont | Final Base | 125 | 565 | 5 | 50 | 930 | 60 | 70 | 45 | 200 | 45 | 50 | 5 | 2150 |
|  |  | Growth Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | - |
|  |  | In Process | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Net New Trips | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Other | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Future Total | 125 | 565 | 5 | 50 | 930 | 60 | 70 | 45 | 200 | 45 | 50 | 5 | 2150 |












| Approach | WB | NB |
| :--- | ---: | ---: |
| HCM Control Delay, s | 76.3 | 0 |
| HCM LOS | F |  |


| Minor Lane/Major Mvmt | NBT | NBRWBLn1 |
| :--- | ---: | ---: |
| Capacity (veh/h) | - | -174 |
| HCM Lane V/C Ratio | - | -0.789 |
| HCM Control Delay (s) | - | -76.3 |
| HCM Lane LOS | - | - |
| HCM 95th \%tile Q(veh) | - | $-\quad 5.2$ |



| Major/Minor | Minor2 | Major1 |  |
| :--- | ---: | ---: | :--- |
| Conflicting Flow All | 1632 | - | 15 |
| $\quad$ Stage 1 | 15 | - | - |
| $\quad$ Stage 2 | 1617 | - | - |


| Approach | EB | NB |
| :--- | ---: | ---: |
| HCM Control Delay, s 134.3 | 0.8 |  |
| HCM LOS | F |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 |  |
| :--- | ---: | ---: | ---: |
| Capacity (veh/h) | 1573 | -70 |  |
| HCM Lane V/C Ratio | 0.098 | -0.706 |  |
| HCM Control Delay (s) | 7.5 | 0 | 134.3 |
| HCM Lane LOS | A | A | F |
| HCM 95th \%tile Q(veh) | 0.3 | - | 3.2 |



| Movement EBT | EBR | WBL | WBT | NBL | NBR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations $\uparrow$ |  |  | 4 | ${ }^{1}$ | 「' |
| Traffic Volume (veh/h) 60 | 0 | 0 | 435 | 635 | 640 |
| Future Volume (veh/h) 60 | 0 | 0 | 435 | 635 | 640 |
| Initial Q $(\mathrm{Qb})$, veh 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach No |  |  | No | No |  |
| Adj Sat Flow, veh/h/ln 1870 | 0 | 0 | 1870 | 1885 | 1885 |
| Adj Flow Rate, veh/h 66 | 0 | 0 | 478 | 698 | 703 |
| Peak Hour Factor 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Percent Heavy Veh, \% 2 | 0 | 0 | 2 | 1 | 1 |
| Cap, veh/h 517 | 0 | 0 | 517 | 816 | 726 |
| Arrive On Green 0.55 | 0.00 | 0.00 | 0.28 | 0.45 | 0.45 |
| Sat Flow, veh/h 1870 | 0 | 0 | 1870 | 1795 | 1598 |
| Grp Volume(v), veh/h 66 | 0 | 0 | 478 | 698 | 703 |
| Grp Sat Flow(s), veh/h/ln1870 | 0 | 0 | 1870 | 1795 | 1598 |
| Q Serve(g_s), s 1.5 | 0.0 | 0.0 | 22.4 | 31.2 | 38.6 |
| Cycle Q Clear(g_c), s 1.5 | 0.0 | 0.0 | 22.4 | 31.2 | 38.6 |
| Prop In Lane | 0.00 | 0.00 |  | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h 517 | 0 | 0 | 517 | 816 | 726 |
| V/C Ratio(X) 0.13 | 0.00 | 0.00 | 0.92 | 0.86 | 0.97 |
| Avail Cap(c_a), veh/h 727 | 0 | 0 | 727 | 938 | 834 |
| HCM Platoon Ratio 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) 0.95 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh 14.9 | 0.0 | 0.0 | 31.7 | 21.9 | 23.9 |
| Incr Delay (d2), s/veh 0.0 | 0.0 | 0.0 | 24.8 | 6.3 | 21.5 |
| Initial Q Delay(d3),s/veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/lm0.6 | 0.0 | 0.0 | 13.5 | 14.0 | 18.1 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |
| LnGrp Delay(d),s/veh 14.9 | 0.0 | 0.0 | 56.4 | 28.2 | 45.4 |
| LnGrp LOS B | A | A | E | C | D |
| Approach Vol, veh/h 66 |  |  | 478 | 1401 |  |
| Approach Delay, s/veh 14.9 |  |  | 56.4 | 36.9 |  |
| Approach LOS B |  |  | E | D |  |


| Timer - Assigned Phs | 2 | 6 | 8 |
| :--- | ---: | ---: | ---: |
| Phs Duration (G+Y+Rc), s | 28.9 | 28.9 | 44.9 |
| Change Period (Y+Rc), s | 4.0 | 4.0 | 4.0 |
| Max Green Setting (Gmax), s | 35.0 | 35.0 | 47.0 |
| Max Q Clear Time (g_c+11), s | 3.5 | 24.4 | 40.6 |
| Green Ext Time (p_c), s | 0.1 | 0.5 | 0.3 |


| Intersection Summary |  |
| :--- | ---: |
| HCM 6th Ctrl Delay | 40.9 |
| HCM 6th LOS | D |

## Table of Contents

Intersection Analysis Summary ..... 2
Intersection Level Of Service Report ..... 3
Intersection 1: 13th/Belmont ..... 3
Intersection 2: 13th/12th ..... 5
Intersection 3: 13th/May ..... 7
Turning Movement Volume: Summary ..... 9
Turning Movement Volume: Detail ..... 10

## Intersection Level Of Service Report Intersection 1: 13th/Belmont

| Control Type: | Roundabout | Delay (sec /veh): |  |
| :---: | :---: | :---: | :---: |
| Analysis Method: | HCM 6th Edition | Level Of Service: |  |
| Analysis Period: | 15 minutes |  |  |

Intersection Setup

| Name |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach |  |  |  |  |  |  |
| Lane Configuration |  |  |  |  |  |  |
| Turning Movement | Thru | Right | Left | Thru | Thru | Thru |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  | 25.00 |  | 25.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | Yes |  | Yes |  | Yes |  |

## Volumes

| Name |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 1010 | 200 | 0 | 375 | 165 | 0 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 8.00 | 2.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 1010 | 200 | 0 | 375 | 165 | 0 |
| Peak Hour Factor | 0.9100 | 0.9100 | 1.0000 | 0.9100 | 0.9100 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 277 | 55 | 0 | 103 | 45 | 0 |
| Total Analysis Volume [veh/h] | 1110 | 220 | 0 | 412 | 181 | 0 |
| Pedestrian Volume [ped/h] | 0 |  | 3 |  | 0 |  |

## Generated with PTV VISTRO

Version 2021 (SP 0-6)

## Intersection Settings

| Number of Conflicting Circulating Lanes | 1 |  | 1 |  | 1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Circulating Flow Rate [veh/h] | 195 |  | 1132 |  | 0 |  |
| Exiting Flow Rate [veh/h] | 0 |  | 420 |  | 1552 |  |
| Demand Flow Rate [veh/h] | 1010 | 200 | 0 | 375 | 165 | 0 |
| Adjusted Demand Flow Rate [veh/h] | 1110 | 220 | 0 | 412 | 181 | 0 |

## Lanes

| Overwrite Calculated Critical Headway | No | No | No |
| :---: | :---: | :---: | :---: |
| User-Defined Critical Headway [s] | 4.00 | 4.00 | 4.00 |
| Overwrite Calculated Follow-Up Time | No | No | No |
| User-Defined Follow-Up Time [s] | 3.00 | 3.00 | 3.00 |
| A (intercept) | 1380.00 | 1380.00 | 1380.00 |
| B (coefficient) | 0.00102 | 0.00102 | 0.00102 |
| HV Adjustment Factor | 0.98 | 0.98 | 0.93 |
| Entry Flow Rate [veh/h] | 1357 | 421 | 196 |
| Capacity of Entry and Bypass Lanes [veh/h] | 1131 | 435 | 1380 |
| Pedestrian Impedance | 1.00 | 1.00 | 1.00 |
| Capacity per Entry Lane [veh/h] | 1109 | 427 | 1278 |
| X, volume / capacity | 1.20 | 0.97 | 0.14 |

Movement, Approach, \& Intersection Results

| Lane LOS | F | F | A |
| :---: | :---: | :---: | :---: |
| 95th-Percentile Queue Length [veh] | 40.13 | 11.57 | 0.49 |
| 95th-Percentile Queue Length [ft] | 1003.29 | 289.17 | 12.33 |
| Approach Delay [s/veh] | 114.70 | 66.79 | 3.99 |
| Approach LOS | F | F |  |
| Intersection Delay [s/veh] |  | 94.02 |  |
| Intersection LOS | F |  |  |

## Intersection Level Of Service Report intersection 2: 13th/12th

Control Type:
Analysis Method: Analysis Period:
Roundabout HCM 6th Edition 15 minutes

Intersection Setup

| Name |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach |  |  |  |  |  |  |
| Lane Configuration |  |  |  |  |  |  |
| Turning Movement | Left | Thru | Thru | Right | Left | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 1 | 0 | 0 | 0 | 0 | 1 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  | 30.00 |  | 25.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | Yes |  | Yes |  | No |  |

## Volumes

| Name |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 160 | 1225 | 125 | 85 | 115 | 1385 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 160 | 1225 | 125 | 85 | 115 | 1385 |
| Peak Hour Factor | 0.9500 | 0.9500 | 0.9100 | 0.9100 | 0.9500 | 0.9500 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 42 | 322 | 34 | 23 | 30 | 364 |
| Total Analysis Volume [veh/h] | 168 | 1289 | 137 | 93 | 121 | 1458 |
| Pedestrian Volume [ped/h] | 0 |  | 13 |  | 0 |  |

## Generated with PTV VISTRO

Version 2021 (SP 0-6)

## Intersection Settings

| Number of Conflicting Circulating Lanes | 2 | 1 | 2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Circulating Flow Rate [veh/h] | 123 |  | 171 | 0 |  |
| Exiting Flow Rate [veh/h] | 1487 |  | 1438 | 1 |  |
| Demand Flow Rate [veh/h] | 160 | 1225 | 0 | 0 | 115 |
| Adjusted Demand Flow Rate [veh/h] | 168 | 1289 | 0 | 0 | 121 |

## Lanes

| Overwrite Calculated Critical Headway | No | No |  | No | No |
| :---: | :---: | :---: | :---: | :---: | :---: |
| User-Defined Critical Headway [s] | 4.00 | 4.00 |  | 4.00 | 4.00 |
| Overwrite Calculated Follow-Up Time | No | No |  | No | No |
| User-Defined Follow-Up Time [s] | 3.00 | 3.00 |  | 3.00 | 3.00 |
| A (intercept) | 1350.00 | 1420.00 |  | 1350.00 | 1420.00 |
| B (coefficient) | 0.00092 | 0.00085 |  | 0.00092 | 0.00085 |
| HV Adjustment Factor | 0.98 | 0.98 |  | 0.98 | 0.98 |
| Entry Flow Rate [veh/h] | 172 | 1315 |  | 757 | 854 |
| Capacity of Entry and Bypass Lanes [veh/h] | 1206 | 1279 |  | 1350 | 1420 |
| Pedestrian Impedance | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Capacity per Entry Lane [veh/h] | 1182 | 1254 |  | 1324 | 1393 |
| X, volume / capacity | 0.14 | 1.03 |  | 0.56 | 0.60 |

Movement, Approach, \& Intersection Results

| Lane LOS | A | F |  | A | A |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 95th-Percentile Queue Length [veh] | 0.50 | 24.32 |  | 3.65 | 4.26 |
| 95th-Percentile Queue Length [ft] | 12.38 | 607.89 |  | 91.16 | 106.50 |
| Approach Delay [s/veh] | 45.83 |  | 0.00 | 9.19 |  |
| Approach LOS | E |  | A | A |  |
| Intersection Delay [s/veh] | 26.77 |  |  |  |  |
| Intersection LOS | D |  |  |  |  |



| Movement EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | $\ddagger$ |  | ${ }^{*}$ | F |  | ${ }^{7}$ | $\uparrow$ |  |  | 4 |  |
| Traffic Volume (veh/h) 50 | 35 | 80 | 310 | 195 | 140 | 100 | 650 | 110 | 25 | 725 | 55 |
| Future Volume (veh/h) 50 | 35 | 80 | 310 | 195 | 140 | 100 | 650 | 110 | 25 | 725 | 55 |
| Initial Q (Qb), veh 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) 0.99 |  | 0.98 | 1.00 |  | 0.98 | 1.00 |  | 0.99 | 1.00 |  | 0.99 |
| Parking Bus, Adj 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln 1870 | 1885 | 1856 | 1870 | 1841 | 1885 | 1870 | 1870 | 1870 | 1870 | 1856 | 1870 |
| Adj Flow Rate, veh/h 53 | 37 | 85 | 330 | 207 | 116 | 106 | 691 | 117 | 27 | 771 | 59 |
| Peak Hour Factor 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh, \% 2 | 1 | 3 | 2 | 4 | 1 | 2 | 2 | 2 | 2 | 3 | 2 |
| Cap, veh/h 87 | 69 | 98 | 330 | 361 | 202 | 275 | 908 | 154 | 55 | 768 | 58 |
| Arrive On Green 0.20 | 0.21 | 0.20 | 0.12 | 0.55 | 0.55 | 0.06 | 0.58 | 0.58 | 0.48 | 0.48 | 0.48 |
| Sat Flow, veh/h 166 | 329 | 468 | 1781 | 1101 | 617 | 1781 | 1557 | 264 | 28 | 1595 | 120 |
| Grp Volume(v), veh/h 175 | 0 | 0 | 330 | 0 | 323 | 106 | 0 | 808 | 857 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln 963 | 0 | 0 | 1781 | 0 | 1718 | 1781 | 0 | 1820 | 1743 | 0 | 0 |
| Q Serve(g_s), s $\quad 5.6$ | 0.0 | 0.0 | 6.2 | 0.0 | 11.2 | 2.5 | 0.0 | 30.0 | 22.0 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s 16.8 | 0.0 | 0.0 | 6.2 | 0.0 | 11.2 | 2.5 | 0.0 | 30.0 | 42.9 | 0.0 | 0.0 |
| Prop In Lane 0.30 |  | 0.49 | 1.00 |  | 0.36 | 1.00 |  | 0.14 | 0.03 |  | 0.07 |
| Lane Grp Cap(c), veh/h 248 | 0 | 0 | 330 | 0 | 563 | 275 | 0 | 1062 | 871 | 0 | 0 |
| V/C Ratio(X) 0.71 | 0.00 | 0.00 | 1.00 | 0.00 | 0.57 | 0.39 | 0.00 | 0.76 | 0.98 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h 248 | 0 | 0 | 330 | 0 | 563 | 282 | 0 | 1062 | 871 | 0 | 0 |
| HCM Platoon Ratio 1.00 | 1.00 | 1.00 | 1.67 | 1.67 | 1.67 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) $\quad 1.00$ | 0.00 | 0.00 | 0.92 | 0.00 | 0.92 | 1.00 | 0.00 | 1.00 | 0.54 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh 34.8 | 0.0 | 0.0 | 34.7 | 0.0 | 16.2 | 9.2 | 0.0 | 14.1 | 23.6 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh 15.6 | 0.0 | 0.0 | 47.3 | 0.0 | 3.9 | 0.9 | 0.0 | 5.1 | 18.8 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/Ir4. 9 | 0.0 | 0.0 | 10.8 | 0.0 | 4.1 | 1.0 | 0.0 | 12.8 | 22.3 | 0.0 | 0.0 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh 50.4 | 0.0 | 0.0 | 82.1 | 0.0 | 20.1 | 10.1 | 0.0 | 19.2 | 42.5 | 0.0 | 0.0 |
| LnGrp LOS D | A | A | F | A | C | B | A | B | D | A | A |
| Approach Vol, veh/h | 175 |  |  | 653 |  |  | 914 |  |  | 857 |  |
| Approach Delay, s/veh | 50.4 |  |  | 51.4 |  |  | 18.2 |  |  | 42.5 |  |
| Approach LOS | D |  |  | D |  |  | B |  |  | D |  |
| Timer - Assigned Phs | 2 | 3 | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $s$ | 56.5 | 10.7 | 22.8 | 9.1 | 47.4 |  | 33.5 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 52.0 | 6.2 | 18.3 | 5.0 | 42.5 |  | 29.0 |  |  |  |  |
| Max Q Clear Time (g_ctl1), s | 32.0 | 8.2 | 18.8 | 4.5 | 44.9 |  | 13.2 |  |  |  |  |
| Green Ext Time (p_c), s | 6.5 | 0.0 | 0.0 | 0.0 | 0.0 |  | 1.9 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay 36.7 |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  | D |  |  |  |  |  |  |  |  |  |





| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2200 | 2183 | 1166 | 2190 | 2186 | 965 | 1167 | 0 |  | 959 | 0 | 0 |
| Stage 1 | 1214 | 1214 | - | 967 | 967 | - | - | - | - | - - | - | - |
| Stage 2 | 986 | 969 |  | 1223 | 1219 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | 4.12 | - |  | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - |  | - - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 | 2.218 | - |  | - 2.218 | - | - |
| Pot Cap-1 Maneuver | 32 | 46 | 236 | ~33 | 46 | 309 | 599 | - |  | 717 | - | - |
| Stage 1 | 222 | 254 | - | 306 | 333 | - | - | - | - | - - | - | - |
| Stage 2 | 298 | 332 | - | 219 | 253 | - | - | - |  | - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  | - |  |  | - | - |
| Mov Cap-1 Maneuver | 21 | 44 | 234 | $\sim 25$ | 44 | 305 | 597 | - |  | 712 | - | - |
| Mov Cap-2 Maneuver | 21 | 44 | - | $\sim 25$ | 44 | - | - | - | - | - - | - | - |
| Stage 1 | 220 | 244 | - | 301 | 328 | - | - | - |  | - | - | - |
| Stage 2 | 260 | 327 | - | 197 | 243 | - | - | - | - | - - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 163 |  |  | \$ 641.7 |  |  | 0.1 |  |  | 0.2 |  |  |
| HCM LOS | F |  |  | F |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvm |  | NBL | NBT | NBR | EBLn1 | NBLn1 | SBL | SBT | SBR |  |  |  |
| Capacity (veh/h) |  | 597 |  |  | 41 | 39 | 712 | - |  |  |  |  |
| HCM Lane V/C Ratio |  | 0.009 | - |  | 0.513 | 1.889 | 0.037 | - | - |  |  |  |
| HCM Control Delay (s) |  | 11.1 | - | - | 1638 | 641.7 | 10.2 | - | - |  |  |  |
| HCM Lane LOS |  | B | - | - | F | F | B | - | - |  |  |  |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | 1.8 | 7.9 | 0.1 | - | - |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ : Volume exceeds capacity |  | \$: Delay exceeds 300s |  |  |  | +: Computation Not Defined |  |  |  | *: All major volume in platoon |  |  |


|  | 4 |  |  | 7 |  |  | 4 | $\dagger$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\hat{F}$ |  |  | \$ |  | \% | $\uparrow$ |  | ${ }^{7}$ | 1 |  |
| Traffic Volume (veh/h) | 70 | 45 | 200 | 15 | 20 | 5 | 120 | 855 | 5 | 50 | 1000 | 100 |
| Future Volume (veh/h) | 70 | 45 | 200 | 15 | 20 | 5 | 120 | 855 | 5 | 50 | 1000 | 100 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 0.99 |  | 0.99 | 0.99 |  | 0.99 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/n | 1870 | 1856 | 1856 | 1781 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1885 |
| Adj Flow Rate, veh/h | 77 | 49 | 71 | 16 | 22 | 5 | 132 | 940 | 5 | 55 | 1099 | 110 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Percent Heavy Veh, \% | 2 | 3 | 3 | 8 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 1 |
| Cap, veh/h | 183 | 69 | 100 | 61 | 70 | 11 | 266 | 1394 | 7 | 431 | 1242 | 124 |
| Arrive On Green | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.05 | 0.75 | 0.75 | 0.04 | 0.74 | 0.74 |
| Sat Flow, veh/h | 1375 | 680 | 986 | 162 | 687 | 112 | 1781 | 1859 | 10 | 1781 | 1672 | 167 |
| Grp Volume(v), veh/h | 77 | 0 | 120 | 43 | 0 | 0 | 132 | 0 | 945 | 55 | 0 | 1209 |
| Grp Sat Flow(s),veh/h/ln | 1375 | 0 | 1666 | 960 | 0 | 0 | 1781 | 0 | 1869 | 1781 | 0 | 1840 |
| Q Serve(g_s), s | 0.0 | 0.0 | 7.8 | 0.1 | 0.0 | 0.0 | 1.9 | 0.0 | 28.5 | 0.8 | 0.0 | 55.1 |
| Cycle Q Clear(g_c), s | 7.7 | 0.0 | 7.8 | 7.9 | 0.0 | 0.0 | 1.9 | 0.0 | 28.5 | 0.8 | 0.0 | 55.1 |
| Prop In Lane | 1.00 |  | 0.59 | 0.37 |  | 0.12 | 1.00 |  | 0.01 | 1.00 |  | 0.09 |
| Lane Grp Cap (c), veh/h | 183 | 0 | 169 | 137 | 0 | 0 | 266 | 0 | 1401 | 431 | 0 | 1366 |
| V/C Ratio(X) | 0.42 | 0.00 | 0.71 | 0.31 | 0.00 | 0.00 | 0.50 | 0.00 | 0.67 | 0.13 | 0.00 | 0.89 |
| Avail Cap(c_a), veh/h | 275 | 0 | 281 | 242 | 0 | 0 | 298 | 0 | 1401 | 447 | 0 | 1366 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 48.5 | 0.0 | 48.7 | 46.3 | 0.0 | 0.0 | 21.7 | 0.0 | 7.1 | 6.5 | 0.0 | 10.8 |
| Incr Delay (d2), s/veh | 1.5 | 0.0 | 5.4 | 1.3 | 0.0 | 0.0 | 1.4 | 0.0 | 2.6 | 0.1 | 0.0 | 8.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/In | 2.2 | 0.0 | 3.5 | 1.2 | 0.0 | 0.0 | 2.4 | 0.0 | 10.7 | 0.3 | 0.0 | 22.1 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 50.0 | 0.0 | 54.1 | 47.6 | 0.0 | 0.0 | 23.1 | 0.0 | 9.7 | 6.6 | 0.0 | 19.5 |
| LnGrp LOS | D | A | D | D | A | A | C | A | A | A | A | B |
| Approach Vol, veh/h |  | 197 |  |  | 43 |  |  | 1077 |  |  | 1264 |  |
| Approach Delay, s/veh |  | 52.5 |  |  | 47.6 |  |  | 11.3 |  |  | 18.9 |  |
| Approach LOS |  | D |  |  | D |  |  | B |  |  | B |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), $s$ | 8.6 | 87.6 |  | 15.3 | 9.4 | 86.8 |  | 15.3 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 |  | 4.5 | 4.5 | 4.5 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 5.1 | 83.1 |  | 18.3 | 6.9 | 81.3 |  | 18.3 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 2.8 | 30.5 |  | 9.8 | 3.9 | 57.1 |  | 9.9 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 10.9 |  | 0.5 | 0.1 | 13.5 |  | 0.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrr DelayHCM 6th LOS |  |  | 18.8 |  |  |  |  |  |  |  |  |  |
|  |  |  | B |  |  |  |  |  |  |  |  |  |






| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Minor1 | Major1 |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 562 | 0 | 0 |
| Stage 1 | - | - | - | - |
| Stage 2 | - | - | - | - |
| Critical Hdwy | - | 6.22 | - | - |
| Critical Hdwy Stg 1 | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - |
| Follow-up Hdwy | - | 3.318 | - | - |
| Pot Cap-1 Maneuver | 0 | 526 | - | - |
| Stage 1 | 0 | - | - | - |
| Stage 2 | 0 | - | - | - |
| Platoon blocked, \% |  |  | - | - |
| Mov Cap-1 Maneuver | - | 514 | - | - |
| Mov Cap-2 Maneuver | - | - | - | - |
| Stage 1 | - | - | - | - |
| Stage 2 | - | - | - | - |
|  |  |  |  |  |
| Approach | WB |  | NB |  |
| HCM Control Delay, s | 14 |  | 0 |  |
| HCM LOS | B |  |  |  |
|  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRI |  |
| Capacity (veh/h) |  | - | - | 514 |
| HCM Lane V/C Ratio |  | - | - |  |
| HCM Control Delay (s) |  | - | - | 14 |
| HCM Lane LOS |  | - | - | B |
| HCM 95th \%tile Q(veh) |  | - | - | 0.9 |



| Major/Minor $\quad$ N | Minor2 |  | Major1 |  |
| :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 697 | - | 15 | 0 |
| Stage 1 | 15 | - | - | - |
| Stage 2 | 682 | - | - | - |
| Critical Hdwy | 6.42 | - | 4.13 | - |
| Critical Hdwy Stg 1 | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - |
| Follow-up Hdwy | 3.518 |  | 2.227 | - |
| Pot Cap-1 Maneuver | 407 | 0 | 1596 | - |
| Stage 1 | - | 0 | - | - |
| Stage 2 | 502 | 0 | - | - |
| Platoon blocked, \% |  |  |  | - |
| Mov Cap-1 Maneuver | 370 | - | 1573 | - |
| Mov Cap-2 Maneuver | 370 | - | - | - |
| Stage 1 | - | - | - | - |
| Stage 2 | 495 | - | - | - |
|  |  |  |  |  |
| Approach | EB |  | NB |  |
| HCM Control Delay, s | 15.3 |  | 0.9 |  |
| HCM LOS | C |  |  |  |
|  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBL | NBT |  |
| Capacity (veh/h) |  | 1573 | - | 370 |
| HCM Lane V/C Ratio |  | 0.045 | - |  |
| HCM Control Delay (s) |  | 7.4 | 0 | 5.3 |
| HCM Lane LOS |  | A | A | C |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | 0.2 |



## Table of Contents

Intersection Analysis Summary ..... 2
Intersection Level Of Service Report .....  3
Intersection 1: 13th/Belmont ..... 3
Turning Movement Volume: Summary ..... 5
Turning Movement Volume: Detail .....  6

Vistro File: C:I...IScen 3_HoodRiver OR281 RABs updated.vistro
Report File: X:I...IScenario 3.pdf

Intersection Analysis Summary

| ID | Intersection Name | Control Type | Method | Worst Mvmt | V/C | Delay (s/veh) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 13th/Belmont | Roundabout | HCM 6th <br> Edition | SB Thru |  | 59.3 | F |

V/C, Delay, LOS: For two-way stop, these values are taken from the movement with the worst (highest) delay value. For all other control types, they are taken for the whole intersection.

## Intersection Level Of Service Report Intersection 1: 13th/Belmont

Control Type: Analysis Method: Analysis Period:
Roundabout HCM 6th Edition 15 minutes

Intersection Setup

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |
| Turning Movement | Thru | Right | Right2 | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | Yes |  |  | Yes |  |  | Yes |  |  | Yes |  |  |

## Volumes

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 120 | 855 | 5 | 50 | 1000 | 100 | 70 | 45 | 200 | 15 | 20 | 5 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 1.00 | 2.00 | 3.00 | 3.00 | 8.00 | 2.00 | 2.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 120 | 855 | 5 | 50 | 1000 | 100 | 70 | 45 | 200 | 15 | 20 | 5 |
| Peak Hour Factor | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 33 | 235 | 1 | 14 | 275 | 27 | 19 | 12 | 55 | 4 | 5 | 1 |
| Total Analysis Volume [veh/h] | 132 | 940 | 5 | 55 | 1099 | 110 | 77 | 49 | 220 | 16 | 22 | 5 |
| Pedestrian Volume [ped/h] | 2 |  |  | 0 |  |  | 5 |  |  | 3 |  |  |

## Generated with PTV VISTRO

Version 2021 (SP 0-6)
Intersection Settings

| Number of Conflicting Circulating Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Circulating Flow Rate [veh/h] | 185 |  |  | 174 |  |  | 1194 |  |  | 1172 |  |  |
| Exiting Flow Rate [veh/h] | 1365 |  |  | 1042 |  |  | 268 |  |  | 112 |  |  |
| Demand Flow Rate [veh/h] | 120 | 855 | 5 | 50 | 1000 | 100 | 70 | 45 | 200 | 15 | 20 | 5 |
| Adjusted Demand Flow Rate [veh/h] | 132 | 940 | 5 | 55 | 1099 | 110 | 77 | 49 | 220 | 16 | 22 | 5 |

## Lanes

| Overwrite Calculated Critical Headway | No | No | No |
| :---: | :---: | :---: | :---: |
| User-Defined Critical Headway [s] | 4.00 | 4.00 | 4.00 |
| Overwrite Calculated Follow-Up Time | No | No | No |
| User-Defined Follow-Up Time [s] | 3.00 | 3.00 | 3.00 |
| A (intercept) | 1380.00 | 1380.00 | 1380.00 |
| B (coefficient) | 0.00102 | 0.00102 | 0.00102 |
| HV Adjustment Factor | 0.98 | 0.98 | 0.97 |
| Entry Flow Rate [veh/h] | 1099 | 1289 | 356 |
| Capacity of Entry and Bypass Lanes [veh/h] | 1143 | 1156 | 409 |
| Pedestrian Impedance | 1.00 | 1.00 | 1.00 |
| Capacity per Entry Lane [veh/h] | 1120 | 1134 | 418 |
| X, volume / capacity | 0.96 | 1.12 | 490 |

Movement, Approach, \& Intersection Results

| Lane LOS | E | F | F | B |
| :---: | :---: | :---: | :---: | :---: |
| 95th-Percentile Queue Length [veh] | 17.60 | 31.41 | 8.64 | 0.36 |
| 95th-Percentile Queue Length [ft] | 439.90 | 785.17 | 215.90 |  |
| Approach Delay [s/veh] | 37.69 | 81.68 | 50.74 |  |
| Approach LOS | E | F | F |  |
| Intersection Delay [s/veh] |  | 59.94 |  |  |
| Intersection LOS | F |  |  |  |

Generated with PTV VISTRO
Version 2021 (SP 0-6)

Vistro File: C:I...IScen 3_HoodRiver OR281 RABs
Scenario 1 1-lane updated.vistro
Report File: X:I...IScenario 3.pdf 1/13/2022

Turning Movement Volume: Summary

|  | Intersection Name | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Thru | Right | 2 | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| 1 | 13th/Belmont | 120 | 855 | 5 | 50 | 1000 | 100 | 70 | 45 | 200 | 15 | 20 | 5 | 2485 |

Generated with PTV VISTRO
Version 2021 (SP 0-6)

Vistro File: C:I...IScen 3_HoodRiver OR281 RABs updated.vistro
Report File: X:I...IScenario 3.pdf
1/13/2022

## Turning Movement Volume: Detail

| ID | Intersection Name | Volume Type | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Thru | Right | 2 | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| 1 | 13th/Belmont | Final Base | 120 | 855 | 5 | 50 | 1000 | 100 | 70 | 45 | 200 | 15 | 20 | 5 | 2485 |
|  |  | Growth Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | - |
|  |  | In Process | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Net New Trips | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Other | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Future Total | 120 | 855 | 5 | 50 | 1000 | 100 | 70 | 45 | 200 | 15 | 20 | 5 | 2485 |

APPENDIX D: ALTERNATIVE TRAFFIC OPERATIONS (MITIGATED)

c Critical Lane Group




HCM 6th TWSC
4: 13th St \& A St



|  | 4 | $\rightarrow$ | 7 | 7 |  | 4 | 4 | 4 | 7 | ( | $\ddagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  | ${ }^{1}$ | $\uparrow$ |  |
| Traffic Volume (veh/h) | 70 | 45 | 200 | 0 | 170 | 5 | 0 | 565 | 5 | 50 | 930 | 60 |
| Future Volume (veh/h) | 70 | 45 | 200 | 0 | 170 | 5 | 0 | 565 | 5 | 50 | 930 | 60 |
| Initial Q $(\mathrm{Qb})$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 0.99 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1856 | 0 | 1870 | 1870 | 0 | 1870 | 1870 | 1870 | 1870 | 1885 |
| Adj Flow Rate, veh/h | 77 | 49 | 72 | 0 | 187 | 5 | 0 | 621 | 5 | 55 | 1022 | 66 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Percent Heavy Veh, \% | 2 | 3 | 3 | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 1 |
| Cap, veh/h | 208 | 127 | 186 | 0 | 340 | 9 | 0 | 1327 | 11 | 579 | 1245 | 80 |
| Arrive On Green | 0.19 | 0.19 | 0.18 | 0.00 | 0.19 | 0.18 | 0.00 | 0.72 | 0.71 | 0.71 | 0.72 | 0.71 |
| Sat Flow, veh/h | 1293 | 676 | 994 | 0 | 1813 | 48 | 0 | 1853 | 15 | 868 | 1737 | 112 |
| Grp Volume(v), veh/h | 77 | 0 | 121 | 0 | 0 | 192 | 0 | 0 | 626 | 55 | 0 | 1088 |
| Grp Sat Flow(s),veh/h/ln | 1293 | 0 | 1670 | 0 | 0 | 1862 | 0 | 0 | 1868 | 868 | 0 | 1850 |
| Q Serve(g_s), s | 4.8 | 0.0 | 5.3 | 0.0 | 0.0 | 7.8 | 0.0 | 0.0 | 11.9 | 2.4 | 0.0 | 33.7 |
| Cycle Q Clear(g_c), s | 12.6 | 0.0 | 5.3 | 0.0 | 0.0 | 7.8 | 0.0 | 0.0 | 11.9 | 14.3 | 0.0 | 33.7 |
| Prop In Lane | 1.00 |  | 0.60 | 0.00 |  | 0.03 | 0.00 |  | 0.01 | 1.00 |  | 0.06 |
| Lane Grp Cap(c), veh/h | 208 | 0 | 313 | 0 | 0 | 349 | 0 | 0 | 1338 | 579 | 0 | 1325 |
| V/C Ratio(X) | 0.37 | 0.00 | 0.39 | 0.00 | 0.00 | 0.55 | 0.00 | 0.00 | 0.47 | 0.10 | 0.00 | 0.82 |
| Avail Cap(c_a), veh/h | 323 | 0 | 462 | 0 | 0 | 515 | 0 | 0 | 1997 | 885 | 0 | 1978 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 36.3 | 0.0 | 29.8 | 0.0 | 0.0 | 30.6 | 0.0 | 0.0 | 5.0 | 8.3 | 0.0 | 8.1 |
| Incr Delay (d2), s/veh | 0.8 | 0.0 | 0.6 | 0.0 | 0.0 | 1.0 | 0.0 | 0.0 | 0.2 | 0.1 | 0.0 | 1.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.5 | 0.0 | 2.2 | 0.0 | 0.0 | 3.5 | 0.0 | 0.0 | 3.7 | 0.4 | 0.0 | 10.8 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 37.1 | 0.0 | 30.3 | 0.0 | 0.0 | 31.6 | 0.0 | 0.0 | 5.2 | 8.4 | 0.0 | 9.6 |
| LnGrp LOS | D | A | C | A | A | C | A | A | A | A | A | A |
| Approach Vol, veh/h |  | 198 |  |  | 192 |  |  | 626 |  |  | 1143 |  |
| Approach Delay, s/veh |  | 33.0 |  |  | 31.6 |  |  | 5.2 |  |  | 9.6 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | A |  |
| Timer - Assigned Phs |  | 2 |  | 4 |  | 6 |  | 8 |  |  |  |  |
| Phs Duration (G+Y+Rc), s |  | 63.6 |  | 19.6 |  | 63.6 |  | 19.6 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s |  | 4.5 |  | 4.5 |  | 4.5 |  | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s |  | 88.5 |  | 22.5 |  | 88.5 |  | 22.5 |  |  |  |  |
| Max Q Clear Time (g_c+11), s |  | 13.9 |  | 14.6 |  | 35.7 |  | 9.8 |  |  |  |  |
| Green Ext Time (p_c), s |  | 7.0 |  | 0.5 |  | 23.4 |  | 0.6 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 12.4 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | B |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 8 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | * |  |  | \$ |  |  | \& |  |
| Traffic Vol, veh/h | 45 | 25 | 5 | 5 | 10 | 5 | 150 | 750 | 40 | 5 | 175 | 30 |
| Future Vol, veh/h | 45 | 25 | 5 | 5 | 10 | 5 | 150 | 750 | 40 | 5 | 175 | 30 |
| Conflicting Peds, \#/hr | 13 | 0 | 0 | 0 | 0 | 13 | 1 | 0 | 8 | 8 | 0 | 1 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 3 | 2 | 2 | 2 | 17 | 2 | 2 | 3 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 47 | 26 | 5 | 5 | 11 | 5 | 158 | 789 | 42 | 5 | 184 | 32 |



HCM 6th TWSC
7: 12th St \& A St/Wilson

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.7 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \& |  |  | * |  |  | $\ddagger$ |  |  | \$ |  |
| Traffic Vol, veh/h | 10 | 15 | 5 | 5 | 35 | 20 | 30 | 730 | 50 | 10 | 210 | 5 |
| Future Vol, veh/h | 10 | 15 | 5 | 5 | 35 | 20 | 30 | 730 | 50 | 10 | 210 | 5 |
| Conflicting Peds, \#/hr | 15 | 0 | 20 | 20 | 0 | 15 | 8 | 0 | 13 | 13 | 0 | 8 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 3 | 2 | 2 | 3 | 6 | 2 | 2 | 2 |
| Mvmt Flow | 11 | 16 | 5 | 5 | 38 | 22 | 32 | 785 | 54 | 11 | 226 | 5 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.4 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | F |  |  | - |
| Traffic Vol, veh/h | 35 | 65 | 745 | 80 | 10 | 225 |
| Future Vol, veh/h | 35 | 65 | 745 | 80 | 10 | 225 |
| Conflicting Peds, \#/hr | 15 | 0 | 0 | 23 | 23 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 91 | 91 | 91 | 91 | 91 | 91 |
| Heavy Vehicles, \% | 2 | 2 | 3 | 2 | 2 | 2 |
| Mvmt Flow | 38 | 71 | 819 | 88 | 11 | 247 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1170 | 886 | 0 | 0 | 930 | 0 |
| Stage 1 | 886 | - | - | - | - | - |
| Stage 2 | 284 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 213 | 343 | - | - | 736 | - |
| Stage 1 | 403 | - | - | - | - | - |
| Stage 2 | 764 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 202 | 335 | - | - | 720 | - |
| Mov Cap-2 Maneuver | 202 | - | - | - | - | - |
| Stage 1 | 394 | - | - | - | - | - |
| Stage 2 | 740 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 26.9 |  | 0 |  | 0.4 |  |
| HCM LOS | D |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 272 | 720 | - |
| HCM Lane V/C Ratio |  | - | - | 0.404 | 0.015 | - |
| HCM Control Delay (s) |  | - | - | 26.9 | 10.1 | 0 |
| HCM Lane LOS |  | - | - | D | B | A |
| HCM 95th \%tile Q(veh) |  | - | - | 1.9 | 0 | - |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| $l$ |  |  |  |  |  |  |



Generated with PTV VISTRO
Version 2021 (SP 0-6)

Vistro File: X:I...IScen 1_HoodRiver OR281 RABs_Mit.vistro
Report File: X:I...IScenario 1 - Mit v2.pdf

Intersection Analysis Summary

| ID | Intersection Name | Control Type | Method | Worst Mvmt | V/C | Delay (s/veh) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 13th/Belmont | Roundabout | HCM 6th <br> Edition | EB Right |  | 33.4 | D |
| 3 | 13th / May | Roundabout | HCM 6th <br> Edition | WB Left |  | 16.5 | C |

V/C, Delay, LOS: For two-way stop, these values are taken from the movement with the worst (highest) delay value. For all other control types, they are taken for the whole intersection.

## Intersection Level Of Service Report Intersection 1: 13th/Belmont

Control Type: Analysis Method: Analysis Period:

## Roundabout HCM 6th Edition 15 minutes

Delay (sec / veh):
Level Of Service:
33.4

D

Intersection Setup

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach |  | orthboun |  |  | outhbound |  |  | astboun |  |  | estboun |  |
| Lane Configuration |  | $\ddagger$ |  |  | $\uparrow$ |  |  | $\leftrightarrows$ |  |  |  |  |
| Turning Movement | Thru | Right | Right2 | Left2 | Left | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | Yes |  |  | Yes |  |  | Yes |  |  | Yes |  |  |

## Volumes

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 125 | 565 | 5 | 50 | 930 | 60 | 115 | 45 | 200 | 0 | 0 | 0 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 1.00 | 2.00 | 3.00 | 3.00 | 8.00 | 2.00 | 2.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 125 | 565 | 5 | 50 | 930 | 60 | 115 | 45 | 200 | 0 | 0 | 0 |
| Peak Hour Factor | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 34 | 155 | 1 | 14 | 255 | 16 | 32 | 12 | 55 | 0 | 0 | 0 |
| Total Analysis Volume [veh/h] | 137 | 621 | 5 | 55 | 1022 | 66 | 126 | 49 | 220 | 0 | 0 | 0 |
| Pedestrian Volume [ped/h] | 2 |  |  | 0 |  |  | 5 |  |  | 3 |  |  |

## Generated with PTV VISTRO

Version 2021 (SP 0-6)

## Intersection Settings

| Number of Conflicting Circulating Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Circulating Flow Rate [veh/h] | 235 |  |  | 140 |  |  | 1099 |  |  | 902 |  |  |
| Exiting Flow Rate [veh/h] | 1269 |  |  | 762 |  |  | 206 |  |  | 112 |  |  |
| Demand Flow Rate [veh/h] | 125 | 565 | 5 | 50 | 930 | 60 | 115 | 45 | 200 | 0 | 0 | 0 |
| Adjusted Demand Flow Rate [veh/h] | 137 | 621 | 5 | 55 | 1022 | 66 | 126 | 49 | 220 | 0 | 0 | 0 |

Lanes

| Overwrite Calculated Critical Headway | No | No | No |  |
| :---: | :---: | :---: | :---: | :---: |
| User-Defined Critical Headway [s] | 4.00 | 4.00 | No | No |
| Overwrite Calculated Follow-Up Time | No | 3.00 | 3.00 |  |
| User-Defined Follow-Up Time [s] | 3.00 | 1380.00 | 1380.00 | 0.00102 |
| A (intercept) | 1380.00 | 0.00102 | 0.97 | 406 |
| B (coefficient) | 0.00102 | 0.98 | 451 |  |
| HV Adjustment Factor | 0.98 | 1166 | 1197 | 1.00 |
| Entry Flow Rate [veh/h] | 779 | 1086 | 1.00 | 439 |
| Capacity of Entry and Bypass Lanes [veh/h | 1.00 | 0.97 |  |  |
| Pedestrian Impedance | 1065 | 0.72 | 0.90 |  |
| Capacity per Entry Lane [veh/h] | X, volume / capacity |  |  |  |

Movement, Approach, \& Intersection Results

| Lane LOS | C | E | F |  |
| :---: | :---: | :---: | :---: | :---: |
| 95th-Percentile Queue Length [veh] | 6.48 | 18.86 | 9.76 |  |
| 95th-Percentile Queue Length [ft] | 162.08 | 471.57 | 244.05 |  |
| Approach Delay [s/veh] | 15.03 | 39.15 | E | F |
| Approach LOS | C | 0.00 |  |  |
| Intersection Delay [s/veh] |  | D |  |  |
| Intersection LOS |  | D |  |  |

## Intersection Level Of Service Report Intersection 3: 13th / May

Control Type: Analysis Method: Analysis Period:

Roundabout HCM 6th Edition 15 minutes

Delay (sec / veh):
Level Of Service:

Intersection Setup

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach |  | orthboun |  |  | outhbound |  |  | astbound |  |  | estbound |  |
| Lane Configuration |  | $\uparrow$ |  |  | $4 F$ |  |  | $\leftrightarrows$ |  |  | $\uparrow$ |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  |
| Grade [\%] | -4.50 |  |  | 4.50 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | Yes |  |  | Yes |  |  | Yes |  |  | Yes |  |  |

## Volumes

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 125 | 500 | 10 | 75 | 625 | 55 | 50 | 35 | 80 | 310 | 145 | 40 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 3.00 | 2.00 | 2.00 | 2.00 | 2.00 | 3.00 | 1.00 | 2.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 125 | 500 | 10 | 75 | 625 | 55 | 50 | 35 | 80 | 310 | 145 | 40 |
| Peak Hour Factor | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 33 | 133 | 3 | 20 | 166 | 15 | 13 | 9 | 21 | 82 | 39 | 11 |
| Total Analysis Volume [veh/h] | 133 | 532 | 11 | 80 | 665 | 59 | 53 | 37 | 85 | 330 | 154 | 43 |
| Pedestrian Volume [ped/h] | 10 |  |  | 1 |  |  | 9 |  |  | 7 |  |  |

## Generated with PTV VISTRO

Version 2021 (SP 0-6)

## Intersection Settings

| Number of Conflicting Circulating Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Circulating Flow Rate [veh/h] | 173 |  |  | 631 |  |  | 1106 |  |  | 732 |  |  |
| Exiting Flow Rate [veh/h] | 1112 |  |  | 641 |  |  | 351 |  |  | 131 |  |  |
| Demand Flow Rate [veh/h] | 125 | 500 | 10 | 75 | 625 | 55 | 50 | 35 | 80 | 310 | 145 | 40 |
| Adjusted Demand Flow Rate [veh/h] | 133 | 532 | 11 | 80 | 665 | 59 | 53 | 37 | 85 | 330 | 154 | 43 |

Lanes

| Overwrite Calculated Critical Headway | No | No | No | No |
| :---: | :---: | :---: | :---: | :---: |
| User-Defined Critical Headway [s] | 4.00 | 4.00 | 4.00 | 4.00 |
| Overwrite Calculated Follow-Up Time | No | No | No | No |
| User-Defined Follow-Up Time [s] | 3.00 | 3.00 | 3.00 | 3.00 |
| A (intercept) | 1380.00 | 1420.00 | 1420.00 | 1380.00 |
| B (coefficient) | 0.00102 | 0.00091 | 0.00091 | 0.00102 |
| HV Adjustment Factor | 0.98 | 0.97 | 0.97 | 0.98 |
| Entry Flow Rate [veh/h] | 690 | 389 | 439 | 179 |
| Capacity of Entry and Bypass Lanes [veh/h | 1157 | 800 | 800 | 4.00 |
| Pedestrian Impedance | 1.00 | 1.00 | 1.00 | 447 |
| Capacity per Entry Lane [veh/h] | 1133 | 777 | 777 | 1.00 |
| X, volume / capacity | 0.60 | 0.49 | 0.55 | 438 |

Movement, Approach, \& Intersection Results

| Lane LOS | B | B | B | C | D |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 95th-Percentile Queue Length [veh] | 4.15 | 2.70 | 3.39 | 1.89 | 8.73 |
| 95th-Percentile Queue Length [ft] | 103.63 | 67.41 | 84.65 | 47.25 | 218.17 |
| Approach Delay [s/veh] | 10.76 |  |  | 15.60 | 30.82 |
| Approach LOS | B |  |  | C | D |
| Intersection Delay [s/veh] | 16.51 |  |  |  |  |
| Intersection LOS | C |  |  |  |  |

Generated with PTV VISTRO
Version 2021 (SP 0-6)

Vistro File: X:I...IScen 1_HoodRiver OR281 RABs_Mit.vistro
Report File: X:I...IScenario 1 - Mit v2.pdf

Turning Movement Volume: Summary

| ID | Intersection Name | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Thru | Right | 2 | 2 | Left | Right | Left | Thru | Right |  |
| 1 | 13th/Belmont | 125 | 565 | 5 | 50 | 930 | 60 | 115 | 45 | 200 | 2095 |


| ID | Intersection Name | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| 3 | 13th / May | 125 | 500 | 10 | 75 | 625 | 55 | 50 | 35 | 80 | 310 | 145 | 40 | 2050 |

Vistro File: X:I...IScen 1_HoodRiver OR281 RABs_Mit.vistro

Turning Movement Volume: Detail

| ID | Intersection Name | Volume Type | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Thru | Right | 2 | 2 | Left | Right | Left | Thru | Right |  |
| 1 | 13th/Belmont | Final Base | 125 | 565 | 5 | 50 | 930 | 60 | 115 | 45 | 200 | 2095 |
|  |  | Growth Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | - |
|  |  | In Process | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Net New Trips | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Other | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Future Total | 125 | 565 | 5 | 50 | 930 | 60 | 115 | 45 | 200 | 2095 |


| ID | Intersection Name | Volume Type | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| 3 | 13th / May | Final Base | 125 | 500 | 10 | 75 | 625 | 55 | 50 | 35 | 80 | 310 | 145 | 40 | 2050 |
|  |  | Growth Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | - |
|  |  | In Process | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Net New Trips | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Other | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Future Total | 125 | 500 | 10 | 75 | 625 | 55 | 50 | 35 | 80 | 310 | 145 | 40 | 2050 |


c Critical Lane Group







| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 23 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | * $\uparrow$ |  |  |  |  |  |
| Traffic Vol, veh/h | 75 | 25 | 0 | 0 | 15 | 5 | 160 | 1225 | 65 | 0 | 0 | 0 |  |
| Future Vol, veh/h | 75 | 25 | 0 | 0 | 15 | 5 | 160 | 1225 | 65 | 0 | 0 | 0 |  |
| Conflicting Peds, \#hr | 13 | 0 | 0 | 0 | 0 | 13 | 1 | 0 | 8 | 8 | 0 | 1 |  |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Stop | Stop | Stop |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - |  | None |  |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | - | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |  |
| Heavy Vehicles, \% | 3 | 2 | 2 | 2 | 17 | 2 | 2 | 3 | 2 | 2 | 2 | 2 |  |
| Mvmt Flow | 79 | 26 | 0 | 0 | 16 | 5 | 168 | 1289 | 68 | 0 | 0 | 0 |  |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Minor2 |  | Major1 |  |
| :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1632 | - | 15 | 0 |
| Stage 1 | 15 | - | - | - |
| Stage 2 | 1617 | - | - | - |
| Critical Hdwy | 6.42 | - | 4.13 | - |
| Critical Hdwy Stg 1 | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - |
| Follow-up Hdwy | 3.518 |  | 2.227 | - |
| Pot Cap-1 Maneuver | 111 | 0 | 1596 | - |
| Stage 1 | - | 0 | - | - |
| Stage 2 | 178 | 0 | - | - |
| Platoon blocked, \% |  |  |  | - |
| Mov Cap-1 Maneuver | 70 | - | 1573 | - |
| Mov Cap-2 Maneuver | 70 | - | - | - |
| Stage 1 | - | - | - | - |
| Stage 2 | 176 | - | - | - |
|  |  |  |  |  |
| Approach | EB |  | NB |  |
| HCM Control Delay, s | 134.3 |  | 0.8 |  |
| HCM LOS | F |  |  |  |
|  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBL NBT EBLn1 |  |  |
| Capacity (veh/h) |  | 1573 | - | 70 |
| HCM Lane V/C Ratio |  | 0.098 | - |  |
| HCM Control Delay (s) |  | 7.5 | 0 |  |
| HCM Lane LOS |  | A | A | F |
| HCM 95th \%tile Q(veh) |  | 0.3 | - | 3.2 |




| Timer - Assigned Phs | 6 |
| :--- | ---: |
| Phs Duration (G+Y+Rc), s | 31.4 |
| Change Period (Y+Rc), s | 4.0 |
| Max Green Setting (Gmax), s | 38.0 |
| Max Q Clear Time (g_c +11 ), s | 26.9 |
| Green Ext Time (p_c), s | 0.5 |
| Intersection Summary |  |
| HCM 6th Ctrl Delay | 48.7 |
| HCM 6th LOS | D |

## Table of Contents

Intersection Analysis Summary ..... 2
Intersection Level Of Service Report ..... 3
Intersection 1: 13th/Belmont ..... 3
Intersection 2: 13th/12th ..... 5
Intersection 3: 13th/May ..... 7
Turning Movement Volume: Summary ..... 9
Turning Movement Volume: Detail ..... 10

Vistro File: C:I...IScen 2_HoodRiver OR281 RABs_Mit.vistro
Report File: X:I...IScenario 2 - Mit.pdf
Intersection Analysis Summary

| ID | Intersection Name | Control Type | Method | Worst Mvmt | V/C | Delay (s/veh) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 13th/Belmont | Roundabout | HCM 6th <br> Edition | EB Thru |  | 21.6 | C |
| 2 | 13 th/12th | Roundabout | HCM 6th <br> Edition | NB Thru |  | 32.4 | D |
| 3 | 13 th/May | Roundabout | HCM 6th <br> Edition | WB Right |  | 16.8 | C |

V/C, Delay, LOS: For two-way stop, these values are taken from the movement with the worst (highest) delay value. For all other control types, they are taken for the whole intersection.

## Intersection Level Of Service Report Intersection 1: 13th/Belmont

Control Type:
Analysis Method: Analysis Period:
Roundabout HCM 6th Edition 15 minutes

Intersection Setup

| Name |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach |  |  |  |  |  |  |
| Lane Configuration |  |  |  |  |  |  |
| Turning Movement | Thru | Right | Left | Thru | Left | Thru |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 1 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  | 25.00 |  | 25.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | Yes |  | Yes |  | Yes |  |

## Volumes

| Name |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 1010 | 200 | 0 | 375 | 165 | 0 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 8.00 | 2.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 1010 | 200 | 0 | 375 | 165 | 0 |
| Peak Hour Factor | 0.9100 | 0.9100 | 1.0000 | 0.9100 | 0.9100 | 1.0000 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 277 | 55 | 0 | 103 | 45 | 0 |
| Total Analysis Volume [veh/h] | 1110 | 220 | 0 | 412 | 181 | 0 |
| Pedestrian Volume [ped/h] | 0 |  | 3 |  | 0 |  |

## Generated with PTV VISTRO

Version 2021 (SP 0-6)

## Intersection Settings

| Number of Conflicting Circulating Lanes | 1 |  | 1 |  | 1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Circulating Flow Rate [veh/h] | 195 |  | 1132 |  | 0 |  |
| Exiting Flow Rate [veh/h] | 0 |  | 420 |  | 1552 |  |
| Demand Flow Rate [veh/h] | 1010 | 200 | 0 | 375 | 165 | 0 |
| Adjusted Demand Flow Rate [veh/h] | 1110 | 220 | 0 | 412 | 181 | 0 |

## Lanes

| Overwrite Calculated Critical Headway | No | No | No | No |
| :---: | :---: | :---: | :---: | :---: |
| User-Defined Critical Headway [s] | 4.00 | 4.00 | 4.00 | 4.00 |
| Overwrite Calculated Follow-Up Time | No | No | No | No |
| User-Defined Follow-Up Time [s] | 3.00 | 3.00 | 3.00 | 3.00 |
| A (intercept) | 1420.00 | 1420.00 | 1380.00 | 1380.00 |
| B (coefficient) | 0.00091 | 0.00091 | 0.00102 | 0.00102 |
| HV Adjustment Factor | 0.98 | 0.98 | 0.98 | 0.93 |
| Entry Flow Rate [veh/h] | 638 | 719 | 421 | 196 |
| Capacity of Entry and Bypass Lanes [veh/h] | 1189 | 1189 | 435 | 1380 |
| Pedestrian Impedance | 1.00 | 1.00 | 1.00 | 1.00 |
| Capacity per Entry Lane [veh/h] | 1166 | 1166 | 427 | 1278 |
| X, volume / capacity | 0.54 | 0.60 | 0.97 | 0.14 |

Movement, Approach, \& Intersection Results

| Lane LOS | A | B | F | A |
| :---: | :---: | :---: | :---: | :---: |
| 95th-Percentile Queue Length [veh] | 3.31 | 4.28 | 11.57 | 0.49 |
| 95th-Percentile Queue Length [ft] | 82.73 | 106.89 | 289.17 | 12.33 |
| Approach Delay [s/veh] | 10.05 |  | 66.79 | 3.99 |
| Approach LOS | B |  | F | A |
| Intersection Delay [s/veh] | 21.63 |  |  |  |
| Intersection LOS | C |  |  |  |

## Intersection Level Of Service Report Intersection 2: 13th/12th

Control Type:
Analysis Method:
Analysis Period:
Roundabout HCM 6th Edition 15 minutes

Intersection Setup

| Name |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach |  |  |  |  |  |  |
| Lane Configuration |  |  |  |  |  |  |
| Turning Movement | Left | Thru | Thru | Right | Left | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 1 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  | 30.00 |  | 25.00 |  |
| Grade [\%] | 0.00 |  | 0.00 |  | 0.00 |  |
| Crosswalk | Yes |  | Yes |  | No |  |

## Volumes

| Name |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 160 | 1290 | 125 | 85 | 100 | 1385 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 160 | 1290 | 125 | 85 | 100 | 1385 |
| Peak Hour Factor | 0.9500 | 0.9500 | 0.9100 | 0.9100 | 0.9500 | 0.9500 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 42 | 339 | 34 | 23 | 26 | 364 |
| Total Analysis Volume [veh/h] | 168 | 1358 | 137 | 93 | 105 | 1458 |
| Pedestrian Volume [ped/h] | 0 |  | 13 |  | 0 |  |

## Generated with PTV VISTRO

Version 2021 (SP 0-6)
Intersection Settings

| Number of Conflicting Circulating Lanes | 2 |  | 1 |  | 1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Circulating Flow Rate [veh/h] | 107 |  | 171 |  | 0 |  |
| Exiting Flow Rate [veh/h] | 1487 |  | 1492 |  | 171 |  |
| Demand Flow Rate [veh/h] | 160 | 1290 | 0 | 0 | 100 | 1385 |
| Adjusted Demand Flow Rate [veh/h] | 168 | 1358 | 0 | 0 | 105 | 1458 |

## Lanes

| Overwrite Calculated Critical Headway | No | No |  | No | No |
| :---: | :---: | :---: | :---: | :---: | :---: |
| User-Defined Critical Headway [s] | 4.00 | 4.00 |  | 4.00 | 4.00 |
| Overwrite Calculated Follow-Up Time | No | No |  | No | No |
| User-Defined Follow-Up Time [s] | 3.00 | 3.00 |  | 3.00 | 3.00 |
| A (intercept) | 1350.00 | 1420.00 |  | 1420.00 | 1420.00 |
| B (coefficient) | 0.00092 | 0.00085 |  | 0.00091 | 0.00091 |
| HV Adjustment Factor | 0.98 | 0.98 |  | 0.98 | 0.98 |
| Entry Flow Rate [veh/h] | 172 | 1386 |  | 750 | 845 |
| Capacity of Entry and Bypass Lanes [veh/h] | 1224 | 1297 |  | 1420 | 1420 |
| Pedestrian Impedance | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Capacity per Entry Lane [veh/h] | 1200 | 1272 |  | 1393 | 1393 |
| X, volume / capacity | 0.14 | 1.07 |  | 0.53 | 0.60 |

Movement, Approach, \& Intersection Results

| Lane LOS | A | F |  | A | A |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 95th-Percentile Queue Length [veh] | 0.49 | 28.65 |  | 3.23 | 4.16 |
| 95th-Percentile Queue Length [ft] | 12.17 | 716.21 |  | 80.63 | 104.06 |
| Approach Delay [s/veh] | 56.72 |  | 0.00 | 8.72 |  |
| Approach LOS | F |  | A | A |  |
| Intersection Delay [s/veh] | 32.43 |  |  |  |  |
| Intersection LOS | D |  |  |  |  |

## Intersection Level Of Service Report Intersection 3: 13th/May

Control Type: Analysis Method: Analysis Period:

Roundabout HCM 6th Edition 15 minutes

Delay (sec / veh):
16.8

Level Of Service:

Intersection Setup

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration |  |  |  | $4 F$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 30.00 |  |  | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  |
| Grade [\%] | 0.00 |  |  | -4.50 |  |  | 4.50 |  |  | 0.00 |  |  |
| Crosswalk | Yes |  |  | Yes |  |  | Yes |  |  | Yes |  |  |

## Volumes

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 0 | 0 | 0 | 25 | 700 | 55 | 50 | 35 | 80 | 335 | 170 | 540 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 3.00 | 2.00 | 2.00 | 1.00 | 3.00 | 2.00 | 4.00 | 1.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 0 | 0 | 0 | 25 | 700 | 55 | 50 | 35 | 80 | 335 | 170 | 540 |
| Peak Hour Factor | 1.0000 | 1.0000 | 1.0000 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 0 | 0 | 0 | 7 | 186 | 15 | 13 | 9 | 21 | 89 | 45 | 144 |
| Total Analysis Volume [veh/h] | 0 | 0 | 0 | 27 | 745 | 59 | 53 | 37 | 85 | 356 | 181 | 574 |
| Pedestrian Volume [ped/h] | 10 |  |  | 1 |  |  | 9 |  |  | 7 |  |  |

## Generated with PTV VISTRO

Version 2021 (SP 0-6)
Intersection Settings

| Number of Conflicting Circulating Lanes | 1 |  |  | 1 |  |  | 2 |  |  | 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Circulating Flow Rate [veh/h] | 119 |  |  | 551 |  |  | 1158 |  |  | 54 |  |  |
| Exiting Flow Rate [veh/h] | 1218 |  |  | 634 |  |  | 248 |  |  | 65 |  |  |
| Demand Flow Rate [veh/h] | 0 | 0 | 0 | 25 | 700 | 55 | 50 | 35 | 80 | 335 | 170 | 540 |
| Adjusted Demand Flow Rate [veh/h] | 0 | 0 | 0 | 27 | 745 | 59 | 53 | 37 | 85 | 356 | 181 | 574 |

## Lanes

| Overwrite Calculated Critical Headway | No | No | No | No |
| :---: | :---: | :---: | :---: | :---: |
| User-Defined Critical Headway [s] | 4.00 | 4.00 | 4.00 | 4.00 |
| Overwrite Calculated Follow-Up Time | No | No | No | No |
| User-Defined Follow-Up Time [s] | 3.00 | 3.00 | 3.00 | 3.00 |
| A (intercept) | 1420.00 | 1420.00 | 1420.00 | 1380.00 |
| B (coefficient) | 0.00091 | 0.00091 | 0.00085 | 0.00102 |
| HV Adjustment Factor | 0.97 | 0.97 | 0.98 | 0.98 |
| Entry Flow Rate [veh/h] | 403 | 454 | 179 | 1131 |
| Capacity of Entry and Bypass Lanes [veh/h] | 860 | 860 | 531 | 1306 |
| Pedestrian Impedance | 1.00 | 1.00 | 1.00 | 1.00 |
| Capacity per Entry Lane [veh/h] | 835 | 835 | 519 | 1282 |
| X, volume / capacity | 0.47 | 0.53 | 0.34 | 0.87 |

Movement, Approach, \& Intersection Results

| Lane LOS |  | B | B | B | C |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 95th-Percentile Queue Length [veh] |  | 2.52 | 3.15 | 1.48 | 12.36 |
| 95th-Percentile Queue Length [ft] |  | 63.11 | 78.72 | 36.90 | 309.09 |
| Approach Delay [s/veh] | 0.00 |  |  | 12.11 | 21.83 |
| Approach LOS | A |  |  | B | C |
| Intersection Delay [s/veh] | 16.80 |  |  |  |  |
| Intersection LOS | C |  |  |  |  |

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Version 2021 (SP 0-6)

Vistro File: C:\...IScen 2_HoodRiver OR281 RABs_Mit.vistro

Scenario 1 Scen2 - Mit
1/13/2022

Turning Movement Volume: Summary

| ID | Intersection Name | Southbound |  | Eastbound |  | Westbound |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Thru | Right | Left | Thru | Left | Thru |  |
| 1 | 13th/Belmont | 1010 | 200 | 0 | 375 | 165 | 0 | 1750 |


| ID | Intersection Name | Northbound |  | Eastbound |  | Total <br> Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Left | Thru | Left | Right |  |
| 2 | 13th/12th | 160 | 1290 | 100 | 1385 | 2935 |


| ID | Intersection Name | Southbound |  |  | Eastbound |  |  | Westbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| 3 | 13th/May | 25 | 700 | 55 | 50 | 35 | 80 | 335 | 170 | 540 | 1990 |

Vistro File: C:I...IScen 2_HoodRiver OR281 RABs_Mit.vistro
Report File: X:I...IScenario 2 - Mit.pdf

Turning Movement Volume: Detail

| ID | Intersection Name | Volume Type | Southbound |  | Eastbound |  | Westbound |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Thru | Right | Left | Thru | Left | Thru |  |
| 1 | 13th/Belmont | Final Base | 1010 | 200 | 0 | 375 | 165 | 0 | 1750 |
|  |  | Growth Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | - |
|  |  | In Process | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Net New Trips | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Other | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Future Total | 1010 | 200 | 0 | 375 | 165 | 0 | 1750 |


| ID | Intersection Name | Volume Type | Northbound |  | Eastbound |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Left | Thru | Left | Right |  |
| 2 | 13th/12th | Final Base | 160 | 1290 | 100 | 1385 | 2935 |
|  |  | Growth Factor | 1.00 | 1.00 | 1.00 | 1.00 | - |
|  |  | In Process | 0 | 0 | 0 | 0 | 0 |
|  |  | Net New Trips | 0 | 0 | 0 | 0 | 0 |
|  |  | Other | 0 | 0 | 0 | 0 | 0 |
|  |  | Future Total | 160 | 1290 | 100 | 1385 | 2935 |


| ID | Intersection Name | Volume Type | Southbound |  |  | Eastbound |  |  | Westbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| 3 | 13th/May | Final Base | 25 | 700 | 55 | 50 | 35 | 80 | 335 | 170 | 540 | 1990 |
|  |  | Growth Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | - |
|  |  | In Process | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Net New Trips | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Other | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Future Total | 25 | 700 | 55 | 50 | 35 | 80 | 335 | 170 | 540 | 1990 |


c Critical Lane Group




HCM 6th TWSC
4: 13th St \& A St


| Major/Minor | Minor2 |  |  | Minor1 |  |  | Major1 |  |  | Major2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 2200 | 2183 | 1166 | 2190 | 2186 | 965 | 1167 | 0 | 0 | O 959 | 0 | 0 |
| Stage 1 | 1214 | 1214 |  | 967 | 967 | - | - | - |  | - - | - | - |
| Stage 2 | 986 | 969 | - | 1223 | 1219 | - | - | - |  | - - | - | - |
| Critical Hdwy | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 | 4.12 | - |  | 4.12 | - | - |
| Critical Hdwy Stg 1 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - |  | - - | - | - |
| Critical Hdwy Stg 2 | 6.12 | 5.52 | - | 6.12 | 5.52 | - | - | - |  | - - | - | - |
| Follow-up Hdwy | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 | 2.218 | - |  | - 2.218 | - | - |
| Pot Cap-1 Maneuver | 32 | 46 | 236 | ~33 | 46 | 309 | 599 | - |  | 717 | - | - |
| Stage 1 | 222 | 254 |  | 306 | 333 | - | - | - |  | - - | - | - |
| Stage 2 | 298 | 332 | - | 219 | 253 | - | - | - |  | - - | - | - |
| Platoon blocked, \% |  |  |  |  |  |  |  | - |  | - | - | - |
| Mov Cap-1 Maneuver | 21 | 44 | 234 | $\sim 25$ | 44 | 305 | 597 | - |  | 712 | - | - |
| Mov Cap-2 Maneuver | 21 | 44 | - | $\sim 25$ | 44 | - | - | - |  | - - | - | - |
| Stage 1 | 220 | 244 | - | 301 | 328 | - | - | - |  | - - | - | - |
| Stage 2 | 260 | 327 | - | 197 | 243 | - | - | - |  | - - | - | - |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 163 |  |  | \$ 849.1 |  |  | 0.1 |  |  | 0.2 |  |  |
| HCM LOS | F |  |  | F |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minor Lane/Major Mvm |  | NBL | NBT | NBR | EBLn1 | NBLn1 | SBL | SBT | SBR |  |  |  |
| Capacity (veh/h) |  | 597 | - |  | 41 | 36 | 712 | - |  |  |  |  |
| HCM Lane V/C Ratio |  | 0.009 | - |  | 0.513 | 2.339 | 0.037 | - |  |  |  |  |
| HCM Control Delay (s) |  | 11.1 | - | - | 1638 | 849.1 | 10.2 | - |  | - |  |  |
| HCM Lane LOS |  | B | - | - | F | F | B | - |  | - |  |  |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | 1.8 | 9.4 | 0.1 | - |  | - |  |  |
| $\xrightarrow{\text { Notes }}$ |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | \$: Delay exceeds 300s |  |  |  | +: Computation Not Defined |  |  |  | *: All major volume in platoon |  |  |


|  | 4 | $\rightarrow$ | 7 | 7 |  | 4 | 4 | 4 | \% | ( | $\ddagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  |  | $\uparrow$ |  |  | 个 |  | ${ }^{1 /}$ | $\uparrow$ |  |
| Traffic Volume (veh/h) | 70 | 45 | 200 | 0 | 140 | 5 | 0 | 855 | 5 | 50 | 1010 | 100 |
| Future Volume (veh/h) | 70 | 45 | 200 | 0 | 140 | 5 | 0 | 855 | 5 | 50 | 1010 | 100 |
| Initial Q $(\mathrm{Qb})$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 0.99 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach |  | No |  |  | No |  |  | No |  |  | No |  |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1856 | 0 | 1870 | 1870 | 0 | 1870 | 1870 | 1870 | 1870 | 1885 |
| Adj Flow Rate, veh/h | 77 | 49 | 72 | 0 | 154 | 5 | 0 | 940 | 5 | 55 | 1110 | 110 |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Percent Heavy Veh, \% | 2 | 3 | 3 | 0 | 2 | 2 | 0 | 2 | 2 | 2 | 2 | 1 |
| Cap, veh/h | 176 | 128 | 188 | 0 | 194 | 6 | 0 | 1242 | 7 | 327 | 1242 | 123 |
| Arrive On Green | 0.05 | 0.19 | 0.19 | 0.00 | 0.11 | 0.10 | 0.00 | 0.67 | 0.66 | 0.04 | 0.74 | 0.74 |
| Sat Flow, veh/h | 1781 | 676 | 994 | 0 | 1801 | 58 | 0 | 1859 | 10 | 1781 | 1674 | 166 |
| Grp Volume(v), veh/h | 77 | 0 | 121 | 0 | 0 | 159 | 0 | 0 | 945 | 55 | 0 | 1220 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 0 | 1670 | 0 | 0 | 1860 | 0 | 0 | 1869 | 1781 | 0 | 1840 |
| Q Serve(g_s), s | 4.4 | 0.0 | 7.4 | 0.0 | 0.0 | 9.8 | 0.0 | 0.0 | 39.8 | 1.0 | 0.0 | 59.4 |
| Cycle Q Clear(g_c), s | 4.4 | 0.0 | 7.4 | 0.0 | 0.0 | 9.8 | 0.0 | 0.0 | 39.8 | 1.0 | 0.0 | 59.4 |
| Prop In Lane | 1.00 |  | 0.60 | 0.00 |  | 0.03 | 0.00 |  | 0.01 | 1.00 |  | 0.09 |
| Lane Grp Cap(c), veh/h | 176 | 0 | 317 | 0 | 0 | 200 | 0 | 0 | 1249 | 327 | 0 | 1365 |
| V/C Ratio(X) | 0.44 | 0.00 | 0.38 | 0.00 | 0.00 | 0.80 | 0.00 | 0.00 | 0.76 | 0.17 | 0.00 | 0.89 |
| Avail Cap(c_a), veh/h | 176 | 0 | 358 | 0 | 0 | 246 | 0 | 0 | 1249 | 340 | 0 | 1365 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 42.5 | 0.0 | 41.6 | 0.0 | 0.0 | 51.0 | 0.0 | 0.0 | 13.0 | 12.8 | 0.0 | 11.6 |
| Incr Delay (d2), s/veh | 1.7 | 0.0 | 0.8 | 0.0 | 0.0 | 13.5 | 0.0 | 0.0 | 2.7 | 0.2 | 0.0 | 9.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 2.0 | 0.0 | 3.2 | 0.0 | 0.0 | 5.3 | 0.0 | 0.0 | 16.5 | 0.6 | 0.0 | 24.3 |
| Unsig. Movement Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| LnGrp Delay(d),s/veh | 44.2 | 0.0 | 42.4 | 0.0 | 0.0 | 64.5 | 0.0 | 0.0 | 15.8 | 13.0 | 0.0 | 20.8 |
| LnGrp LOS | D | A | D | A | A | E | A | A | B | B | A | C |
| Approach Vol, veh/h |  | 198 |  |  | 159 |  |  | 945 |  |  | 1275 |  |
| Approach Delay, s/veh |  | 43.1 |  |  | 64.5 |  |  | 15.8 |  |  | 20.5 |  |
| Approach LOS |  | D |  |  | E |  |  | B |  |  | C |  |
| Timer - Assigned Phs | 1 | 2 |  | 4 |  | 6 | 7 | 8 |  |  |  |  |
| Phs Duration (G+Y+Rc), s | 8.7 | 82.2 |  | 26.2 |  | 90.9 | 9.6 | 16.6 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ), s | 4.5 | 4.5 |  | 4.5 |  | 4.5 | 4.5 | 4.5 |  |  |  |  |
| Max Green Setting (Gmax), s | 5.0 | 76.9 |  | 24.6 |  | 86.4 | 5.1 | 15.0 |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 3.0 | 41.8 |  | 9.4 |  | 61.4 | 6.4 | 11.8 |  |  |  |  |
| Green Ext Time (p_c), s | 0.0 | 10.1 |  | 0.5 |  | 14.0 | 0.0 | 0.2 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 6th Ctrl Delay |  |  | 23.2 |  |  |  |  |  |  |  |  |  |
| HCM 6th LOS |  |  | C |  |  |  |  |  |  |  |  |  |






| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 2.3 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations |  | $\mathbf{T}$ | $\boldsymbol{F}$ |  |  |  |
| Traffic Vol, veh/h | 0 | 105 | 450 | 80 | 0 | 0 |
| Future Vol, veh/h | 0 | 105 | 450 | 80 | 0 | 0 |
| Conflicting Peds, \#/hr | 15 | 0 | 0 | 23 | 23 | 0 |
| Sign Control | Stop | Stop | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 0 | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | -16979 |  |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 91 | 91 | 91 | 91 | 91 | 91 |
| Heavy Vehicles, \% | 2 | 2 | 3 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 115 | 495 | 88 | 0 | 0 |


| Major/Minor M | Major1 |  |  |
| :---: | :---: | :---: | :---: |
| Conflicting Flow All | 562 | 0 | 0 |
| Stage 1 | - | - | - |
| Stage 2 | - | - | - |
| Critical Hdwy | 6.22 | - | - |
| Critical Hdwy Stg 1 | - | - | - |
| Critical Hdwy Stg 2 | - | - | - |
| Follow-up Hdwy | 3.318 | - | - |
| Pot Cap-1 Maneuver | 526 | - | - |
| Stage 1 | - | - | - |
| Stage 2 | - | - | - |
| Platoon blocked, \% |  | - | - |
| Mov Cap-1 Maneuver | 514 | - | - |
| Mov Cap-2 Maneuver | - | - | - |
| Stage 1 | - | - | - |
| Stage 2 | - | - | - |
|  |  |  |  |
| Approach |  | NB |  |
| HCM Control Delay, s |  | 0 |  |
| HCM LOS |  |  |  |
|  |  |  |  |
| Minor Lane/Major Mvmt | NBT | RV |  |
| Capacity (veh/h) | - | - | 514 |
| HCM Lane V/C Ratio | - | - | 24 |
| HCM Control Delay (s) | - | - | 14 |
| HCM Lane LOS | - | - | B |
| HCM 95th \%tile Q(veh) | - | - | 0.9 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Minor2 |  | Major1 |  |
| :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 697 | - | 15 | 0 |
| Stage 1 | 15 | - | - | - |
| Stage 2 | 682 | - | - | - |
| Critical Hdwy | 6.42 | - | 4.13 | - |
| Critical Hdwy Stg 1 | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - |
| Follow-up Hdwy | 3.518 |  | 2.227 | - |
| Pot Cap-1 Maneuver | 407 | 0 | 1596 | - |
| Stage 1 | - | 0 | - | - |
| Stage 2 | 502 | 0 | - | - |
| Platoon blocked, \% |  |  |  | - |
| Mov Cap-1 Maneuver | 370 | - | 1573 | - |
| Mov Cap-2 Maneuver | 370 | - | - | - |
| Stage 1 | - | - | - | - |
| Stage 2 | 495 | - | - | - |
|  |  |  |  |  |
| Approach | EB |  | NB |  |
| HCM Control Delay, s | 15.3 |  | 0.9 |  |
| HCM LOS | C |  |  |  |
|  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBL NBT EBLn1 |  |  |
| Capacity (veh/h) |  | 1573 | - | 370 |
| HCM Lane V/C Ratio |  | 0.045 | - |  |
| HCM Control Delay (s) |  | 7.4 | 0 | 5.3 |
| HCM Lane LOS |  | A | A | C |
| HCM 95th \%tile Q(veh) |  | 0.1 | - | 0.2 |



## Table of Contents

Intersection Analysis Summary ..... 2
Intersection Level Of Service Report ..... 3
Intersection 1: 13th/Belmont ..... 3
Intersection 3: 13th/May ..... 5
Turning Movement Volume: Summary ..... 7
Turning Movement Volume: Detail .....  8

Vistro File: C:I...IScen 3_HoodRiver OR281 RABs_Mit updated.vistro
Report File: X:I...IScenario 3 - Mit.pdf

Intersection Analysis Summary

| ID | Intersection Name | Control Type | Method | Worst Mvmt | V/C | Delay (s/veh) | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 13th/Belmont | Roundabout | HCM 6th <br> Edition | EB Right |  | 26.5 | D |
| 3 | 13th/May | Roundabout | HCM 6th <br> Edition | WB Left |  | 18.3 | C |

V/C, Delay, LOS: For two-way stop, these values are taken from the movement with the worst (highest) delay value. For all other control types, they are taken for the whole intersection.

## Intersection Level Of Service Report Intersection 1: 13th/Belmont

Control Type: Analysis Method: Analysis Period:
Roundabout HCM 6th Edition 15 minutes

Intersection Setup

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $\uparrow$ |  |  | $\dagger$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  |
| Turning Movement | Thru | Right | Right2 | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  |
| Grade [\%] | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | Yes |  |  | Yes |  |  | Yes |  |  | Yes |  |  |

## Volumes

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 120 | 865 | 5 | 50 | 1000 | 100 | 70 | 45 | 200 | 15 | 20 | 5 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 | 1.00 | 2.00 | 3.00 | 3.00 | 8.00 | 2.00 | 2.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 120 | 865 | 5 | 50 | 1000 | 100 | 70 | 45 | 200 | 15 | 20 | 5 |
| Peak Hour Factor | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 | 0.9100 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 33 | 238 | 1 | 14 | 275 | 27 | 19 | 12 | 55 | 4 | 5 | 1 |
| Total Analysis Volume [veh/h] | 132 | 951 | 5 | 55 | 1099 | 110 | 77 | 49 | 220 | 16 | 22 | 5 |
| Pedestrian Volume [ped/h] | 2 |  |  | 0 |  |  | 5 |  |  | 3 |  |  |

## Generated with PTV VISTRO

Version 2021 (SP 0-6)
Intersection Settings

| Number of Conflicting Circulating Lanes | 1 |  |  | 1 |  |  | 1 |  |  | 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Circulating Flow Rate [veh/h] | 185 |  |  | 174 |  |  | 1194 |  |  | 1183 |  |  |
| Exiting Flow Rate [veh/h] | 1365 |  |  | 1054 |  |  | 268 |  |  | 112 |  |  |
| Demand Flow Rate [veh/h] | 120 | 865 | 5 | 50 | 1000 | 100 | 70 | 45 | 200 | 15 | 20 | 5 |
| Adjusted Demand Flow Rate [veh/h] | 132 | 951 | 5 | 55 | 1099 | 110 | 77 | 49 | 220 | 16 | 22 | 5 |

## Lanes

| Overwrite Calculated Critical Headway | No | No | No | No | No |
| :---: | :---: | :---: | :---: | :---: | :---: |
| User-Defined Critical Headway [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| Overwrite Calculated Follow-Up Time | No | No | No | No | No |
| User-Defined Follow-Up Time [s] | 3.00 | 3.00 | 3.00 | 3.00 | 3.00 |
| A (intercept) | 1380.00 | 1420.00 | 1420.00 | 1380.00 | 1380.00 |
| B (coefficient) | 0.00102 | 0.00091 | 0.00091 | 0.00102 | 0.00102 |
| HV Adjustment Factor | 0.98 | 0.98 | 0.98 | 0.97 | 0.96 |
| Entry Flow Rate [veh/h] | 1110 | 606 | 683 | 356 | 45 |
| Capacity of Entry and Bypass Lanes [veh/h] | 1143 | 1212 | 1212 | 409 | 413 |
| Pedestrian Impedance | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Capacity per Entry Lane [veh/h] | 1120 | 1188 | 1189 | 398 | 397 |
| X, volume / capacity | 0.97 | 0.50 | 0.56 | 0.87 | 0.11 |

Movement, Approach, \& Intersection Results

| Lane LOS | E | A | A | F | B |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 95th-Percentile Queue Length [veh] | 18.31 | 2.89 | 3.66 | 8.64 | 0.36 |
| 95th-Percentile Queue Length [ft] | 457.66 | 72.22 | 91.62 | 215.90 | 9.05 |
| Approach Delay [s/veh] | 39.71 |  |  | 50.74 | 10.73 |
| Approach LOS | E |  |  | F | B |
| Intersection Delay [s/veh] | 26.55 |  |  |  |  |
| Intersection LOS | D |  |  |  |  |

## Intersection Level Of Service Report Intersection 3: 13th/May

Control Type:
Analysis Method:
Analysis Period:
Roundabout HCM 6th Edition 15 minutes

Intersection Setup

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  |
| Lane Configuration | $\uparrow$ |  |  | $4 F$ |  |  | $\uparrow$ |  |  | $\dagger \Gamma$ |  |  |
| Turning Movement | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Lane Width [ft] | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 | 12.00 |
| No. of Lanes in Entry Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Entry Pocket Length [ft] | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 | 100.00 |
| No. of Lanes in Exit Pocket | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Exit Pocket Length [ft] | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Speed [mph] | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  | 25.00 |  |  |
| Grade [\%] | -4.50 |  |  | 4.50 |  |  | 0.00 |  |  | 0.00 |  |  |
| Crosswalk | Yes |  |  | Yes |  |  | Yes |  |  | Yes |  |  |

## Volumes

| Name |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Base Volume Input [veh/h] | 100 | 650 | 110 | 25 | 725 | 55 | 50 | 35 | 80 | 310 | 195 | 140 |
| Base Volume Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Heavy Vehicles Percentage [\%] | 2.00 | 2.00 | 2.00 | 2.00 | 3.00 | 2.00 | 2.00 | 1.00 | 3.00 | 2.00 | 4.00 | 1.00 |
| Growth Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| In-Process Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Site-Generated Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Diverted Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pass-by Trips [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Existing Site Adjustment Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other Volume [veh/h] | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Hourly Volume [veh/h] | 100 | 650 | 110 | 25 | 725 | 55 | 50 | 35 | 80 | 310 | 195 | 140 |
| Peak Hour Factor | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 | 0.9400 |
| Other Adjustment Factor | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 | 1.0000 |
| Total 15-Minute Volume [veh/h] | 27 | 173 | 29 | 7 | 193 | 15 | 13 | 9 | 21 | 82 | 52 | 37 |
| Total Analysis Volume [veh/h] | 106 | 691 | 117 | 27 | 771 | 59 | 53 | 37 | 85 | 330 | 207 | 149 |
| Pedestrian Volume [ped/h] | 10 |  |  | 1 |  |  | 9 |  |  | 7 |  |  |

## Generated with PTV VISTRO

Version 2021 (SP 0-6)
Intersection Settings

| Number of Conflicting Circulating Lanes | 1 |  |  | 1 |  |  | 2 |  |  | 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Circulating Flow Rate [veh/h] | 119 |  |  | 660 |  |  | 1158 |  |  | 867 |  |  |
| Exiting Flow Rate [veh/h] | 1218 |  |  | 909 |  |  | 384 |  |  | 184 |  |  |
| Demand Flow Rate [veh/h] | 100 | 650 | 110 | 25 | 725 | 55 | 50 | 35 | 80 | 310 | 195 | 140 |
| Adjusted Demand Flow Rate [veh/h] | 106 | 691 | 117 | 27 | 771 | 59 | 53 | 37 | 85 | 330 | 207 | 149 |

## Lanes

| Overwrite Calculated Critical Headway | No | No | No | No | No | No |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| User-Defined Critical Headway [s] | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 | 4.00 |
| Overwrite Calculated Follow-Up Time | No | No | No | No | No | No |
| User-Defined Follow-Up Time [s] | 3.00 | 3.00 | 3.00 | 3.00 | 3.00 | 3.00 |
| A (intercept) | 1380.00 | 1420.00 | 1420.00 | 1420.00 | 1420.00 | 1420.00 |
| B (coefficient) | 0.00102 | 0.00091 | 0.00091 | 0.00085 | 0.00091 | 0.00091 |
| HV Adjustment Factor | 0.98 | 0.97 | 0.97 | 0.98 | 0.97 | 0.99 |
| Entry Flow Rate [veh/h] | 933 | 415 | 468 | 179 | 552 | 151 |
| Capacity of Entry and Bypass Lanes [veh/h] | 1223 | 779 | 779 | 531 | 646 | 646 |
| Pedestrian Impedance | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Capacity per Entry Lane [veh/h] | 1197 | 757 | 757 | 519 | 628 | 639 |
| X, volume / capacity | 0.76 | 0.53 | 0.60 | 0.34 | 0.86 | 0.23 |

Movement, Approach, \& Intersection Results

| Lane LOS | C | B | B | B | D | A |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 95th-Percentile Queue Length [veh] | 7.92 | 3.19 | 4.07 | 1.48 | 9.63 | 0.90 |
| 95th-Percentile Queue Length [ft] | 198.08 | 79.75 | 101.77 | 36.91 | 240.65 | 22.51 |
| Approach Delay [s/veh] | 15.80 |  |  | 12.12 |  |  |
| Approach LOS | C |  |  | B |  |  |
| Intersection Delay [s/veh] | 18.33 |  |  |  |  |  |
| Intersection LOS | C |  |  |  |  |  |

Generated with PTV VISTRO
Version 2021 (SP 0-6)

Vistro File: C:I...IScen 3_HoodRiver OR281 RABs_Mit
Scenario 1 Scen3-Mit updated.vistro
Report File: X:I...IScenario 3 - Mit.pdf
1/13/2022

Turning Movement Volume: Summary

|  | Intersection Name | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Thru | Right | 2 | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| 1 | 13th/Belmont | 120 | 865 | 5 | 50 | 1000 | 100 | 70 | 45 | 200 | 15 | 20 | 5 | 2495 |


| ID | Intersection Name | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| 3 | 13th/May | 100 | 650 | 110 | 25 | 725 | 55 | 50 | 35 | 80 | 310 | 195 | 140 | 2475 |

Generated with PTV VISTRO
Version 2021 (SP 0-6)

Vistro File: C:I...IScen 3_HoodRiver OR281 RABs_Mit updated.vistro
Report File: X:I...IScenario 3 - Mit.pdf
1/13/2022

Turning Movement Volume: Detail

| ID | Intersection Name | Volume Type | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Thru | Right | 2 | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| 1 | 13th/Belmont | Final Base | 120 | 865 | 5 | 50 | 1000 | 100 | 70 | 45 | 200 | 15 | 20 | 5 | 2495 |
|  |  | Growth Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | - |
|  |  | In Process | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Net New Trips | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Other | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Future Total | 120 | 865 | 5 | 50 | 1000 | 100 | 70 | 45 | 200 | 15 | 20 | 5 | 2495 |


| ID | Intersection Name | Volume Type | Northbound |  |  | Southbound |  |  | Eastbound |  |  | Westbound |  |  | Total Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |  |
| 3 | 13th/May | Final Base | 100 | 650 | 110 | 25 | 725 | 55 | 50 | 35 | 80 | 310 | 195 | 140 | 2475 |
|  |  | Growth Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | - |
|  |  | In Process | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Net New Trips | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Other | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
|  |  | Future Total | 100 | 650 | 110 | 25 | 725 | 55 | 50 | 35 | 80 | 310 | 195 | 140 | 2475 |

APPENDIX E: SIMTRAFFIC REPORTS (MITIGATED AND TSP BUILD)

## Summary of All Intervals

| Run Number | 1 | 10 | 2 | 3 | 4 | 5 | 7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Start Time | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ |
| End Time | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ |
| Total Time (min) | 70 | 70 | 70 | 70 | 70 | 70 | 70 |
| Time Recorded (min) | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| \# of Intervals | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| \# of Recorded Intervals | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Vehs Entered | 4370 | 4233 | 4319 | 4273 | 4228 | 4255 | 4363 |
| Vehs Exited | 4342 | 4226 | 4333 | 4231 | 4239 | 4308 | 4429 |
| Starting Vehs | 194 | 188 | 195 | 160 | 218 | 194 | 222 |
| Ending Vehs | 222 | 195 | 181 | 202 | 207 | 141 | 156 |
| Travel Distance (mi) | 2805 | 2752 | 2796 | 2723 | 2725 | 2749 | 2800 |
| Travel Time (hr) | 199.8 | 194.6 | 206.5 | 202.0 | 208.0 | 199.7 | 199.7 |
| Total Delay (hr) | 78.9 | 76.2 | 86.8 | 84.8 | 90.8 | 81.4 | 79.1 |
| Total Stops | 6966 | 7077 | 7866 | 6746 | 7615 | 7196 | 7301 |
| Fuel Used (gal) | 114.4 | 112.0 | 116.3 | 113.1 | 114.9 | 113.5 | 114.5 |

## Summary of All Intervals

| Run Number | 9 | Avg |
| :--- | ---: | ---: |
| Start Time | $6: 57$ | $6: 57$ |
| End Time | $8: 07$ | $8: 07$ |
| Total Time (min) | 70 | 70 |
| Time Recorded (min) | 60 | 60 |
| \# of Intervals | 3 | 3 |
| \# of Recorded Intervals | 2 | 2 |
| Vehs Entered | 4265 | 4287 |
| Vehs Exited | 4246 | 4294 |
| Starting Vehs | 211 | 194 |
| Ending Vehs | 230 | 191 |
| Travel Distance (mi) | 2757 | 2764 |
| Travel Time (hr) | 200.9 | 201.4 |
| Total Delay (hr) | 82.5 | 82.6 |
| Total Stops | 7245 | 7251 |
| Fuel Used (gal) | 113.5 | 114.0 |

Interval \#0 Information Seeding

| Start Time | $6: 57$ |
| :--- | :---: |
| End Time | $7: 07$ |
| Total Time (min) | 10 |
| Volumes adjusted by PHF, Growth Factors. |  |
|  |  |

Interval \#1 Information Recording1

| Start Time 7:07 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| End Time 7:22 |  |  |  |  |  |  |  |
| Total Time (min) 15 |  |  |  |  |  |  |  |
| Volumes adjusted by PHF, Growth Factors. |  |  |  |  |  |  |  |
| Run Number | 1 | 10 | 2 | 3 | 4 | 5 | 7 |
| Vehs Entered | 1156 | 1214 | 1173 | 1176 | 1193 | 1189 | 1218 |
| Vehs Exited | 1152 | 1181 | 1168 | 1109 | 1163 | 1156 | 1226 |
| Starting Vehs | 194 | 188 | 195 | 160 | 218 | 194 | 222 |
| Ending Vehs | 198 | 221 | 200 | 227 | 248 | 227 | 214 |
| Travel Distance (mi) | 719 | 734 | 722 | 711 | 734 | 728 | 751 |
| Travel Time (hr) | 51.1 | 53.7 | 53.9 | 48.8 | 60.6 | 56.9 | 58.4 |
| Total Delay (hr) | 20.0 | 22.2 | 22.9 | 18.2 | 29.0 | 25.5 | 26.0 |
| Total Stops | 1760 | 2014 | 2035 | 1778 | 2175 | 2005 | 2137 |
| Fuel Used (gal) | 29.5 | 30.4 | 30.4 | 28.6 | 31.9 | 31.1 | 31.6 |

## Interval \#1 Information Recording1

| Start Time | $7: 07$ |  |
| :--- | ---: | ---: |
| End Time | $7: 22$ |  |
| Total Time (min) |  |  |
| Volumes adjusted by PHF, Growth Factors. |  |  |
| Run Number |  |  |
| Vehs Entered | 9 | Avg |
| Vehs Exited | 1163 | 1183 |
| Starting Vehs | 1129 | 1161 |
| Ending Vehs | 211 | 194 |
| Travel Distance (mi) | 245 | 222 |
| Travel Time (hr) | 723 | 728 |
| Total Delay (hr) | 56.1 | 54.9 |
| Total Stops | 25.1 | 23.6 |
| Fuel Used (gal) | 1966 | 1982 |
|  | 30.6 | 30.5 |

Interval \#2 Information Recording2

| Start Time | 7:22 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| End Time | 8:07 |  |  |  |  |  |  |
| Total Time (min) | 45 |  |  |  |  |  |  |
| Volumes adjusted by Growth Factors, Anti PHF. |  |  |  |  |  |  |  |
| Run Number | 1 | 10 | 2 | 3 | 4 | 5 | 7 |
| Vehs Entered | 3214 | 3019 | 3146 | 3097 | 3035 | 3066 | 3145 |
| Vehs Exited | 3190 | 3045 | 3165 | 3122 | 3076 | 3152 | 3203 |
| Starting Vehs | 198 | 221 | 200 | 227 | 248 | 227 | 214 |
| Ending Vehs | 222 | 195 | 181 | 202 | 207 | 141 | 156 |
| Travel Distance (mi) | 2086 | 2019 | 2074 | 2012 | 1992 | 2021 | 2050 |
| Travel Time (hr) | 148.6 | 140.9 | 152.6 | 153.2 | 147.4 | 142.9 | 141.3 |
| Total Delay (hr) | 58.8 | 54.0 | 63.9 | 66.6 | 61.8 | 55.8 | 53.0 |
| Total Stops | 5206 | 5063 | 5831 | 4968 | 5440 | 5191 | 5164 |
| Fuel Used (gal) | 84.9 | 81.6 | 86.0 | 84.5 | 82.9 | 82.4 | 82.9 |

## Interval \#2 Information Recording2

| Start Time | $7: 22$ |  |
| :--- | ---: | ---: |
| End Time | $8: 07$ |  |
| Total Time (min) | A5 |  |
| Volumes adjusted by Growth Factors, Anti PHF |  |  |
| Run Number | 9 | Avg |
| Vehs Entered | 3102 | 3104 |
| Vehs Exited | 3117 | 3133 |
| Starting Vehs | 245 | 222 |
| Ending Vehs | 230 | 191 |
| Travel Distance (mi) | 2034 | 2036 |
| Travel Time (hr) | 144.8 | 146.5 |
| Total Delay (hr) | 57.5 | 58.9 |
| Total Stops | 5279 | 5265 |
| Fuel Used (gal) | 82.9 | 83.5 |

Arterial Level of Service: NB 13th St

| Cross Street | Node | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Oak St | 1 | 41.8 | 63.2 | 0.3 | 19 |
| Total |  | 41.8 | 63.2 | 0.3 | 19 |

Arterial Level of Service: SB 13th St

| Cross Street | Node | Delay <br> $(\mathrm{s} /$ veh $)$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| May St | 2 | 68.6 | 113.0 | 0.3 | 10 |
|  | 13 | 1.0 | 9.2 | 0.1 | 22 |
| Taylor | 3 | 0.5 | 9.4 | 0.1 | 24 |
| A St | 4 | 2.0 | 23.2 | 0.1 | 23 |
| Belmont | 5 | 8.0 | 14.7 | 0.0 | 11 |
| Total | 25 | 1.0 | 5.2 | 0.0 | 20 |

## Arterial Level of Service: NB 12th St

| Cross Street | Node | Delay <br> $(\mathrm{s} /$ veh $)$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Union | 6 | 1.0 | 10.0 | 0.1 | 23 |
| Wilson | 7 | 1.2 | 7.8 | 0.0 | 22 |
| Pine | 8 | 1.7 | 20.0 | 0.1 | 23 |
| Taylor | 9 | 0.4 | 3.7 | 0.0 | 21 |
| May St | 10 | 18.4 | 35.8 | 0.1 | 12 |
| Total |  | 22.7 | 77.3 | 0.4 | 18 |

Queuing and Blocking Report

Intersection: 1: 13th St \& Oak St

| Movement | EB | EB | WB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | T | L | R |
| Maximum Queue (ft) | 657 | 175 | 224 | 856 | 778 | 255 |
| Average Queue (ft) | 276 | 153 | 218 | 455 | 455 | 130 |
| 95th Queue (ft) | 582 | 213 | 246 | 878 | 794 | 295 |
| Link Distance (ft) | 833 |  |  | 898 | 1624 |  |
| Upstream Blk Time (\%) | 1 |  |  | 3 |  |  |
| Queuing Penalty (veh) | 0 |  |  | 0 |  |  |
| Storage Bay Dist (ft) |  | 150 | 200 |  |  | 230 |
| Storage Blk Time (\%) | 15 | 7 | 38 | 0 | 33 | 0 |
| Queuing Penalty (veh) | 71 | 17 | 87 | 1 | 36 | 1 |

Intersection: 2: 13th St \& May St

| Movement | EB | EB | WB | WB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | LT | R | LTR |
| Maximum Queue (ft) | 105 | 98 | 352 | 280 | 1354 |
| Average Queue (ft) | 47 | 38 | 258 | 13 | 806 |
| 95th Queue (ft) | 94 | 79 | 382 | 118 | 1379 |
| Link Distance (ft) | 804 |  | 316 | 316 | 1624 |
| Upstream Blk Time (\%) |  |  | 5 | 0 | 0 |
| Queuing Penalty (veh) |  |  | 24 | 1 | 0 |
| Storage Bay Dist (ft) |  | 120 |  |  |  |
| Storage Blk Time (\%) | 0 | 0 |  |  |  |
| Queuing Penalty (veh) | 0 | 0 |  |  |  |

Intersection: 3: 13th St \& Taylor

| Movement | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | LT | LT | TR |
| Maximum Queue (ft) | 57 | 164 | 60 | 69 |
| Average Queue (ft) | 18 | 69 | 8 | 8 |
| 95th Queue (ft) | 50 | 127 | 37 | 39 |
| Link Distance (ft) | 591 | 229 | 271 | 271 |
| Upstream Blk Time (\%) |  | 0 |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |

Queuing and Blocking Report

Intersection: 4: 13th St \& A St

| Movement | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | LT | LT | TR |
| Maximum Queue (ft) | 51 | 133 | 125 | 140 |
| Average Queue (ft) | 16 | 53 | 15 | 29 |
| 95th Queue (ft) | 47 | 103 | 75 | 97 |
| Link Distance (ft) | 745 | 215 | 731 | 731 |
| Upstream Blk Time (\%) |  | 0 |  |  |
| Queuing Penalty (veh) | 0 |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 5: 13th St \& Belmont

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | LT | LT | TR |
| Maximum Queue (ft) | 214 | 124 | 163 | 200 | 213 |
| Average Queue (ft) | 65 | 70 | 75 | 133 | 154 |
| 95th Queue (ft) | 161 | 121 | 130 | 202 | 216 |
| Link Distance (ft) | 887 |  | 206 | 186 | 186 |
| Upstream Blk Time (\%) |  |  | 0 | 1 | 3 |
| Queuing Penalty (veh) |  |  | 0 | 9 | 17 |
| Storage Bay Dist (ft) |  | 100 |  |  |  |
| Storage Blk Time (\%) | 3 | 2 |  |  |  |

Intersection: 6: 12th St \& Belmont/Union

| Movement | EB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LT | TR | LT | TR |
| Maximum Queue (ft) | 209 | 63 | 89 | 68 |
| Average Queue (ft) | 93 | 14 | 8 | 5 |
| 95th Queue (ft) | 178 | 46 | 48 | 32 |
| Link Distance (ft) | 206 | 693 | 287 | 287 |
| Upstream Blk Time (\%) | 2 |  |  |  |
| Queuing Penalty (veh) | 4 |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |

Intersection: 7: 12th St \& A St/Wilson

| Movement | EB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LT | TR | LT | TR |
| Maximum Queue (ft) | 119 | 132 | 127 | 124 |
| Average Queue (ft) | 48 | 46 | 26 | 22 |
| 95th Queue (ft) | 100 | 103 | 88 | 78 |
| Link Distance (ft) | 215 | 700 | 197 | 197 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 8: 12th St \& Pine

| Movement | WB | NB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | R | T | TR |
| Maximum Queue (ft) | 134 | 65 | 94 |
| Average Queue (ft) | 57 | 8 | 15 |
| 95th Queue (ft) | 98 | 36 | 61 |
| Link Distance (ft) | 838 | 616 | 616 |
| Upstream Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Storage Bay Dist (ft) |  |  |  |

## Intersection: 9: 12th St \& Taylor

| Movement | EB | NB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | L | LT | T |
| Maximum Queue (ft) | 81 | 75 | 63 |
| Average Queue (ft) | 33 | 7 | 4 |
| 95th Queue (ft) | 70 | 39 | 28 |
| Link Distance (ft) | 229 | 64 | 64 |
| Upstream Blk Time (\%) |  | 0 | 0 |
| Queuing Penalty (veh) |  | 3 | 1 |
| Storage Bay Dist (ft) |  |  |  |

Intersection: 10: 12th St \& May St

| Movement | EB | WB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | T | L | R |
| Maximum Queue (ft) | 94 | 156 | 162 | 460 | 383 |
| Average Queue (ft) | 34 | 114 | 100 | 261 | 142 |
| 95th Queue (ft) | 76 | 162 | 171 | 417 | 284 |
| Link Distance (ft) | 316 | 87 | 87 | 567 | 567 |
| Upstream Blk Time (\%) |  | 29 | 16 | 0 | 0 |
| Queuing Penalty (veh) |  | 60 | 33 | 0 | 0 |
| Storage Bay Dist (ft) |  |  |  |  |  |

## Intersection: 11: May St

| Movement | EB | WB | SB | B27 | B26 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | TR | LR | T | T |
| Maximum Queue (ft) | 141 | 385 | 267 | 154 | 116 |
| Average Queue (ft) | 33 | 172 | 141 | 36 | 20 |
| 95th Queue (ft) | 117 | 390 | 266 | 171 | 146 |
| Link Distance (ft) | 87 | 1326 | 170 | 184 | 654 |
| Upstream Blk Time (\%) | 3 |  | 21 | 7 |  |
| Queuing Penalty (veh) | 22 |  | 0 | 0 |  |
| Storage Bay Dist (ft) |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |

Intersection: 14: 12th St

| Movement |
| :--- |
| Directions Served |
| Maximum Queue (ft) |
| Average Queue (ft) |
| 95th Queue (ft) |
| Link Distance (ft) |
| Upstream Blk Time (\%) |
| Queuing Penalty (veh) |
| Storage Bay Dist (ft) |
| Storage Blk Time (\%) |
| Queuing Penalty (veh) |
| Network Summary |
| Network wide Queuing Penalty: 396 |

SimTraffic Simulation Summary
Scenario 1 - Mitigated
Summary of All Intervals

| Run Number | 1 | 10 | 2 | 3 | 4 | 5 | 6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Start Time | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ |
| End Time | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ |
| Total Time (min) | 70 | 70 | 70 | 70 | 70 | 70 | 70 |
| Time Recorded (min) | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| \# of Intervals | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| \# of Recorded Intervals | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Vehs Entered | 4595 | 3091 | 4475 | 4560 | 4510 | 4510 | 4538 |
| Vehs Exited | 4592 | 2820 | 4453 | 4577 | 4496 | 4518 | 4529 |
| Starting Vehs | 243 | 273 | 198 | 243 | 202 | 208 | 238 |
| Ending Vehs | 246 | 544 | 220 | 226 | 216 | 200 | 247 |
| Travel Distance (mi) | 2978 | 1767 | 2927 | 2963 | 2934 | 2925 | 2945 |
| Travel Time (hr) | 232.5 | 763.8 | 215.2 | 242.6 | 222.9 | 213.8 | 317.4 |
| Total Delay (hr) | 107.2 | 689.3 | 92.2 | 117.9 | 99.2 | 90.8 | 193.3 |
| Total Stops | 9021 | 7341 | 8201 | 9467 | 8289 | 8165 | 9655 |
| Fuel Used (gal) | 125.5 | 217.2 | 120.0 | 127.1 | 121.9 | 119.8 | 144.1 |

Summary of All Intervals

| Run Number | 7 | 8 | 9 | Avg |
| :--- | ---: | ---: | ---: | ---: |
| Start Time | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ |
| End Time | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ |
| Total Time (min) | 70 | 70 | 70 | 70 |
| Time Recorded (min) | 60 | 60 | 60 | 60 |
| \# of Intervals | 3 | 3 | 3 | 3 |
| \# of Recorded Intervals | 2 | 2 | 2 | 2 |
| Vehs Entered | 4589 | 4655 | 4609 | 4409 |
| Vehs Exited | 4516 | 4619 | 4506 | 4362 |
| Starting Vehs | 222 | 219 | 206 | 217 |
| Ending Vehs | 295 | 255 | 309 | 269 |
| Travel Distance (mi) | 2938 | 3025 | 2949 | 2835 |
| Travel Time (hr) | 279.1 | 258.5 | 259.9 | 300.6 |
| Total Delay (hr) | 155.3 | 131.1 | 135.8 | 181.2 |
| Total Stops | 10510 | 8513 | 9026 | 8821 |
| Fuel Used (gal) | 134.3 | 131.7 | 130.4 | 137.2 |

Interval \#0 Information Seeding

| Start Time | $6: 57$ |
| :--- | :---: |
| End Time | $7: 07$ |
| Total Time $(\mathrm{min})$ | 10 |
| Volumes adjusted by PHF, Growth Factors. |  |
| No data recorded this interval. |  |

Interval \#1 Information Recording1

| Start Time | $7: 07$ |
| :--- | ---: |
| End Time | $7: 22$ |
| Total Time (min) | 15 |
| Volumes adjusted by PHF, Growth Factors. |  |


| Run Number | 1 | 10 | 2 | 3 | 4 | 5 | 6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vehs Entered | 1236 | 1167 | 1212 | 1277 | 1249 | 1250 | 1213 |
| Vehs Exited | 1221 | 1068 | 1159 | 1271 | 1179 | 1223 | 1187 |
| Starting Vehs | 243 | 273 | 198 | 243 | 202 | 208 | 238 |
| Ending Vehs | 258 | 372 | 251 | 249 | 272 | 235 | 264 |
| Travel Distance (mi) | 777 | 708 | 757 | 797 | 765 | 777 | 754 |
| Travel Time (hr) | 57.9 | 75.9 | 61.0 | 66.2 | 58.9 | 55.4 | 69.1 |
| Total Delay (hr) | 25.1 | 46.2 | 29.3 | 32.7 | 26.6 | 22.7 | 37.2 |
| Total Stops | 2192 | 2453 | 2207 | 2651 | 2189 | 2035 | 2442 |
| Fuel Used (gal) | 32.2 | 34.5 | 31.9 | 34.5 | 32.0 | 31.5 | 34.1 |

Interval \#1 Information Recording1

| Start Time | $7: 07$ |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| End Time | $7: 22$ |  |  |  |
| Total Time (min) | 15 |  |  |  |
| Volumes adjusted by PHF, Growth Factors. |  |  |  |  |
| Run Number | 7 | 8 | 9 | Avg |
| Vehs Entered | 1254 | 1325 | 1236 | 1242 |
| Vehs Exited | 1224 | 1281 | 1198 | 1202 |
| Starting Vehs | 222 | 219 | 206 | 217 |
| Ending Vehs | 252 | 263 | 244 | 256 |
| Travel Distance (mi) | 781 | 816 | 771 | 770 |
| Travel Time (hr) | 66.7 | 67.7 | 54.4 | 63.3 |
| Total Delay (hr) | 33.7 | 33.4 | 22.2 | 30.9 |
| Total Stops | 2723 | 2344 | 1971 | 2317 |
| Fuel Used (gal) | 34.3 | 35.3 | 31.2 | 33.1 |

Interval \#2 Information Recording2

| Start Time | $7: 22$ |
| :--- | ---: |
| End Time | $8: 07$ |
| Total Time (min) | 45 |
| Volumes adjusted by Growth Factors, Anti PHF. |  |


| Run Number | 1 | 10 | 2 | 3 | 4 | 5 | 6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vehs Entered | 3359 | 1924 | 3263 | 3283 | 3261 | 3260 | 3325 |
| Vehs Exited | 3371 | 1752 | 3294 | 3306 | 3317 | 3295 | 3342 |
| Starting Vehs | 258 | 372 | 251 | 249 | 272 | 235 | 264 |
| Ending Vehs | 246 | 544 | 220 | 226 | 216 | 200 | 247 |
| Travel Distance (mi) | 2201 | 1059 | 2171 | 2166 | 2169 | 2147 | 2192 |
| Travel Time (hr) | 174.7 | 687.9 | 154.2 | 176.4 | 164.0 | 158.4 | 248.3 |
| Total Delay (hr) | 82.1 | 643.1 | 63.0 | 85.2 | 72.5 | 68.1 | 156.1 |
| Total Stops | 6829 | 4888 | 5994 | 6816 | 6100 | 6130 | 7213 |
| Fuel Used (gal) | 93.3 | 182.7 | 88.2 | 92.6 | 89.8 | 88.4 | 110.0 |

## Interval \#2 Information Recording2

| Start Time | $7: 22$ |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| End Time | $8: 07$ |  |  |  |
| Total Time (min) | 45 |  |  |  |
| Volumes adjusted by Growth Factors, Anti PHF. |  |  |  |  |
| Run Number | 7 | 8 | 9 | Avg |
| Vehs Entered | 3335 | 3330 | 3373 | 3171 |
| Vehs Exited | 3292 | 3338 | 3308 | 3161 |
| Starting Vehs | 252 | 263 | 244 | 256 |
| Ending Vehs | 295 | 255 | 309 | 269 |
| Travel Distance (mi) | 2157 | 2209 | 2178 | 2065 |
| Travel Time (hr) | 212.3 | 190.8 | 205.5 | 237.2 |
| Total Delay (hr) | 121.6 | 97.7 | 113.7 | 150.3 |
| Total Stops | 7787 | 6169 | 7055 | 6492 |
| Fuel Used (gal) | 100.0 | 96.4 | 99.2 | 104.0 |

## Arterial Level of Service: NB 13th St

| Cross Street | Node | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Belmont | 5 | 13.7 | 22.6 | 0.1 | 10 |
| A St | 4 | 2.4 | 9.2 | 0.0 | 18 |
| Taylor | 3 | 11.6 | 32.8 | 0.1 | 16 |
| May St | 2 | 31.8 | 49.4 | 0.1 | 9 |
| Oak St | 1 | 49.6 | 91.7 | 0.3 | 13 |
| Total |  | 109.1 | 205.7 | 0.7 | 12 |

## Arterial Level of Service: SB 13th St

| Cross Street | Node | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| May St | 2 | 104.1 | 144.9 | 0.3 | 8 |
| Taylor | 3 | 9.5 | 26.5 | 0.1 | 16 |
| A St | 4 | 30.1 | 54.8 | 0.1 | 10 |
| Belmont | 5 | 9.4 | 16.3 | 0.0 | 11 |
|  | 25 | 1.8 | 10.4 | 0.1 | 20 |
| Total |  | 155.0 | 252.8 | 0.7 | 10 |

Arterial Level of Service: NB 12th St

| Cross Street | Node | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Union | 6 | 4.7 | 13.5 | 0.1 | 17 |
| Wilson | 7 | 2.6 | 9.6 | 0.0 | 18 |
| Pine | 8 | 7.2 | 26.8 | 0.1 | 19 |
| Taylor | 9 | 0.6 | 3.1 | 0.0 | 18 |
| May St | 10 | 16.6 | 34.2 | 0.1 | 13 |
| Total |  | 31.7 | 87.3 | 0.4 | 16 |

## Arterial Level of Service: SB 12th St

|  |  | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Cross Street | 9 | 4.2 | 22.7 | 0.1 | 19 |
| Taylor | 8 | 1.0 | 3.5 | 0.0 | 16 |
| Pine | 7 | 16.4 | 34.2 | 0.1 | 14 |
| A St | 6 | 7.3 | 14.0 | 0.0 | 12 |
| Belmont | 14 | 25.7 | 35.3 | 0.1 | 6 |
| Total |  | 54.7 | 109.9 | 0.4 | 12 |

Intersection: 1: 13th St \& Oak St

| Movement | EB | EB | WB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | T | L | R |
| Maximum Queue (ft) | 629 | 175 | 225 | 813 | 757 | 255 |
| Average Queue (ft) | 286 | 150 | 214 | 467 | 414 | 133 |
| 95th Queue (ft) | 594 | 217 | 251 | 956 | 751 | 304 |
| Link Distance (ft) | 826 |  |  | 892 | 1618 |  |
| Upstream Blk Time (\%) | 3 |  |  | 14 |  |  |
| Queuing Penalty (veh) | 0 |  |  | 0 |  |  |
| Storage Bay Dist (ft) |  | 150 | 200 |  |  | 230 |
| Storage Blk Time (\%) | 14 | 14 | 43 | 0 | 30 | 0 |
| Queuing Penalty (veh) | 63 | 31 | 95 | 1 | 33 | 2 |

Intersection: 2: 13th St \& May St

| Movement | EB | WB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | TR | L | TR | L | TR | L | TR |
| Maximum Queue (ft) | 301 | 320 | 309 | 275 | 560 | 124 | 1485 |
| Average Queue (ft) | 137 | 244 | 131 | 167 | 315 | 66 | 1041 |
| 95th Queue (ft) | 335 | 340 | 273 | 322 | 585 | 143 | 1774 |
| Link Distance (ft) | 812 | 297 | 297 |  | 560 |  | 1618 |
| Upstream Blk Time (\%) | 2 | 10 | 2 |  | 3 |  | 5 |
| Queuing Penalty (veh) | 0 | 26 | 4 |  | 21 |  | 42 |
| Storage Bay Dist (ft) |  |  |  | 250 |  | 100 |  |
| Storage Blk Time (\%) |  |  |  | 11 | 12 | 3 | 57 |
| Queuing Penalty (veh) |  |  |  | 58 | 16 | 18 | 42 |

Intersection: 3: 13th St \& Taylor

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 94 | 155 | 527 | 425 |
| Average Queue (ft) | 29 | 60 | 129 | 102 |
| 95th Queue (ft) | 75 | 139 | 411 | 360 |
| Link Distance (ft) | 600 | 194 | 732 | 560 |
| Upstream Blk Time (\%) |  | 3 | 0 | 4 |
| Queuing Penalty (veh) |  | 3 | 1 | 36 |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |

Intersection: 4: 13th St \& A St

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 80 | 151 | 178 | 730 |
| Average Queue (ft) | 23 | 59 | 31 | 453 |
| 95th Queue (ft) | 64 | 128 | 130 | 818 |
| Link Distance (ft) | 744 | 191 | 179 | 732 |
| Upstream Blk Time (\%) |  | 1 | 2 | 5 |
| Queuing Penalty (veh) |  | 1 | 11 | 48 |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |

Intersection: 5: 13th St \& Belmont

| Movement | EB | EB | WB | NB | B25 | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | TR | T | L | TR |
| Maximum Queue (ft) | 222 | 403 | 185 | 314 | 122 | 93 | 224 |
| Average Queue (ft) | 69 | 214 | 106 | 175 | 14 | 37 | 186 |
| 95th Queue (ft) | 163 | 538 | 187 | 311 | 75 | 102 | 256 |
| Link Distance (ft) |  | 892 | 175 | 236 | 70 | 179 | 179 |
| Upstream Blk Time (\%) |  | 6 | 3 | 8 | 6 | 4 | 16 |
| Queuing Penalty (veh) |  | 0 | 5 | 46 | 33 | 22 | 84 |
| Storage Bay Dist (ft) | 200 |  |  |  |  |  |  |
| Storage Blk Time (\%) | 0 | 14 |  |  |  |  |  |
| Queuing Penalty (veh) | 1 | 10 |  |  |  |  |  |

Intersection: 6: 12th St \& Belmont/Union

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 161 | 75 | 268 | 111 |
| Average Queue (ft) | 73 | 24 | 86 | 21 |
| 95th Queue (ft) | 160 | 63 | 222 | 99 |
| Link Distance (ft) | 175 | 705 | 268 | 196 |
| Upstream Blk Time (\%) | 7 |  | 3 | 5 |
| Queuing Penalty (veh) | 7 |  | 28 | 10 |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

## Intersection: 7: 12th St \& A St/Wilson

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 62 | 122 | 195 | 150 |
| Average Queue (ft) | 25 | 43 | 40 | 42 |
| 95th Queue (ft) | 59 | 92 | 129 | 251 |
| Link Distance (ft) | 191 | 712 | 196 | 644 |
| Upstream Blk Time (\%) |  |  | 2 | 4 |
| Queuing Penalty (veh) |  |  | 17 | 9 |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 8: 12th St \& Pine

| Movement | WB | NB | SB |
| :--- | ---: | ---: | ---: |
| Directions Served | LR | TR | LT |
| Maximum Queue (ft) | 322 | 413 | 35 |
| Average Queue (ft) | 102 | 79 | 12 |
| 95th Queue (ft) | 303 | 287 | 39 |
| Link Distance (ft) | 848 | 644 | 35 |
| Upstream Blk Time (\%) | 0 | 2 | 6 |
| Queuing Penalty (veh) | 0 | 14 | 13 |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |

## Intersection: 9: 12th St \& Taylor

| Movement | EB | NB | SB |
| :--- | ---: | ---: | ---: |
| Directions Served | LR | LT | TR |
| Maximum Queue (ft) | 84 | 43 | 129 |
| Average Queue (ft) | 38 | 17 | 22 |
| 95th Queue (ft) | 74 | 47 | 119 |
| Link Distance (ft) | 194 | 35 | 565 |
| Upstream Blk Time (\%) |  | 4 |  |
| Queuing Penalty (veh) |  | 37 |  |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |

## Intersection: 10: 12th St \& May St

| Movement | EB | WB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | TR | LT | T | L | R |
| Maximum Queue (ft) | 172 | 103 | 104 | 124 | 310 |
| Average Queue (ft) | 67 | 80 | 76 | 69 | 128 |
| 95th Queue (ft) | 135 | 102 | 105 | 136 | 257 |
| Link Distance (ft) | 297 | 75 | 75 |  | 565 |
| Upstream Blk Time (\%) |  | 21 | 10 |  | 0 |
| Queuing Penalty (veh) |  | 52 | 25 |  | 0 |
| Storage Bay Dist (ft) |  |  |  | 100 |  |
| Storage Blk Time (\%) |  |  |  | 3 | 9 |
| Queuing Penalty (veh) |  |  |  | 18 | 12 |

## Intersection: 11: May St

| Movement | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| Directions Served | LT | TR | LR |
| Maximum Queue (ft) | 92 | 252 | 669 |
| Average Queue (ft) | 9 | 97 | 362 |
| 95th Queue (ft) | 47 | 265 | 881 |
| Link Distance (ft) | 75 | 664 | 891 |
| Upstream Blk Time (\%) | 0 | 1 | 12 |
| Queuing Penalty (veh) | 1 | 0 | 0 |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |

Intersection: 14: 12th St

| Movement | WB | NB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | L | T | R | T |
| Maximum Queue (ft) | 165 | 489 | 576 | 76 |
| Average Queue (ft) | 72 | 120 | 133 | 22 |
| 95th Queue (ft) | 161 | 653 | 674 | 63 |
| Link Distance (ft) | 268 | 1032 | 1032 | 70 |
| Upstream Blk Time (\%) | 5 | 8 | 8 | 0 |
| Queuing Penalty (veh) | 9 | 0 | 0 | 2 |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
|  |  |  |  |  |

SimTraffic Simulation Summary
Scenario 2 - Mitigated
Summary of All Intervals

| Run Number | 10 | 2 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Start Time | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ |
| End Time | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ |
| Total Time (min) | 70 | 70 | 70 | 70 | 70 | 70 | 70 |
| Time Recorded (min) | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| \# of Intervals | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| \# of Recorded Intervals | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Vehs Entered | 4134 | 4198 | 1990 | 4083 | 4063 | 4096 | 3841 |
| Vehs Exited | 4050 | 4082 | 1711 | 4010 | 4002 | 4084 | 3711 |
| Starting Vehs | 208 | 218 | 196 | 244 | 215 | 224 | 250 |
| Ending Vehs | 292 | 334 | 475 | 317 | 276 | 236 | 380 |
| Travel Distance (mi) | 2361 | 2366 | 983 | 2318 | 2306 | 2363 | 2140 |
| Travel Time (hr) | 348.0 | 340.7 | 1160.1 | 444.6 | 415.7 | 324.8 | 541.4 |
| Total Delay (hr) | 245.5 | 237.6 | 1117.4 | 344.2 | 315.5 | 222.4 | 448.7 |
| Total Stops | 9336 | 9397 | 3787 | 9022 | 9750 | 8605 | 10237 |
| Fuel Used (gal) | 138.5 | 137.4 | 288.8 | 159.3 | 153.5 | 133.6 | 178.1 |

## Summary of All Intervals

| Run Number | 9 | Avg |
| :--- | ---: | ---: |
| Start Time | $6: 57$ | $6: 57$ |
| End Time | $8: 07$ | $8: 07$ |
| Total Time (min) | 70 | 70 |
| Time Recorded (min) | 60 | 60 |
| \# of Intervals | 3 | 3 |
| \# of Recorded Intervals | 2 | 2 |
| Vehs Entered | 4112 | 3813 |
| Vehs Exited | 4075 | 3718 |
| Starting Vehs | 179 | 218 |
| Ending Vehs | 216 | 312 |
| Travel Distance (mi) | 2359 | 2150 |
| Travel Time (hr) | 303.5 | 484.9 |
| Total Delay (hr) | 200.9 | 391.5 |
| Total Stops | 7975 | 8512 |
| Fuel Used (gal) | 128.1 | 164.7 |

Interval \#0 Information Seeding

| Start Time | $6: 57$ |
| :--- | :---: |
| End Time | $7: 07$ |
| Total Time (min) | 10 |
| Volumes adjusted by PHF, Growth Factors. |  |
|  |  |

Interval \#1 Information Recording1

| Start Time | $7: 07$ |
| :--- | :---: | :--- |
| End Time | $7: 22$ |
| Total Time (min) | 15 |
| Volumes adjusted by PHF, Growth Factors. |  |


| Run Number | 10 | 2 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vehs Entered | 1151 | 1134 | 927 | 1119 | 1144 | 1129 | 1130 |
| Vehs Exited | 1059 | 1058 | 880 | 1021 | 1018 | 1060 | 1030 |
| Starting Vehs | 208 | 218 | 196 | 244 | 215 | 224 | 250 |
| Ending Vehs | 300 | 294 | 243 | 342 | 341 | 293 | 350 |
| Travel Distance (mi) | 613 | 601 | 505 | 598 | 595 | 609 | 583 |
| Travel Time (hr) | 69.4 | 72.8 | 78.3 | 78.8 | 70.7 | 74.9 | 87.5 |
| Total Delay (hr) | 42.8 | 46.5 | 56.2 | 52.9 | 44.9 | 48.4 | 62.5 |
| Total Stops | 2449 | 2243 | 1760 | 2349 | 2398 | 2488 | 2651 |
| Fuel Used (gal) | 31.4 | 31.7 | 30.8 | 33.1 | 30.9 | 32.6 | 34.8 |

Interval \#1 Information Recording1

| Start Time | $7: 07$ |  |
| :--- | ---: | ---: |
| End Time |  |  |
| Total Time (min) |  |  |
| Volumes adjusted by PHF, Growth Factors. |  |  |
| Run Number |  |  |
| Vehs Entered | 9 | Avg |
| Vehs Exited | 1140 | 1108 |
| Starting Vehs | 1037 | 1018 |
| Ending Vehs | 179 | 218 |
| Travel Distance (mi) | 282 | 301 |
| Travel Time (hr) | 594 | 587 |
| Total Delay (hr) | 58.7 | 73.9 |
| Total Stops | 32.8 | 48.4 |
| Fuel Used (gal) | 2008 | 2289 |
|  | 28.3 | 31.7 |

Interval \#2 Information Recording2

| Start Time | $7: 22$ |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

## Interval \#2 Information Recording2

| Start Time | $7: 22$ |  |
| :--- | ---: | ---: |
| End Time | $8: 07$ |  |
| Total Time (min) | 45 |  |
| Volumes adjusted by Growth Factors, Anti PHF. |  |  |
| Run Number | 9 | Avg |
| Vehs Entered | 2972 | 2708 |
| Vehs Exited | 3038 | 2692 |
| Starting Vehs | 282 | 301 |
| Ending Vehs | 216 | 312 |
| Travel Distance (mi) | 1765 | 1562 |
| Travel Time (hr) | 244.7 | 411.0 |
| Total Delay (hr) | 168.0 | 343.1 |
| Total Stops | 5967 | 6224 |
| Fuel Used (gal) | 99.8 | 133.0 |

## Arterial Level of Service: NB 13th St

| Cross Street | Node | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Oak St | 1 | 18.0 | 29.7 | 0.3 | 40 |
| Total |  | 18.0 | 29.7 | 0.3 | 40 |

Arterial Level of Service: SB 13th St

| Cross Street | Node | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| May St | 2 | 131.4 | 172.3 | 0.3 | 7 |
|  | 13 | 5.1 | 13.6 | 0.1 | 15 |
| Taylor | 3 | 8.1 | 18.6 | 0.1 | 13 |
| A St | 4 | 20.6 | 43.7 | 0.1 | 13 |
| Belmont | 5 | 9.9 | 17.2 | 0.0 | 10 |
| Total | 25 | 1.0 | 5.6 | 0.0 | 20 |

## Arterial Level of Service: NB 12th St

| Cross Street | Node | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Union | 6 | 14.1 | 28.7 | 0.1 | 10 |
| Wilson | 7 | 4.9 | 11.7 | 0.0 | 15 |
| Pine | 8 | 17.5 | 40.6 | 0.1 | 13 |
| Taylor | 9 | 1.3 | 3.7 | 0.0 | 15 |
| May St | 10 | 26.6 | 52.0 | 0.1 | 10 |
| Total |  | 64.6 | 136.7 | 0.4 | 11 |

Intersection: 1: 13th St \& Oak St

| Movement | EB | EB | WB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | T | L | R |
| Maximum Queue (ft) | 772 | 175 | 225 | 915 | 566 | 255 |
| Average Queue (ft) | 387 | 161 | 221 | 710 | 286 | 103 |
| 95th Queue (ft) | 794 | 215 | 239 | 1184 | 509 | 258 |
| Link Distance (ft) | 833 |  |  | 898 | 1603 |  |
| Upstream Blk Time (\%) | 11 |  |  | 40 |  |  |
| Queuing Penalty (veh) | 0 |  |  | 0 |  |  |
| Storage Bay Dist (ft) |  | 150 | 200 |  |  | 230 |
| Storage Blk Time (\%) | 16 | 22 | 60 | 0 | 18 | 0 |
| Queuing Penalty (veh) | 76 | 51 | 133 | 1 | 19 | 1 |

Intersection: 2: 13th St \& May St

| Movement | EB | EB | WB | WB | WB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | R | L | T | R | TR |
| Maximum Queue (ft) | 259 | 139 | 223 | 315 | 218 | 1593 |
| Average Queue (ft) | 106 | 59 | 156 | 136 | 104 | 1266 |
| 95th Queue (ft) | 351 | 120 | 244 | 277 | 187 | 1927 |
| Link Distance (ft) | 816 |  |  | 316 | 316 | 1603 |
| Upstream Blk Time (\%) | 3 |  |  | 7 | 0 | 10 |
| Queuing Penalty (veh) | 0 |  |  | 38 | 0 | 83 |
| Storage Bay Dist (ft) |  | 120 | 200 |  |  |  |
| Storage Blk Time (\%) | 2 | 6 | 12 | 0 |  |  |
| Queuing Penalty (veh) | 2 | 5 | 20 | 1 |  |  |

Intersection: 3: 13th St \& Taylor

| Movement | EB | WB | SB | B13 |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | TR | LT | LTR | T |
| Maximum Queue (ft) | 107 | 210 | 322 | 224 |
| Average Queue (ft) | 30 | 96 | 95 | 44 |
| 95th Queue (ft) | 96 | 194 | 319 | 204 |
| Link Distance (ft) | 603 | 229 | 271 | 234 |
| Upstream Blk Time (\%) |  | 2 | 11 | 9 |
| Queuing Penalty (veh) |  | 3 | 126 | 102 |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 4: 13th St \& A St

| Movement | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| Directions Served | TR | LT | LTR |
| Maximum Queue (ft) | 67 | 126 | 569 |
| Average Queue (ft) | 17 | 45 | 225 |
| 95th Queue (ft) | 52 | 99 | 735 |
| Link Distance (ft) | 743 | 209 | 732 |
| Upstream Blk Time (\%) |  |  | 11 |
| Queuing Penalty (veh) |  | 126 |  |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |

Intersection: 5: 13th St \& Belmont

| Movement | EB | EB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | LT | LT | TR |
| Maximum Queue (ft) | 371 | 174 | 177 | 219 | 236 |
| Average Queue (ft) | 199 | 71 | 76 | 133 | 134 |
| 95th Queue (ft) | 710 | 163 | 161 | 221 | 237 |
| Link Distance (ft) | 886 |  | 196 | 186 | 186 |
| Upstream Blk Time (\%) | 14 |  | 0 | 12 | 4 |
| Queuing Penalty (veh) | 0 |  | 1 | 73 | 25 |
| Storage Bay Dist (ft) |  | 200 |  |  |  |
| Storage Blk Time (\%) | 17 | 1 |  |  |  |
| Queuing Penalty (veh) | 33 | 1 |  |  |  |

Intersection: 6: 12th St \& Belmont/Union

| Movement | EB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LT | TR | LT | TR |
| Maximum Queue (ft) | 205 | 188 | 325 | 335 |
| Average Queue (ft) | 114 | 73 | 112 | 169 |
| 95th Queue (ft) | 226 | 220 | 336 | 382 |
| Link Distance (ft) | 196 | 693 | 287 | 287 |
| Upstream Blk Time (\%) | 22 |  | 13 | 17 |
| Queuing Penalty (veh) | 22 |  | 91 | 119 |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |

## Intersection: 7: 12th St \& A St/Wilson

| Movement | EB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LT | TR | L | TR |
| Maximum Queue (ft) | 203 | 451 | 112 | 228 |
| Average Queue (ft) | 102 | 264 | 7 | 95 |
| 95th Queue (ft) | 218 | 640 | 64 | 239 |
| Link Distance (ft) | 209 | 706 | 196 | 196 |
| Upstream Blk Time (\%) | 9 | 11 | 1 | 3 |
| Queuing Penalty (veh) | 6 | 0 | 4 | 21 |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

Intersection: 8: 12th St \& Pine

| Movement | WB | NB |
| :--- | ---: | ---: |
| Directions Served | R | TR |
| Maximum Queue (ft) | 874 | 631 |
| Average Queue (ft) | 767 | 252 |
| 95th Queue (ft) | 1133 | 623 |
| Link Distance (ft) | 850 | 650 |
| Upstream Blk Time (\%) | 77 | 1 |
| Queuing Penalty (veh) | 0 | 16 |
| Storage Bay Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |

Intersection: 9: 12th St \& Taylor

| Movement | EB | NB |
| :--- | ---: | ---: |
| Directions Served | L | LT |
| Maximum Queue (ft) | 177 | 82 |
| Average Queue (ft) | 68 | 28 |
| 95th Queue (ft) | 173 | 70 |
| Link Distance (ft) | 229 | 30 |
| Upstream Blk Time (\%) | 2 | 9 |
| Queuing Penalty (veh) | 1 | 113 |
| Storage Bay Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |

## Intersection: 10: 12th St \& May St

| Movement | WB | NB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | T | L | R |
| Maximum Queue (ft) | 109 | 560 | 125 |
| Average Queue (ft) | 88 | 319 | 111 |
| 95th Queue (ft) | 99 | 603 | 166 |
| Link Distance (ft) | 74 | 558 |  |
| Upstream Blk Time (\%) | 50 | 6 |  |
| Queuing Penalty (veh) | 219 | 69 |  |
| Storage Bay Dist (ft) |  |  | 100 |
| Storage Blk Time (\%) |  | 22 | 6 |
| Queuing Penalty (veh) |  | 140 | 39 |

## Intersection: 11: May St

| Movement | EB | WB | SB | B27 | B26 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | TR | LR | T | T |
| Maximum Queue (ft) | 66 | 270 | 313 | 314 | 405 |
| Average Queue (ft) | 5 | 104 | 272 | 270 | 340 |
| 95th Queue (ft) | 32 | 311 | 305 | 332 | 469 |
| Link Distance (ft) | 74 | 664 | 183 | 184 | 331 |
| Upstream Blk Time (\%) | 0 | 3 | 99 | 97 | 87 |
| Queuing Penalty (veh) | 0 | 0 | 0 | 0 | 0 |
| Storage Bay Dist (ft) |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |

Intersection: 14: 12th St

| Movement | NB | NB | B25 |
| :--- | ---: | ---: | ---: |
| Directions Served | T | T | T |
| Maximum Queue (ft) | 175 | 198 | 7 |
| Average Queue (ft) | 73 | 90 | 0 |
| 95th Queue (ft) | 207 | 223 | 7 |
| Link Distance (ft) | 151 | 151 | 102 |
| Upstream Blk Time (\%) | 22 | 28 |  |
| Queuing Penalty (veh) | 0 | 0 |  |
| Storage Bay Dist (ft) |  |  |  |
| Storage Bk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Network Summary |  |  |  |
| Network wide Queuing Penalty: 1779 |  |  |  |

SimTraffic Simulation Summary
Scenario 3 - Mitigated
Summary of All Intervals

| Run Number | 1 | 10 | 2 | 3 | 5 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Start Time | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ | $6: 57$ |
| End Time | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ | $8: 07$ |
| Total Time (min) | 70 | 70 | 70 | 70 | 70 | 70 | 70 |
| Time Recorded (min) | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| \# of Intervals | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| \# of Recorded Intervals | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Vehs Entered | 4289 | 4156 | 4120 | 4198 | 4280 | 4324 | 4272 |
| Vehs Exited | 4190 | 4006 | 4063 | 4149 | 4167 | 4275 | 4192 |
| Starting Vehs | 206 | 230 | 220 | 216 | 232 | 231 | 238 |
| Ending Vehs | 305 | 380 | 277 | 265 | 345 | 280 | 318 |
| Travel Distance (mi) | 2606 | 2486 | 2523 | 2595 | 2640 | 2643 | 2602 |
| Travel Time (hr) | 341.7 | 371.5 | 318.8 | 262.8 | 377.1 | 288.6 | 375.5 |
| Total Delay (hr) | 229.5 | 264.4 | 210.4 | 151.0 | 263.7 | 174.8 | 263.6 |
| Total Stops | 10101 | 9350 | 9299 | 7515 | 11636 | 9995 | 10306 |
| Fuel Used (gal) | 142.1 | 146.9 | 135.5 | 124.6 | 151.9 | 130.9 | 151.1 |

Summary of All Intervals

| Run Number | 9 | Avg |
| :--- | ---: | ---: |
| Start Time | $6: 57$ | $6: 57$ |
| End Time | $8: 07$ | $8: 07$ |
| Total Time (min) | 70 | 70 |
| Time Recorded (min) | 60 | 60 |
| \# of Intervals | 3 | 3 |
| \# of Recorded Intervals | 2 | 2 |
| Vehs Entered | 4297 | 4242 |
| Vehs Exited | 4242 | 4161 |
| Starting Vehs | 214 | 213 |
| Ending Vehs | 269 | 299 |
| Travel Distance (mi) | 2649 | 2593 |
| Travel Time (hr) | 345.1 | 335.1 |
| Total Delay (hr) | 231.2 | 223.6 |
| Total Stops | 10551 | 9847 |
| Fuel Used (gal) | 144.0 | 140.9 |

Interval \#0 Information Seeding

| Start Time | $6: 57$ |
| :--- | :---: |
| End Time | $7: 07$ |
| Total Time (min) | 10 |
| Volumes adjusted by PHF, Growth Factors. |  |
|  |  |

Interval \#1 Information Recording1

| Start Time | $7: 07$ |
| :--- | :---: | :--- |
| End Time | $7: 22$ |
| Total Time (min) | 15 |
| Volumes adjusted by PHF, Growth Factors. |  |


| Run Number | 1 | 10 | 2 | 3 | 5 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vehs Entered | 1176 | 1202 | 1114 | 1159 | 1229 | 1153 | 1127 |
| Vehs Exited | 1083 | 1135 | 1013 | 1132 | 1133 | 1113 | 1067 |
| Starting Vehs | 206 | 230 | 220 | 216 | 232 | 231 | 238 |
| Ending Vehs | 299 | 297 | 321 | 243 | 328 | 271 | 298 |
| Travel Distance (mi) | 672 | 697 | 642 | 693 | 706 | 686 | 638 |
| Travel Time (hr) | 68.4 | 58.3 | 70.9 | 61.4 | 70.0 | 63.4 | 77.3 |
| Total Delay (hr) | 39.4 | 28.4 | 43.3 | 31.5 | 39.6 | 33.8 | 49.8 |
| Total Stops | 2551 | 2150 | 2538 | 2003 | 2762 | 2314 | 2523 |
| Fuel Used (gal) | 32.3 | 30.7 | 32.1 | 31.4 | 33.4 | 31.1 | 33.6 |

Interval \#1 Information Recording1

| Start Time | $7: 07$ |  |
| :--- | ---: | ---: |
| End Time | $7: 22$ |  |
| Total Time (min) | 15 |  |
| Volumes adjusted by PHF, Growth Factors. |  |  |
| Run Number | 9 | Avg |
| Vehs Entered | 1219 | 1170 |
| Vehs Exited | 1115 | 1098 |
| Starting Vehs | 214 | 213 |
| Ending Vehs | 318 | 294 |
| Travel Distance (mi) | 696 | 679 |
| Travel Time (hr) | 72.5 | 67.8 |
| Total Delay (hr) | 42.5 | 38.6 |
| Total Stops | 2721 | 2444 |
| Fuel Used (gal) | 33.4 | 32.2 |

Interval \#2 Information Recording2

| Start Time | 7:22 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| End Time | 8:07 |  |  |  |  |  |  |
| Total Time (min) | 45 |  |  |  |  |  |  |
| Volumes adjusted by Growth Factors, Anti PHF. |  |  |  |  |  |  |  |
| Run Number | 1 | 10 | 2 | 3 | 5 | 7 | 8 |
| Vehs Entered | 3113 | 2954 | 3006 | 3039 | 3051 | 3171 | 3145 |
| Vehs Exited | 3107 | 2871 | 3050 | 3017 | 3034 | 3162 | 3125 |
| Starting Vehs | 299 | 297 | 321 | 243 | 328 | 271 | 298 |
| Ending Vehs | 305 | 380 | 277 | 265 | 345 | 280 | 318 |
| Travel Distance (mi) | 1934 | 1789 | 1881 | 1902 | 1935 | 1956 | 1964 |
| Travel Time (hr) | 273.3 | 313.2 | 247.9 | 201.4 | 307.1 | 225.2 | 298.2 |
| Total Delay (hr) | 190.1 | 236.1 | 167.1 | 119.5 | 224.1 | 140.9 | 213.8 |
| Total Stops | 7550 | 7200 | 6761 | 5512 | 8874 | 7681 | 7783 |
| Fuel Used (gal) | 109.8 | 116.2 | 103.4 | 93.2 | 118.5 | 99.8 | 117.5 |

## Interval \#2 Information Recording2

| Start Time | $7: 22$ |  |
| :--- | ---: | ---: |
| End Time | $8: 07$ |  |
| Total Time (min) | 45 |  |
| Volumes adjusted by Growth Factors, Anti PHF. |  |  |
| Run Number | 9 | Avg |
| Vehs Entered | 3078 | 3064 |
| Vehs Exited | 3127 | 3063 |
| Starting Vehs | 318 | 294 |
| Ending Vehs | 269 | 299 |
| Travel Distance (mi) | 1953 | 1914 |
| Travel Time (hr) | 272.6 | 267.4 |
| Total Delay (hr) | 188.7 | 185.0 |
| Total Stops | 7830 | 7397 |
| Fuel Used (gal) | 110.5 | 108.6 |

## Arterial Level of Service: NB 13th St

| Cross Street | Node | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Belmont | 5 | 9.9 | 15.7 | 0.0 | 9 |
| A St | 4 | 2.0 | 8.8 | 0.0 | 19 |
| Taylor | 3 | 8.5 | 29.4 | 0.1 | 18 |
|  | 13 | 10.1 | 19.1 | 0.1 | 12 |
| May St | 2 | 19.2 | 27.1 | 0.1 | 8 |
| Oak St | 1 | 38.1 | 83.9 | 0.3 | 14 |
| Total |  | 87.7 | 184.0 | 0.7 | 13 |

Arterial Level of Service: SB 13th St

|  | Node | Delay <br> $(\mathrm{s} / \mathrm{veh})$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Cross Street | 2 | 109.0 | 151.4 | 0.3 | 8 |
| May St | 13 | 4.4 | 12.8 | 0.1 | 16 |
|  | 3 | 9.2 | 19.0 | 0.1 | 12 |
| Taylor | 4 | 34.7 | 58.7 | 0.1 | 10 |
| A St | 5 | 9.8 | 17.3 | 0.0 | 10 |
| Belmont | 25 | 1.5 | 7.5 | 0.0 | 19 |
| Total |  | 168.6 | 266.7 | 0.7 | 9 |

Arterial Level of Service: NB 12th St

| Cross Street | Node | Delay <br> $(\mathrm{s} /$ veh $)$ | Travel <br> time $(\mathrm{s})$ | Dist <br> $(\mathrm{mi})$ | Arterial <br> Speed |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Union | 6 | 12.0 | 21.0 | 0.1 | 11 |
| Wilson | 7 | 12.1 | 19.4 | 0.0 | 9 |
| Pine | 8 | 35.8 | 69.7 | 0.1 | 9 |
| Taylor | 9 | 0.4 | 2.8 | 0.0 | 20 |
| May St | 10 | 11.6 | 28.5 | 0.1 | 15 |
| Total |  | 71.9 | 141.4 | 0.4 | 11 |

Intersection: 1: 13th St \& Oak St

| Movement | EB | EB | WB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | R | L | T | L | R |
| Maximum Queue (ft) | 790 | 175 | 225 | 898 | 622 | 255 |
| Average Queue (ft) | 370 | 160 | 217 | 557 | 341 | 126 |
| 95th Queue (ft) | 772 | 215 | 253 | 1087 | 590 | 291 |
| Link Distance (ft) | 826 |  |  | 892 | 1618 |  |
| Upstream Blk Time (\%) | 5 |  |  | 24 |  |  |
| Queuing Penalty (veh) | 0 |  |  | 0 |  |  |
| Storage Bay Dist (ft) |  | 150 | 200 |  |  | 230 |
| Storage Blk Time (\%) | 22 | 12 | 48 | 0 | 22 | 0 |
| Queuing Penalty (veh) | 100 | 28 | 108 | 1 | 24 | 1 |

Intersection: 2: 13th St \& May St

| Movement | EB | WB | WB | NB | NB | B13 | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LTR | L | TR | L | TR | T | L | TR |
| Maximum Queue (ft) | 850 | 326 | 321 | 175 | 328 | 335 | 123 | 1545 |
| Average Queue (ft) | 752 | 214 | 210 | 115 | 275 | 162 | 42 | 1158 |
| 95th Queue (ft) | 984 | 333 | 336 | 205 | 397 | 375 | 113 | 1926 |
| Link Distance (ft) | 810 | 310 | 310 |  | 235 | 271 | 1618 |  |
| Upstream Blk Time (\%) | 62 | 4 | 2 |  | 23 | 6 |  | 3 |
| Queuing Penalty (veh) | 0 | 12 | 7 |  | 206 | 52 |  | 27 |
| Storage Bay Dist (ft) |  |  |  | 150 |  |  | 100 |  |
| Storage Blk Time (\%) |  |  |  | 7 | 26 |  | 7 | 47 |
| Queuing Penalty (veh) |  |  |  | 55 | 26 |  | 55 | 12 |

Intersection: 3: 13th St \& Taylor

| Movement | EB | WB | NB | NB | SB | SB | B13 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | L | TR | L | TR | T |
| Maximum Queue (ft) | 147 | 206 | 119 | 524 | 102 | 360 | 273 |
| Average Queue (ft) | 57 | 123 | 30 | 119 | 13 | 183 | 59 |
| 95th Queue (ft) | 132 | 243 | 84 | 411 | 58 | 422 | 230 |
| Link Distance (ft) | 597 | 211 |  | 732 |  | 271 | 235 |
| Upstream Blk Time (\%) |  | 20 |  | 0 |  | 9 | 2 |
| Queuing Penalty (veh) |  | 13 |  | 2 |  | 99 | 19 |
| Storage Bay Dist (ft) |  |  | 100 |  | 100 |  |  |
| Storage Blk Time (\%) |  |  | 0 | 7 | 0 | 15 |  |
| Queuing Penalty (veh) |  |  | 2 | 2 | 0 | 2 |  |

Intersection: 4: 13th St \& A St

| Movement | EB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | L | TR | L | TR |
| Maximum Queue (ft) | 220 | 208 | 34 | 170 | 119 | 754 |
| Average Queue (ft) | 98 | 128 | 5 | 30 | 24 | 610 |
| 95th Queue (ft) | 268 | 237 | 24 | 116 | 75 | 930 |
| Link Distance (ft) | 751 | 197 |  | 180 |  | 732 |
| Upstream Blk Time (\%) |  | 17 |  | 0 |  | 4 |
| Queuing Penalty (veh) |  | 13 |  | 1 |  | 44 |
| Storage Bay Dist (ft) |  |  | 10 |  | 100 |  |
| Storage Blk Time (\%) |  |  | 4 | 1 | 0 | 29 |
| Queuing Penalty (veh) |  |  | 40 | 0 | 0 | 7 |

Intersection: 5: 13th St \& Belmont

| Movement | EB | EB | WB | NB | B25 | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | TR | TR | T | L | TR |
| Maximum Queue (ft) | 124 | 543 | 196 | 236 | 240 | 124 | 219 |
| Average Queue (ft) | 71 | 244 | 113 | 197 | 131 | 47 | 202 |
| 95th Queue (ft) | 144 | 472 | 204 | 296 | 292 | 112 | 239 |
| Link Distance (ft) |  | 892 | 187 | 146 | 149 |  | 180 |
| Upstream Blk Time (\%) |  | 0 | 3 | 19 | 11 |  | 22 |
| Queuing Penalty (veh) |  | 0 | 5 | 165 | 93 |  | 248 |
| Storage Bay Dist (ft) | 100 |  |  |  |  | 100 |  |
| Storage Blk Time (\%) | 4 | 46 |  |  |  | 2 | 26 |
| Queuing Penalty (veh) | 9 | 32 |  |  |  | 17 | 13 |

## Intersection: 6: 12th St \& Belmont/Union

| Movement | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | LT | TR | LTR |
| Maximum Queue (ft) | 148 | 70 | 243 |
| Average Queue (ft) | 55 | 18 | 98 |
| 95th Queue (ft) | 123 | 55 | 299 |
| Link Distance (ft) | 187 | 705 | 266 |
| Upstream Blk Time (\%) | 2 |  | 15 |
| Queuing Penalty (veh) | 2 |  | 97 |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |

## Intersection: 7: 12th St \& A St/Wilson

| Movement | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| Directions Served | LT | TR | LTR |
| Maximum Queue (ft) | 77 | 187 | 209 |
| Average Queue (ft) | 23 | 67 | 82 |
| 95th Queue (ft) | 61 | 178 | 242 |
| Link Distance (ft) | 197 | 712 | 197 |
| Upstream Blk Time (\%) |  |  | 17 |
| Queuing Penalty (veh) |  |  | 86 |
| Storage Bay Dist (ft) |  |  |  |
| Storage Blk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |

Intersection: 8: 12th St \& Pine

| Movement | WB | NB |
| :--- | ---: | ---: |
| Directions Served | R | TR |
| Maximum Queue (ft) | 275 | 464 |
| Average Queue (ft) | 109 | 183 |
| 95th Queue (ft) | 294 | 632 |
| Link Distance (ft) | 850 | 650 |
| Upstream Blk Time (\%) |  | 12 |
| Queuing Penalty (veh) |  | 53 |
| Storage Bay Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |

Intersection: 9: 12th St \& Taylor

| Movement | EB | NB |
| :--- | ---: | :--- |
| Directions Served | L | LT |
| Maximum Queue (ft) | 45 | 66 |
| Average Queue (ft) | 17 | 20 |
| 95th Queue (ft) | 46 | 63 |
| Link Distance (ft) | 211 | 30 |
| Upstream Blk Time (\%) |  | 18 |
| Queuing Penalty (veh) |  | 97 |
| Storage Bay Dist (ft) |  |  |
| Storage Blk Time (\%) |  |  |
| Queuing Penalty (veh) |  |  |

## Intersection: 10: 12th St \& May St

| Movement | EB | WB | WB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | T | L | R |
| Maximum Queue (ft) | 121 | 92 | 101 | 297 | 125 |
| Average Queue (ft) | 51 | 65 | 77 | 92 | 79 |
| 95th Queue (ft) | 97 | 96 | 105 | 226 | 138 |
| Link Distance (ft) | 310 | 74 | 74 | 566 |  |
| Upstream Blk Time (\%) |  | 7 | 12 |  |  |
| Queuing Penalty (veh) |  | 14 | 26 |  |  |
| Storage Bay Dist (ft) |  |  |  | 4 | 2 |
| Storage Blk Time (\%) |  |  |  | 12 | 4 |

## Intersection: 11: May St

| Movement | EB | WB | SB | B27 | B26 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | LT | TR | LR | T | T |
| Maximum Queue (ft) | 58 | 120 | 255 | 114 | 3 |
| Average Queue (ft) | 4 | 57 | 114 | 8 | 0 |
| 95th Queue (ft) | 26 | 97 | 219 | 63 | 2 |
| Link Distance (ft) | 74 | 664 | 169 | 184 | 331 |
| Upstream Blk Time (\%) | 0 |  | 8 | 0 |  |
| Queuing Penalty (veh) | 0 |  | 0 | 0 |  |
| Storage Bay Dist (ft) |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |

Intersection: 14: 12th/12th St

| Movement | NB | NB | SE |
| :--- | ---: | ---: | ---: |
| Directions Served | L | T | R |
| Maximum Queue (ft) | 459 | 467 | 7 |
| Average Queue (ft) | 220 | 197 | 0 |
| 95th Queue (ft) | 601 | 597 | 7 |
| Link Distance (ft) | 503 | 503 | 149 |
| Upstream Blk Time (\%) | 13 | 13 |  |
| Queuing Penalty (veh) | 0 | 0 |  |
| Storage Bay Dist (ft) |  |  |  |
| Storage Bk Time (\%) |  |  |  |
| Queuing Penalty (veh) |  |  |  |
| Network Summary |  |  |  |
| Network wide Queuing Penalty: 1931 |  |  |  |

APPENDIX F: MITIGATED ROUNDABOUT CONCEPT


- Hybrid multi-lane (dual SBT, single lane all other lanes)
- $140^{\prime}$ ICD
- ODOT standard single lane: $\mathbf{1 6 5}^{\prime}$
- $140^{\prime}$ provides minimal opportunity for central landscaped island. Changing May St. design vehicle to WB-40 would increase central island landscape/art opportunity.
- Design Vehicle: WB-67
- Footprint offset of $12^{\prime}$ for bike/ped
- *Does not show bike facility transitions on approaches

APPENDIX G: NCHRP 562 PEDESTRIAN CROSSING EVALUATION

## GUIDELINES FOR PEDESTRIAN CROSSING TREATMENTS

This spreadsheet combines Worksheet 1 and Worksheet 2 (Appendix A, pages 69-70) of TCRP Report 112/NCHRP Report 562 (Improvina Pedestrian Safety at Unsianalized Intersections) into an electronic format. This spreadsheet should be used in conjunction with, and not independent of, Appendix A documentation.


## This spreadsheet is still under development, please inform TTI if errors are identified

 Blue fields contain descriptive informationGreen fields are required and must be completed.
Tan fields are adjustments that are filled out only under certain conditions (follow instructions to the left of the cell). Gray fields are automatically calculated and should not be edited.



This worksheet provides general recommendations on pedestrian crossing treatments to consider at unsignalized intersections; in all cases, engineering judgment should be used in selecting a specific treatment for installation. This worksheet does not apply to school crossings. In addition to the results provided by this worksheet, users should consider whether a pedestrian treatment could present an increased safety risk to pedestrians, such as where there is poor sight distance, complex geometrics, or nearby traffic signals.

## GUIDELINES FOR PEDESTRIAN CROSSING TREATMENTS

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Because the volume in Step 4 e is different from the volume in Step 3a, the graph may show a different result than the Treatment Category above.

This worksheet provides general recommendations on pedestrian crossing treatments to consider at unsignalized intersections; in all cases, engineering judgment should be used in selecting a specific treatment for installation. This worksheet does not apply to school crossings. In addition to the results provided by this worksheet, users should consider whether a pedestrian treatment could present an increased safety risk to pedestrians, such as where there is poor sight distance, complex geometrics, or nearby traffic signals.

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$\square$ Blue fields contain descriptive information.
Green fields are required and must be completed.
Tan fields are adjustments that are filled out only under certain conditions (follow instructions to the left of the cell). Gray fields are automatically calculated and should not be edited.

| Analyst and Site Information |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Analyst | ALC | Major Street Minor Street or Location Peak Hour | 12th St - Scenario 2 |  |  |
| Analysis Date D | Dec-21 |  | Varies |  |  |
| Data Collection Date | N/A |  | N/A |  |  |
| Step 1: Select worksheet: |  |  |  |  |  |
| Posted or statutory speed limit (or 85th percentile speed) on the major street (mph) |  |  |  | $1 a$ | 25 |
| Is the population of the surrounding area $<10,000$ ? (enter YES or $\boldsymbol{N O}$ ) |  |  |  | $1 b$ | NO |
| Step 2: Does the crossing meet minimum pedestrian volumes to be considered for a traffic control device? |  |  |  |  |  |
| Peak-hour pedestrian volume (ped/h), $\mathrm{V}_{\mathrm{p}}$ |  |  |  | $2 a$ | 35 |
| Result: Go to step 3. |  |  |  |  |  |
| Step 3: Does the crossing meet the pedestrian warrant for a traffic signal? |  |  |  |  |  |
| Major road volume, total of both approaches during peak hour (veh/h), $\mathrm{V}_{\text {maj-s }}$ |  |  |  | $3 a$ | 1360 |
| [Calculated automatically] Preliminary (before min. threshold) peak hour pedestrian volume to meet warrant |  |  |  | $3 b$ | 154 |
| [Calculated automatically] Minimum required peak hour pedestrian volume to meet traffic signal warrant |  |  |  | 3 c | 154 |
| Is 15th percentile crossing speed of pedestrians less than $3.5 \mathrm{ft} / \mathrm{s}(1.1 \mathrm{~m} / \mathrm{s}$ )? (enter $\boldsymbol{Y}$ ES or $\boldsymbol{N O}$ ) |  |  |  | $3 d$ | NO |
| If 15th percentile crossing speed of pedestrians is less than $3.5 \mathrm{ft} / \mathrm{s}$ $(1.1 \mathrm{~m} / \mathrm{s})$, then reduce $3 c$ by up to $50 \%$. |  |  | \% rate of reduction for $3 c$ (up to 50\%) | 3 e | 0\% |
|  |  |  | e or $3 c$ | $3 f$ | 154 |
| Result: The signal warrant is not met. Go to step 4. |  |  |  |  |  |
| Step 4: Estimate pedestrian delay. |  |  |  |  |  |
| Pedestrian crossing distance, curb to curb (ft), L |  |  |  | $4 a$ | 12 |
| Pedestrian walking speed (ft/s), $\mathrm{S}_{\mathrm{p}}$ (suggested speed $=3.5 \mathrm{ft} / \mathrm{s}$ ) |  |  |  | $4 b$ | 3.5 |
| Pedestrian start-up time and end clearance time (s), $\mathrm{t}_{\mathrm{s}}$ (suggested start-up time $=3 \mathrm{sec}$ ) |  |  |  | $4 c$ | 3 |
| [Calculated automatically] Critical gap required for crossing pedestrian (s), $\mathrm{t}_{\mathrm{c}}$ |  |  |  | $4 d$ | 6 |
| Major road volume, total both approaches OR approach being crossed if raised median island is present, during peak hour (veh/h), $\mathrm{V}_{\text {maj-d }}$ |  |  |  | $4 e$ | 1360 |
| Major road flow rate (veh/s), v |  |  |  | $4 f$ | 0.38 |
| Average pedestrian delay (s/person), $\mathrm{d}_{\mathrm{p}}$ |  |  |  | $4 g$ | 21 |
| Total pedestrian delay (h), $D_{p}$ The value in 4h is the calculated estimated delay for all pedestrians crossing the major roadway without a crossing treatment (assumes $0 \%$ compliance). If the actual total pedestrian delay has been measured at the site, that value can be entered in 4 i to replace the calculated value in 4 h . |  |  |  | 4h | 0.2 |
|  |  |  |  | $4 i$ |  |
| Step 5: Select treatment based up on total pedestrian delay and expected motorist compliance. |  |  |  |  |  |
| Expected motorist compliance at pedestrian crossings in region: enter HIGH for High Compliance or LOW for Low Compliance |  |  |  | $5 a$ | HIGH |
| Treatment Category: |  | CROSSWALK |  |  |  |



This worksheet provides general recommendations on pedestrian crossing treatments to consider at unsignalized intersections; in all cases, engineering judgment should be used in selecting a specific treatment for installation. This worksheet does not apply to school crossings. In addition to the results provided by this worksheet, users should consider whether a pedestrian treatment could present an increased safety risk to pedestrians, such as where there is poor sight distance, complex geometrics, or nearby traffic signals.

## GUIDELINES FOR PEDESTRIAN CROSSING TREATMENTS

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## Key

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Green fields are required and must be completed.
Tan fields are adjustments that are filled out only under certain conditions (follow instructions to the left of the cell). Gray fields are automatically calculated and should not be edited.



This worksheet provides general recommendations on pedestrian crossing treatments to consider at unsignalized intersections; in all cases, engineering judgment should be used in selecting a specific treatment for installation. This worksheet does not apply to school crossings. In addition to the results provided by this worksheet, users should consider whether a pedestrian treatment could present an increased safety risk to pedestrians, such as where there is poor sight distance, complex geometrics, or nearby traffic signals.

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Green fields are required and must be completed.
Tan fields are adjustments that are filled out only under certain conditions (follow instructions to the left of the cell). Gray fields are automatically calculated and should not be edited.

| Analyst and Site Information |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Analyst | ALC | Major Street Minor Street or Location Peak Hour | 13th St - Scenario 3 |  |  |
| Analysis Date | Dec-21 |  | Varies |  |  |
| Data Collection Date | N/A |  | N/A |  |  |
| Step 1: Select worksheet: |  |  |  |  |  |
| Posted or statutory speed limit (or 85th percentile speed) on the major street (mph) |  |  |  | $1 a$ | 25 |
| Is the population of the surrounding area <10,000? (enter YES or NO) |  |  |  | 1b | NO |
| Step 2: Does the crossing meet minimum pedestrian volumes to be considered for a traffic control device? |  |  |  |  |  |
| Peak-hour pedestrian volume (ped/h), $\mathrm{V}_{\mathrm{p}}$ |  |  |  | $2 a$ | 20 |
| Result: Go to step 3. |  |  |  |  |  |
| Step 3: Does the crossing meet the pedestrian warrant for a traffic signal? |  |  |  |  |  |
| Major road volume, total of both approaches during peak hour (veh/h), $\mathrm{V}_{\text {maj-s }}$ |  |  |  | $3 a$ | 1740 |
| [Calculated automatically] Preliminary (before min. threshold) peak hour pedestrian volume to meet warrant |  |  |  | $3 b$ | 133 |
| [Calculated automatically] Minimum required peak hour pedestrian volume to meet traffic signal warrant |  |  |  | 3 c | 133 |
| Is 15th percentile crossing speed of pedestrians less than $3.5 \mathrm{ft} / \mathrm{s}(1.1 \mathrm{~m} / \mathrm{s}$ )? (enter $\boldsymbol{Y E S}$ or $\boldsymbol{N} \boldsymbol{O}$ ) |  |  |  | $3 d$ | NO |
| If 15th percentile crossing speed of pedestrians is less than $3.5 \mathrm{ft} / \mathrm{s}$ $(1.1 \mathrm{~m} / \mathrm{s})$, then reduce $3 c$ by up to $50 \%$. |  |  | duction for 3 c (up to 50\%) | $3 e$ | 0\% |
|  |  |  | e or 3c | $3 f$ | 133 |
| Result: The signal warrant is not met. Go to step 4. |  |  |  |  |  |
| Step 4: Estimate pedestrian delay. |  |  |  |  |  |
| Pedestrian crossing distance, curb to curb (ft), L |  |  |  | $4 a$ | 36 |
| Pedestrian walking speed (ft/s), $\mathrm{S}_{\mathrm{p}}$ (suggested speed $=3.5 \mathrm{ft} / \mathrm{s}$ ) |  |  |  | $4 b$ | 3.5 |
| Pedestrian start-up time and end clearance time (s), $\mathrm{t}_{\mathrm{s}}$ (suggested start-up time $=3 \mathrm{sec}$ ) |  |  |  | 4 c | 3 |
| [Calculated automatically] Critical gap required for crossing pedestrian ( s ), $\mathrm{t}_{\mathrm{c}}$ |  |  |  | $4 d$ | 13 |
| Major road volume, total both approaches OR approach being crossed if raised median island is present, during peak hour (veh/h), $\mathrm{V}_{\text {maj-d }}$ |  |  |  | $4 e$ | 1740 |
| Major road flow rate (veh/s), v |  |  |  | $4 f$ | 0.48 |
| Average pedestrian delay ( $\mathrm{s} /$ person), $\mathrm{d}_{\mathrm{p}}$ |  |  |  | $4 g$ | 1210 |
| Total pedestrian delay (h), $D_{p}$ The value in $4 h$ is the calculated estimated delay for all pedestrians crossing the major roadway without a crossing treatment (assumes $0 \%$ compliance). If the actual total pedestrian delay has been measured at the site, that value can be entered in 4 i to replace the calculated value in 4 h . |  |  |  | 4h | 6.7 |
|  |  |  |  | $4 i$ |  |
| Step 5: Select treatment based up on total pedestrian delay and expected motorist compliance. |  |  |  |  |  |
| Expected motorist compliance at pedestrian crossings in region: enter HIGH for High Compliance or LOW for Low Compliance |  |  |  | $5 a$ | HIGH |
| Treatment Category: $\quad$ ACTIVE OR ENHANCED |  |  |  |  |  |



This worksheet provides general recommendations on pedestrian crossing treatments to consider at unsignalized intersections; in all cases, engineering judgment should be used in selecting a specific treatment for installation. This worksheet does not apply to school crossings. In addition to the results provided by this worksheet, users should consider whether a pedestrian treatment could present an increased safety risk to pedestrians, such as where there is poor sight distance, complex geometrics, or nearby traffic signals.

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Because the volume in Step 4 e is different from the volume in Step 3a, the graph may show a different result than the Treatment Category above.

This worksheet provides general recommendations on pedestrian crossing treatments to consider at unsignalized intersections; in all cases, engineering judgment should be used in selecting a specific treatment for installation. This worksheet does not apply to school crossings. In addition to the results provided by this worksheet, users should consider whether a pedestrian treatment could present an increased safety risk to pedestrians, such as where there is poor sight distance, complex geometrics, or nearby traffic signals.

## APPENDIX C

Heights Streetscape Plan - Full Evaluation of Preliminary Design Alternatives
MIG \#15174.0
2/8/2021

| Evaluation Rating Key |
| :---: |
| Very good alignment with project goals |
| Good alignment with projet toals |
| Average alignment with project gools |
| Poor alignent with project goals |
| Undesirable alignment with project goals |


|  |  | Goal \#1 |  |  | Goal \#2 |  |  |  | Goal \#3 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Evaluation Criteria |  | Provides traffic calming | Accommodates vehicular traffic | Improves intersections | Accommodates parking | Supports the local economy | Supports livability | Adapts Seasonally | Opportunity for creating identity | Supports the Heights as a local destination | Opportunity for enhanced landscape |
| Evaluation Metric |  | 1. Based on how street cross section reinforces target speed (20-25 mph) <br> 2. Potential for additional traffic calming measures | 1. Intersection Operations - v/c ratios, Levels of Service, seconds of delay 2. Travel time from end to end (through the corridor) <br> 3. Accommodates emergency services access based on feedback from police and fire | 1. Truck accessibility (ability to make turns) 2. Improved pedestrian visibility and locations of crosswalks at intersections 3. Relative improvements in safety qualitative assessment, reference Crash Reduction Factors where available, ability to address past crash trends/issues | 1. Based on quantity (compared to TSP) and location of parking | 1. Based on visibility of storefronts <br> 2. Ease of parking and delivery access <br> 3. Ease of access for people walking and biking <br> 4. Impacts to property access | $\begin{aligned} & \text { 1. How the design } \\ & \text { contributes to traffic } \\ & \text { reduction } \\ & \text { 2. Potential diversion of } \\ & \text { traffic through } \\ & \text { neighborhoods and } \\ & \text { lowerclasified streets. } \\ & \text { 3. Access to owowstress } \\ & \text { crossings ffrequency) } \end{aligned}$ | 1. How the cross section might function/be used in winter <br> 2. How the cross section might be maintained in winter | 1. Based on opportunities or areas created to enhance community identity | 1. How the alternative improves local access | 1. How the alternative enhances opportunities for street trees, planting and GSI |
| Design Alternative 1: Two-way, two-lane traffic | ${ }^{12 \text { th }}$ |  |  |  |  |  |  |  |  |  |  |
|  | 13th |  |  |  |  |  |  |  |  |  |  |
|  | Street |  |  |  |  |  |  |  |  |  |  |
| Design Alternative 2: One-way, one-lane traffic | ${ }^{12 \text { th }}$ |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Design Alternative 3: Hybrid traffic | 12th |  |  |  |  |  |  |  |  |  |  |
|  | Street |  |  |  |  |  |  |  |  |  |  |
|  | $\left\lvert\, \begin{aligned} & 13 \mathrm{trh} \\ & \text { Street } \end{aligned}\right.$ |  |  |  |  |  |  |  |  |  |  |

## APPENDIX C

Heights Streetscape Plan - Full Evaluation of Preliminary Design Alternatives
MIG \#15174.01
2/8/2021

| Evaluation Rating Key |  |
| :---: | :---: |
|  | Very good alignment with project goals |
|  | Good alignment with project goals |
|  | Average alignment with project goals |
|  | Poor alignment with project goas |

Coorag alignment with project goals
Poor alignment with project goals

| Goal \#4 |  |  |  |  | Goal \#5 | Goal \#7 | Feasibility Criteria |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Provides comfortable places for walking | Provides comfortable places for biking | Aligns with SRTS goals | Improves connections | Connects to planned bike routes | Impacts to utility infrastructure | Creates opportunities for placemaking | Potential cost and funding opportunities for implementation | Potential implementation considerations and construction impact | $\begin{aligned} & \hline \begin{array}{l} \text { Ability to maintain } \\ \text { proposed } \\ \text { improvements } \end{array} \end{aligned}$ | Ease of obtaining ODOT design approval | Property impacts/ROW acquisition |
| 1. Based on space available <br> 2. Separation from traffic and people biking 3. Pedestrian crossing distances on 12th and 13th Streets | 1. Based on facility type provided and predictability for non- bike suers 2. Based on space availible 3. Separation from traffic and people walking | 1. How the alternative aligns with project recommendations (and goals) from the City's SRTS project | 1. Based on how the system improves connections to parks/schools/trails 2. Ability to accommodate transit stop amenities (geometric) 3. Bus stop accessibility proximity to enhanced crossings | 1. Based on transitions to existing/planned bike routes | 1. Potential implications for replacing and maintaining utilities based on where/how infrastructure is located | 1. Based on the number and size of potential gatherings areas (supports lingering, public "third places") 2. Creates/supports opportunities for street closures/festival streets | 1. Higher potential cost is lower rated 2. Higher potential for outside funding is higher rated | 1. General feasibility and ability to implement and phase construction over time 2. Potentially longer construction would be more impactful and lower rated | 1. Does the alternative create unique/additional maintenance needs? (lower maintenance need is rated more favorably) | 1. Potential for easier/simper design approval to be rated more favorably 2. Based on how permittable improvements are through ODOT | Based on how much ight of way would be eeded to implement he design (more area is rated less favorably; plantability) Higher impact to roperties and access is red less favorably |
| ${ }_{\text {fista }}{ }^{\text {ninja }}$ total score) |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  | n/a |  |  | n/a |  |  |  |  |  |  | $n / a$ (just a single total score) |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  | $n / a$ (just a single total score) |
|  | n/a |  |  | n/a |  |  |  |  |  |  |  |

THEHEIGHTS
STREETSCAPE PLAN

CURRENT ADOPTED PLAN - TRANSPORTATION SYSTEM PLAN CIRCULATION + STREET SECTIONS 2011, amended April 202l). This plan has been adopted by the city as the future direction for OR 288 t throught the Heights and has been nopproved by onot


13th STREET

( $50^{\prime}$ R/W $+5^{\prime}$ Utility Easements)
TRANSIT DISCUSSION - Accommodating bus stops in the Heights
Columbia Area Transit (CAT) does not currently have bus stops on 12th and 13th Streets within the Heights project area. The project team has coordinated with CAT to identify potential locations for future bus stops in the Heights. The locations shown are one example for how bus stops might be located; bus stops outside of the project area are not shown. Any changes to current bus stops will be coordinnted with CAT and the specific location, configuration, and design of bus stops will be developed as future street improvements are designed.

( $60^{\prime} \mathrm{R} / \mathrm{W}+10^{\prime}$ Easement)
EXAMPLE OF BuFFered bike lane - 12TH \& 13TH STReETS


( $60^{\prime} \mathrm{R} / \mathrm{W}+10^{\prime}$ Easement)
EXAMPLE OF CONVENTIONAL BIKE LANE - MAY STREET



STREETSCAPE PLAN


1. Limits of sidewalk extend to R/W or existing
$\begin{array}{ll}\text { Parcel Lines } & \text { back of walk, whichever is further. } \\ \text { Roodway } & \text { 2. Trees to be located in a later design phase. } \\ \text { Sidewalk } & \text { 3. Existing driveway locations are not shown and } \\ \text { will be incorporated in a later design phase. }\end{array}$
$\begin{array}{ll}\text { Parcel Lines } & \text { back of walk, whichever is further. } \\ \text { Roodway } & \text { 2. Trees to be located in a later design phase. } \\ \text { Sidewalk } & \text { 3. Existing driveway locations are not shown and } \\ \text { will be incorporated in a later design phase. }\end{array}$



LEGEND
ー ニ Right of Way
$\longrightarrow$ Parcel Lines

- Roodway

Sidewalk
Planting

NOTES

1. Limits of sidewalk extend to R/W or existing back of walk, whichever is further. 2. Trees to be located in a later design phase. 3. Existing driveway locations are not shown and will be incorporated in a later design phase. 4. Property acquisition required. Extents of property acquisition to be determined during design.


13th STREET "GREEN STREET"

(50' R/W + [2] $5^{\prime}$ Utility Easements) EXAMPLE OF SHARED USE PATH-13TH STREET


Source:MAG

12th STREET "PARKING STREET"


## [60'R/W]

TRANSIT DISCUSSION - Accommodating bus stops in the Heights
Columbia Area Transit (CAT) does not currently have bus stops on 12th and 13th Streets within the Heights project area. The project team has coordinated with CAT to identify potentio locations for future bus stops in the Heights. The locations shown are one example for how bus stops might be located; bus stops outside of the project area are not shown. Any changes to current bus stops will be coordinated with CAT and the specific location, configuration, and design of bus stops will be developed as future street improvements are designed.

MAY STREET

( $60^{\prime} \mathrm{R} / \mathrm{W}+10^{\prime}$ Easement)
example of ralsed vegetation Separated bile lane-may street


(2) Paved Splitter Island at Roundabout to Accommodate Truck| Bus Access


| LEGEND | Notes |
| :---: | :---: |
| - ユ Rightof Way | 1. Limits of sidewalk extend to R/W or existing |
| $\square$ Parcel Lines | back of walk, whichever is further. |
| Roodway | 2. Trees to be located in a later design phase. |
| Raised Pavement for Truck Access | 3. Existing driveway locations are not shown and will he incorporated in a later design phose. |
| Sidewalk | 4. Property acquisition required. Extents of |
| Planting | property acquisition to be determined during |
| Bike Lane | design. |



## ROUNDABOUT DISCUSSION

1. The design shown for the double roundabout is conceptual and should only be considered an illustration of potentiol traffic flow. The actual extents of the roundabout design and potential property impacts will be refined if fecommended as part of a refined concept and troffic analysis,


12TH AND I3TH STREETS AT MAY STREET


STREETSCAPE PLAN



[^0]:    ${ }^{1}$ Hood River Heights Urban Renewal Area - Transportation Study, Toole Design, February 7, 2020.

[^1]:    ${ }^{2} 2020$ data obtained from ODOT TransGIS https://gis.odot.state.or.us/transGIS/

[^2]:    ${ }^{3}$ OR 281 is a state highway routed over a City street, where ODOT maintains jurisdiction between the curbs.
    ${ }^{4}$ Typically, ODOT would design to lower v/c ratios in the Highway Design Manual when planning for improvement projects. However, the v/c ratios in the 1999 Oregon Highway Plan are more consistent with the long-range vision for this area as expressed by the City. Therefore, for the purpose of this plan, it is assumed that ODOT would not require designing future improvements to meet the Highway Design Manual standards.

[^3]:    ${ }^{5} 95^{\text {th }}$ percentile queues represent queue lengths that have a five percent probability of being exceeded during the analysis period and are typically used when designing appropriate storage lengths at intersections.

[^4]:    ${ }^{6}$ ODOT Crash Reduction Factor List, 2020, CMF ID: 228

[^5]:    7 https://nacto.org/publication/transit-street-design-guide/station-stop-elements/stop-elements/small-transit-shelter/

